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Effective Length Factors

for

Solid Round Diagonals in Guyed Communication Towers

Ву

YEAN SUN

A Thesis Submitted to
The College of Graduate Studies and Research
Through The Faculty of Engineering
(Civil Engineering Program)
In Partial Fulfillment of the Requirements for
The Degree of Master of Applied Science at the University of Windsor

Windsor, Ontario, Canada 1999



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ABSTRACT

The objective of this investigation is to determine the effective length factors for solid round diagonals in all-welded communication towers. A total of thirty-three welded towers were tested in the investigation with all the towers in a horizontal position and concentrated load at mid-span. Of the thirty-three specimens, fifteen specimens were six-panel cross-braced towers with a span of 4572 mm (180 in). The leg sizes were 38.1 mm (1.5 in), 50.8 mm (2 in), 69.85 mm (2.75 in) diameter, and diagonal sizes were 12.7 mm (0.5 in), 14.29 mm (0.563 in),15.88 mm (0.625 in) diameter. Sixteen specimens were eight-panel cross-braced towers with a span of 5690 mm (224 in). The leg sizes were 38.1 mm (1.5 in), 50.8 mm (2 in), 57.15 mm (2.25 in) diameter, and the diagonal sizes were 19.05 mm (0.75 in), 22.23 mm (0.875 in),15.88 mm (0.625 in) diameter. Two specimens were six-panel single-braced towers with leg sizes of 50.8 mm (2.0 in) and 76.2 mm (3.0 in) and diagonal sizes of 22.23 mm (0.875 in), 28.58 mm (1.125 in) diameter.

Two specimens were fixed with strain gauges on every member, while all other specimens were tested with strain gauges fixed on only one panel.

After the test, tensile specimens were cut from the diagonals of the tower, and tested for the yield stress and tensile strength. Axial forces in the diagonal and leg members were calculated based on the actual yield stress and strain readings, assuming an elastic perfectly-plastic stress-strain curve for steel.

The buckling loads were determined from the maximum axial forces in the tested members, and effective length factors were calculated according to CSA-S37-94 Standard and AISC-LRFD Specifications. The average effective length based on CSA-S37-94 for cross-braced diagonals is 0.35 of the total diagonal length, while

the effective length is 0.37 of the total diagonal length based on AISC-LRFD. The effective length factor for single-braced diagonals is 0.50 and 0.56 based on CSA-S37-94 and AISC-LRFD, respectively.

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TABLE OF CONTENTS

| ABSTRACT | - vi |
|--|--------|
| ACKNOWLEDGEMENTS | – viii |
| LIST OF TABLES | - xii |
| LIST OF FIGURES | - xiii |
| NOTATION | - Xiv |
| CHAPTER 1 INTRODUCTION | |
| 1.1 General | - 2 |
| 1.2 Necessity for the Investigation | - 3 |
| 1.3 Objectives of Present Research | - 3 |
| CHAPTER 2 LITERATURE REVIEW | |
| 2.1 General | - 5 |
| 2.2 Flexural Buckling Theory and Experimental Investigation | |
| 2.2.1 Euler Formula | - 5 |
| 2.2.2 Tangent Modulus Theory | - 6 |
| 2.2.3 Reduced Modulus Theory | - 6 |
| 2.2.4 Effect of Residual Stress | |
| and Initial Out-of -Straightness | - 7 |
| 2.2.5 Flexural Buckling - Experimental Investigation | - 8 |
| 2.3 Buckling Theory and Experimental Investigation of Bracin | 9 |
| 2.4 Cross Bracing as a Continuous Beam on Elastic Support | - 13 |
| 2.5 Design Specifications for Cross-Bracings | |
| Based on CSA-S37-94 and AISC-LRFD | - 15 |
| 2.5.1 CSA-S37-94 Standard | - 15 |
| 2.5.2 AISC-LRFD Specifications | - 17 |

| CHAPIER 3 EXP | PERIMENTAL INVESTIGATION |
|-------------------|---|
| 3.1 General | |
| 3.2 Details of S | pecimens |
| | Braced Specimens |
| | Braced Specimens |
| | *************************************** |
| | en Set-Up |
| | cement of Compression Diagonals |
| | Bauges |
| | equisition System |
| | oplication |
| | Results |
| | ral Response |
| | al Properties |
| | • |
| CHAPTER 4 ANAL | YSIS OF RESULTS |
| 4.1 Failure Patte | ern of Tower Members |
| | aced Specimens |
| | raced Specimens |
| | of Axial Forces in Tested Members |
| | quilibrium Check |
| | n of Experimental Buckling Loads |
| and Effective | Length Factors |
| | ial Forces in Tension Diagonals |
| | Length Factors |
| | |
| CHAPTER 5 CONC | LUSIONS AND RECOMMENDATIONS |
| 5.1 Conclusions - | |
| | tions for further research |
| | _ |

| REFERENCES | 55 |
|-------------------------------------|--------------------|
| APPENDIX A | |
| Strain Gauge Location | 59-93 |
| APPENDIX B | |
| Load-Strain Data and Axial Forces 9 |) 4-191 |
| VITA AUCTORIS | 192 |

LIST OF TABLES

| Table 3.2.1a | |
|---|------|
| Details of Test Specimens (6-panel Cross-Braced Specimens) | - 20 |
| Table 3.2.1b | |
| Details of Test Specimens (8-panel Cross-Braced Specimens) | - 21 |
| Table 3.2.2 | |
| Details of Test Specimens (6-panel Single-Braced Specimens) | - 23 |
| Table 3.3.5a | |
| Calibration of (445kN) 100 kip Load Cell | - 30 |
| Table 3.3.5b | |
| Calibration of (890kN) 200 kip Load Cell | · 31 |
| Table 3.4.2a | |
| Yield Stresses and Tensile Strengths of Diagonals | |
| (6-panel Cross-Braced Specimens) | 32 |
| Table 3.4.2b | |
| Yield Stresses and Tensile Strengths of Diagonals | |
| (8-panel Cross-Braced Specimens) | 33 |
| Table 3.4.2c | |
| Yield Stresses and Tensile Strengths of Diagonals | |
| (6-panel Single-Braced Specimens) | 34 |
| Table 4.1.1 | |
| Failure Patterns of Buckled Compression Diagonals | 37 |
| Tables 4.4a, b, and c | |
| Effective Length Factors Using CAN/CSA-S16.1-94 | 45 |
| Tables 4.4d, e, and f | |
| Effective Length Factors Using AISC-LRFD Specifications | 48 |
| Table 4.4g | |
| Average Effective Length Factors | 51 |

LIST OF FIGURES

| Figure 2.5.1 | |
|--|----|
| Tension-compression Web System | 16 |
| Figure 3.2.1a | |
| Dimensions of 6-Panel Cross-Braced Specimens | 20 |
| Figure 3.2.1b | |
| Dimensions of 8- Panel Cross-Braced Specimens | 21 |
| Figure 3.2.2 | |
| Dimensions of 6-Panel Single-braced Specimens | 23 |
| Figure 3.3.2a | |
| Reinforcement of Specimens with horizontal at midspan | 24 |
| Figure 3.3.2b | |
| Reinforcement of Specimens without horizontal at midspan | 25 |
| Figure 3.3.5a | |
| Photograph of Test Set-Up | 27 |
| Figure 3.3.5b | |
| Test Set-Up | 28 |
| Figure 3.3.5c | |
| Calibration of 100 kip Load Cell | 30 |
| Figure 3.3.5d | |
| Calibration of 200 kip Load Cell | 31 |
| Figure 4.2.1 | |
| Diagram for Axial Force Calculation | 38 |
| Figure 4.2.2 | |
| Diagram for Axial Force Calculation | 40 |

NOTATION

| A | cross-sectional area |
|------------------|--|
| B _m | the thickness of slice "m" |
| С | force in the cross-braced compression member |
| C _{cr} | the critical load for compression member |
| C _e | Euler critical load |
| CT | the critical tangent modulus load |
| Cr | compressive resistance |
| D | diameter of the test member |
| dy | the thickness of slice |
| E | modulus of elasticity |
| E _T | tangent modulus of elasticity |
| Er | reduced modulus of elasticity |
| E _{eff} | effective modulus of elasticity |
| = | resultant axial force in the test member |
| cr | critical load according to AISC-LRFD Specification |
| m | resultant force in the slice "m" |
| y | yield stress of material |
| | moment of inertia |
| ì | moment of inertia of the tension diagonal |

| lc | moment of inertia of the compression diagonal |
|----------------|--|
| K | effective length factor |
| KL/ r | effective slenderness ratio of the member |
| L | length of compressive member |
| Ld | total length of diagonal center to center of legs |
| T | force in the cross-braced tension member |
| X | the depth of neutral axis |
| Ym | the distance measured from the center of slice to centroidal axis of the |
| | cross section |
| r | the radius of gyration |
| α | stiffness furnished by the tension member to compression member |
| α_{lim} | the limiting value of the stiffness of the elastic support |
| λ | the nondimensional slenderness parameter |
| ф | resistance factor for compression |
| € _m | the strain in the center of the slice "m" |
| σ_{m} | the stress for slice "m" |
| E1, E2 | strain readings in the opposite sides of the test member |

CHAPTER 1

INTRODUCTION

1.1 General

With the rapid development of world economy and technology, in the fields of construction and telecommunication, more and more welded towers are constructed and used. The welded towers are either self-supporting or guyed towers. Self-supporting latticed towers are of variable cross-section, whereas guyed communication towers are of constant triangular or square cross-section.

Welded towers consist of legs, diagonals, and sometimes horizontals, which are connected together by welding. Solid rounds, tubes, as well as angles are used for the components of the welded towers. Diagonals can be arranged in cross-braced or single-braced configuration.

Towers with cross-braced diagonals can be fabricated in one of the following ways:

Type I: one diagonal straight and the other bent around and welded at the intersection.

Type II: both the cross-braced diagonals are in-plane with one of them continuous and the other cut and welded to the continuous member.

Type III: both the cross-braced diagonals are out-plane at mid-span and then welded together at their intersection.

During the design of welded towers, effective length factors for diagonals are a major parameter in the computation of the compressive strength of diagonals. Effective length factors for cross-braced diagonals of type III are the subject of this investigation.

1.2 Necessity for the Investigation

To the best of author's knowledge, though many experiments have been carried out on the behavior of cross-braced angle diagonals, little experimental investigation was carried out on the behavior of cross-braced solid round members. CSA-S37-94 "Antennas, Towers and Antenna-Supporting Structures" (CSA 1994) doesn't give specific effective length factors for solid rounds. It only gives 0.75 for the cross-braced angle diagonals, and notes that for the cross-braced solid round diagonals, the philosophy is the same as that of angles. Based on the preliminary results of investigation carried out at the University of Windsor (Jaboo 1998), the effective length was found to be less than 0.5 of the diagonal length. There is a need to confirm this result by carrying out tests on additional specimens fabricated by different manufacturers.

1.3 Objectives of Present Research

The objectives of this investigation are:

- To study the failure patterns of cross-braced and of single-braced solid round diagonals for welded towers.
- To determine effective length factors of type III cross-braced and of single-braced solid round diagonals for welded towers.

CHAPTER 2

LITERATURE REVIEW

2.1 General

The use of solid round columns dates back many centuries. The materials used varied from stone, wood, concrete, and metals. Steel has been widely used in many structural elements. Solid round steel bars have been used in constructing trusses, frames, and towers. In lattice towers, solid rounds are used for legs, horizontals, and bracing diagonals. Single and cross-braced diagonals are frequently used in such structures.

A large amount of literature is available, theoretical and experimental, about the design of cross-bracings, but most of the work carried out was on angles and flat bars. Very little literature is available on cross-bracings made of solid round bars, although this type of section is quite common for antenna towers.

Structural member buckling capacities are dependent upon the mode of buckling. For axisymmetrical solid round cross sections, the mode of buckling is flexural buckling.

2.2 Flexural Buckling Theory and Experimental Investigation

2.2.1 Euler Formula

Stability of columns has been one of the most widely known aspects of structural engineering. Research with regard to a solution to column problem dates back to many centuries. One of the most important contributions to the problem was made by Euler (1759) who established a formula for the buckling of columns in analyzing the elastic stability of many engineering structures. Euler's formula is as follows:

$$C = \frac{\pi^{-2} EA}{\left(\frac{KL}{r}\right)^2}$$
 (2.1)

where, E is the modulus of elasticity, A is the area of the cross-section, K is the effective length factor, L is the length of the column, and r is the radius of gyration. Euler's load, C_e, is the critical load at which a slender elastic column can be held in a bent configuration under axial load alone. The formula is valid only when the stress does not go beyond the elastic limit of the material.

2.2.2 Tangent Modulus Theory

Due to lack of knowledge as to relationship between stress, strain, curvature, and bending moment beyond the elastic range, progress beyond Euler's early statements concerning inelastic behavior remained dormant for many years. In 1889, Engesser proposed that the Euler's formula be extended to include the inelastic range by introducing a variable quantity E_T which is called the tangent modulus, instead of the constant modulus E. Thus for a hinged-end column, the buckling formula should be changed to tangent modulus formula:

$$C_{T} = \frac{\pi^{-2} E_{T} A}{\left(\frac{KL}{r}\right)^{2}}$$
 (2.2)

where, E_T is the slope of the tangent to stress-strain curve corresponding to the the stress at failure, KL/r is the effective slenderness ratio of the member, and C_T is the critical tangent modulus load.

2.2.3 Reduced Modulus Theory

Independent of Engesser, Considere in 1889 conducted a series of 32 column tests and suggested that if buckling occurred above the proportional limit, the elastic modulus, E, should be replaced in Euler's formula by the effective modulus $E_{\text{eff.}}$ He stated that the effective modulus should be somewhere between E and E_t . Jasinsky (1889) brought Considere's work to the attention of

Engesser, who revised his theory by introducing two different moduli for the two parts, convex and concave sides of the buckled shape of the cross-section.

In 1910 Karman derived explicit expressions for the reduced modulus for both rectangular and idealized H-section columns. The formula for critical reduced modulus stress in a pinned-end column is the same as equation (2.2) except that E_T (tangent modulus) is replaced by E_r (reduced modulus), where

$$E_r = f(E_T, E) \tag{2.3}$$

2.2.4 Effect of Residual Stress and Initial Out-of-Straightness

The need for information on the strength of solid round compression members became necessary from the increased use of these bars in communication towers. For this reason, an extensive program of experimental and analytical work was initiated in 1954 at Lehigh University, Bethlehem, Pennsylvania. Beedle, Galambos, and Tall (Beedle et al. 1961) studied the effect of heattreatment and cold bending on the residual stresses and column strength. Effects of initial out-of-straightness were also illustrated. It was stated that for solid round bars, the residual stress distribution is triaxial, i.e. there are longitudinal, tangential and radial residual stresses. Different final heat treatment methods like quenching, air cooling, and stress relieving were considered in the study. It was found that of the three types of heat treatment, quenching leads to high residual stresses while the other two methods reduce the stresses considerably. It was also shown that columns with initial out-of-straightness have lower strength than straight columns. Fujita and Driscoll (1962) presented results of the aforementioned experimental investigation on the strength of axially and eccentrically loaded solid round columns of 69.9 mm (2-3/4 in.) diameter. Comparison with a theory based on "the tangent modulus" concept for axially loaded columns showed that the strength of solid round columns may be predicted adequately. Galambos (1965) presented the research on the strength

of solid rounds carried out between 1954 and 1965 at Lehigh University. Recommendations for the design of axially loaded steel columns were presented based on the research program. It was stated that both residual stresses and initial crookedness have a significant influence on the strength of round columns in the inelastic region. Galambos' paper was discussed by Williamson and Johnston (1965).

2.2.5 Flexural Buckling - Experimental Investigation

Experimental investigations on columns date back to the first half of the eighteenth century. A practical investigation of the phenomenon of lateral buckling was first undertaken by Mussghenbrock (Timoshenko 1953). As a result of this research, it was stated that the buckling load was inversely proportional to the square of the length of the strut. During the closing years of the eighteenth century, a series of investigations with wooden struts were made.

Hodgkinson in 1840 (Timoshenko 1953) tested specimens of cast iron. Cylindrical, solid and hollow specimens with rounded and flat ends were tested. For slender, solid struts, good agreement was found with Euler's formula. At the end of the nineteenth century, more experiments on buckling of columns were conducted by Bauschinger, Tetmajer, and Considere (Timoshenko 1953).

Several researchers studied the column buckling criteria in the first half of this century and found that the results showed column failure at tangent modulus loads. Templin and others (Templin et al. 1938) also discovered that practical tests on columns yielded capacities that were closer to tangent modulus theory than to the seemingly more refined reduced modulus theory.

As discussed earlier, the primary research on the strength of solid rounds was carried out between 1954 and 1965 at Lehigh University. The tests were performed primarily on stress relieved constructional alloy steel bars. Twenty-

seven bars, some with 69.9 mm (2-3/4 in) diameter and others with 190.5 mm (7-1/2 in) diameter were tested to failure as axially loaded columns. In the main phase of the research program, the effect of residual stresses and initial crookedness on the strength of the axially loaded columns was investigated. To the best of author's knowledge, no major research work in this area was undertaken after this time.

2.3 Buckling Theory and Experimental Investigation of Bracing

Bracings are widely used in many structures. Bracings in wooden bridge trusses and roof trusses were used by the Romans. The first metal trusses in England were built in 1845 (Timoshenko 1953).

The first experiments on lattice girders, treated as cantilevers, were made in 1857 by Lohse (Todhunter 1960). Single, double, triple, and fourfold types of bracings were used. The bars were riveted to each other. The loads at which the bracing buckled were noted. It is noteworthy that in several cases the bracing bars failed elastically into an approximate S-form, a result which the researchers at the time did not take into account in their theoretical analysis. From these experiments, a great increase of strength, due to multiple bracing and to the riveting together of the bracing bars, was noticed.

Wohler in 1855 (Todhunter 1960) deduced that the stresses in the bracing bars of a girder from purely statistical consideration. De clercq in 1857 and Winkler in 1859 theoretically analyzed lattice girders and the stresses in the bracing bars (Todhunter 1960).

For cross-braced or tension-compression diagonals, Jasinsky was the first to investigate the stability of the compressed diagonals and to evaluate the strengthening afforded by the diagonals in tension in lattice trusses (Timoshenko 1953).

Dewolf and Pelliccione (1979) reported that the design practice for cross- braced members adopted at that time, which entirely neglected the contribution of the compression member and relied solely on the tension member, was conservative and would result in overdesign. Eight sets of cross-bracings, using flat bars with rectangular cross section, were tested to failure. A square frame was used with connections at each corner of the frame designed to allow all members to rotate in the plane of the frame and for the two diagonals to rotate out of the plane. Strain gauges were placed in pairs on opposite sides of the members on the faces parallel to the plane of the frame. From the tests in that investigation, it was observed that using the design practice, which neglects the contribution of compression members, predicted frame load ranged from 40% to 78% of the failure load. The critical load of the compression member about its in-plane axis is related to the force in the tension member that braces it at the center, and when the two members are made of the same material, the tension member is equivalent to an unyielding support. Thus the compression member buckles into a full sine wave, S-shape, at a load equal to four times that without any center bracing. The stiffness, α , furnished by the tension member acting on compression member in the out-of-plane direction was given as follows:

$$\alpha = \frac{48EI}{L^3} \left(\frac{\mu^3}{3(\mu - \tanh \mu)} \right)$$
 (2.4)

where L represents the total length of the diagonal, and

$$\mu = \frac{L}{2} \sqrt{\frac{T}{EI}} \tag{2.5}$$

in which T is the force in tension member.

It was also stated that following buckling of the compression member, its load decreased and the load in the tension member then increased with an overall increase in frame load. Predicted frame loads, based on the critical load in the compression member determined by using the tension member as a brace, were within 10% of the test load for compression members with low slenderness ratios and on the conservative side for those with higher ratios.

A theoretical investigation was made by Vickers (1982) into the behavior and design of cross-bracing. His discussion emphasized the use of cruciform (star shaped) double angle struts for bracing members. The extent of lateral support provided to the compression diagonal by the tension diagonal at their point of intersection was analyzed. From his study, it was concluded that the design concept of shared load between tension and compression members with the compression member designed using effective length equal to half the total length of the diagonals is more realistic than "tension only" bracing design.

El-Tayem and Goel (1986) studied experimentally and theoretically full-scale cross-bracing specimens. Five single-angle cross-braced specimens and one double-angle cross-braced specimen were included in the study. Quasi-static cyclic loading was used in the tests and strain gauges were attached to measure the loads. It was noted that the interconnection provided an elastic restraint against both lateral and rotational deformations of the compression diagonal at the point of intersection. It was concluded that for cross-braced systems made from single equal-leg angles, an effective length of 0.85 times the half diagonal length is reasonable.

Picard and Beaulieu (1987) did a theoretical study aimed at the determination of the transverse stiffness offered by the tension diagonal in cross-braced systems and at the evaluation of this stiffness on the out-of-plane buckling resistance of the compression diagonal. When the diagonals were continuous and attached at the intersection, it was concluded that the effective length of the compression

diagonal is 0.5 times the total diagonal length. A simpler form of equation was given by the writers for the stiffness, α , provided by the tension diagonal, assuming the two diagonals to be equal in length and to have the same cross-sectional area:

$$\alpha = \frac{48 EI}{L^3} + 4.36 \frac{T}{L}$$
 (2.6)

where, L is the total length of the diagonal, and T is the force in tension diagonal. They also suggested that the effective length factor, K, for calculating the buckling load of the compression diagonal to be as follows:

$$K = \sqrt{0.523 - \frac{0.428}{C/T}} \ge 0.5 \tag{2.7}$$

where C and T are the forces, just before buckling, in the compression and the tension diagonals respectively.

Picard and Beaulieu (1988) performed two series of tests to demonstrate the validity of their theoretical study. Seven transverse stiffness tests and fifteen buckling tests were performed on flat bars and the results verified the validity of the equations presented by them.

The theoretical analysis carried out in 1987 by the same authors was generalized in 1989 (Picard and Beaulieu 1989), which gives the following the effective length factor for cross bracings:

$$K = \sqrt{\frac{1 - 0.818 (C/T)}{1 + 0.911 (I_{t}/I_{c})}}$$
 (2.8)

where, C/T is the ratio of the force in compression member just before buckling to the force in tension diagonal, and lt/lc is the ratio of moment of inertia of the

tension diagonal to the moment of inertia of the compression diagonal. This theoretical study was also verified by fifteen buckling tests carried out in 1988 (Picard and Beaulieu 1988).

Kemp and Behncke (1998) described a series of tests on cross-braced systems with slenderness ratios in the range of 102 to 160. Other variables included the inclination of the main legs and bracing, the number of bolts in each end connection, and the size of the main leg relative to the bracing. The measured behaviour was compared with the results of a flexibility-based analysis and the formulas from the American and European Transmission Tower Design manuals. The results confirmed the complexity of the behavior of cross-bracing in latticed towers. Strain measurements showed that yielding of the extreme fiber of the strut in the central region of the largest sub-span is the primary cause of failure. The effect of the end eccentricity was partially alleviated by the restraint provided by the main legs to the ends of the compression diagonal. Consequently the ultimate strength in the tests was increased up to 17% by changing the number of bolts at the end connection from one to two. A smaller but nevertheless significant, 10%, benefit was obtained by increasing the size ratio of the main leg relative to the bracing.

Jaboo (1998) conducted an experimental investigation on 8 single-braced and 18 cross-braced towers to determine effective length factors for solid round members. He found effective length factor, K = 0.525 for single-braced solid round diagonal, K=0.429 and 0.365 for type I and type II cross-braced solid round members, respectively.

2.4 Cross-Bracing as a Continuous Beam on Elastic Support

Connections in trusses and frames are treated in many different ways, but the traditional assumption of considering these connections to be perfectly hinged joints in an idealized frame made the design of such frames or trusses simpler.

In cross-braced diagonals, the tension diagonal acts as an elastic spring at the point of intersection with the compression diagonal. Thus the compression diagonal could be assumed as a continuous bar simply supported at the ends and having an intermediate elastic support.

Timoshenko and Gere (1961) discussed such a problem. A case where the intermediate elastic support is at the middle and the axial force does not change within the two halves of the member was explained. It was shown that if the stiffness of the elastic support, α , approaches infinity, the deflected shape of a bar on three hinged supports will be a full-sine wave, and the critical load, C_{cr} , for the compression member will be:

$$C_{cr} = \frac{\pi^{-2} EA}{\left(\frac{0.5 L}{r}\right)^2}$$
 (2.9)

And when α approaches zero assuming the intermediate support to be absolutely flexible, the shape of the deflection curve of the buckled bar will be as half sine wave, and the critical load, C_{cr} , will be:

$$C_{cr} = C_{e} = \frac{\pi^{2} EA}{\left(\frac{L}{r}\right)^{2}}$$
 (2.10)

The limiting value of the stiffness of the elastic support, at which the full sine wave shape of the buckled bar occurs, is given as below:

$$\alpha_{lim} = \frac{16 \pi^2 EI}{L^3}$$
 (2.11)

For values of α smaller than α_{lim} , the flexibility of the intermediate support should be considered, and it is shown that the relation between the elastic critical load C_{cr} and the stiffness of the elastic support α is:

$$C_{cr} = C_e + \frac{3\alpha L}{16} \le 4C_e$$
 (2.12)

It has to be mentioned that the assumption of hinged joints does not represent correctly all the types of connections in trusses or frames as the rotational restraint exists in cases where the joints are welded or even bolted. But because of the complexity associated, especially with the degree of rotational constraint provided by different types of connections, it is always preferable to assume a hinged end condition which is a conservative assumption.

2.5 Design Specifications for Cross-Bracings Based on CSA-S37-94 and AISC-LRFD

2.5.1 CSA-S37-94 Standard

CSA-S37-94 is the Canadian Standard for communication towers. The maximum slenderness ratio for bracing members is limited to 200 as stated in Clause 6.1.5.2 of CSA-S37.

For the computation of compressive strength of solid rounds as single bracing in towers, Clause 6.2.2.1 of the Standard states:

"The unbraced length, L_d of compression members other than leg members, shall be the distance along the axis of the member to which it is attached. For simple web bracing systems, with web member connected directly or by gussets to the leg member, the slenderness ratio is L_d/r , where, L_d is the length of the diagonal, and r is the radius of gyration."

As for cross bracing, Clause 6.2.2.2 of the Standard states:

"For tension-compression web systems the diagonals shall be connected where they intersect and the lengths of the compression member (L_1 and L_2 in Figure 2.5.1) shall be the distances from the intersection of the two diagonal members to the center of the leg members at the ends of the compression member."

The effective slenderness ratio of the compression member is KL/r, where $KL = L_1 + 0.5L_2$ (L₁ larger than L₂), and r = radius of gyration.

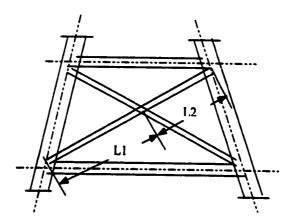


Figure 2.5.1 Tension-Compression Web System

After determining the slenderness ratio of the member, the nondimensional slenderness parameter, λ , is calculated as:

$$\lambda = \frac{KL_d}{r} \sqrt{\frac{F_y}{E\pi^2}}$$
 (2.13)

This nondimensional slenderness parameter, λ , is used in computing factored compressive resistance C_r of the member:

$$C_r = \phi A F_y (1 + \lambda^{2n})^{-\frac{1}{n}}$$
 (2.14)

where

φ resistance factor for compression

A cross-sectional area of the member

Fy yield stress

 λ nondimensional slenderness parameter

n = 1.34

2.5.2 AISC-LRFD Specifications

Formula given by above specifications is as follows:

$$\lambda = \frac{KL}{r \pi} \sqrt{\frac{F_y}{E}}$$
 (2.15)

For

$$\lambda \leq 1.5$$
,

$$F_{cr} = (0.685^{\lambda_c^2}) F_y \tag{2.16}$$

$$\lambda > 1.5$$

$$F_{cr} = \left\{ \frac{0.877}{\lambda_c^2} \right\} F_{y} \tag{2.17}$$

where

Fy = specified yield stress

E = modulus of elasticity

K = effective length factor

L = unbraced length of member

r = governing radius of gyration about plane of buckling

CHAPTER 3

EXPERIMENTAL INVESTIGATION

3.1 General

For this investigation, tests were conducted on thirty-three specimens that were fabricated by three different American tower manufactures. Fifteen of the specimens were six-panel cross-braced towers with seven of the specimens having horizontals and the others no horizontals. Sixteen of the specimens were eight-panel cross-braced towers with half of the specimens having horizontals and the other half no horizontals. Finally, the last two specimens were six-panel single-braced towers with flat horizontals. Three sizes of legs (38.1 mm, 50.8 mm, 69.9 mm diameter), three sizes of diagonals (12.7 mm, 14.3 mm, 15.9 mm diameter) and one size of horizontal (19.1 mm diameter) were used for the six-panel towers. Similarly, the eight-panel towers were fabricated with three sizes of legs (38.1 mm, 50.8 mm, 57.2 mm diameter) and three sizes of diagonals (15.9 mm, 19.1 mm, 22.2 mm diameter). Two sizes of diagonals (28.6 mm, 22.2 mm diameter) and two sizes of legs (50.8 mm and 76.2 mm diameter) were used for the two single-braced specimens.

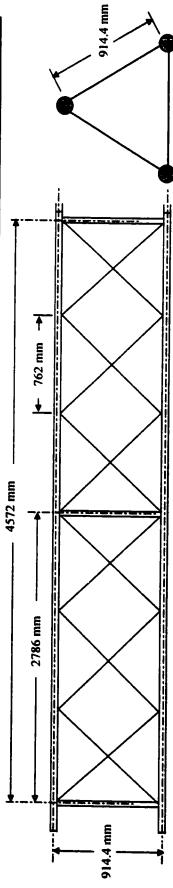
3.2 Details of Specimens

3.2.1 Cross-Braced Specimens

Fifteen six-panel specimens and sixteen eight-panel specimens are included in the investigation. They all have a 914.4 mm triangular section with all legs, horizontals (where present), and diagonal members connected together by welding. The six-panel specimens have a total length of 4572 mm (one panel of 762 mm) with the diagonals continuously-bent and welded at the leg junction. The eight-panel specimens have a total length of 5690 mm (one panel length of 711 mm) with the diagonals cut and welded at the leg junction. Each pair of cross-braced diagonals is welded together at their junction. The details of the specimens are shown in Tables 3.2.1a and b and Figures 3.2.1a and b.

Table 3.2.1a: DETAILS OF TEST SPECIMENS

| | | | 7 | Τ | Τ | Т | Τ | Τ | Т | Т | Т | Т | Т | Т | Т | Т | Т | 7 |
|--------------------------------|------------|--------------|----------------------|----------------------|----------------------|-----------------------|----------------------|-----------------------|-----------------------|----------------------|----------------------|-------------------------|----------------------|----------------------|----------------------|----------------------|-------------------------|---|
| • | | Fabricator | ERI Inc. Chandler IN | ERI Inc. Chandler IN | ERI Inc. Chandler IN | ERI. Inc. Chandler IN | ERI Inc. Chandler IN | ERI. Inc. Chandler IN | ERI. Inc. Chandler IN | ERI Inc. Chandler IN | ERI Inc. Chandler IN | ERI, Inc., Chandler, IN | ERI Inc. Chandler IN | ERI, Inc., Chandler, IN | |
| | Horizontal | Size | No. | 19.1 | 19.1 | 19.1 | 2 | 2 | 19.1 | 19.1 | 19.1 | 2 | 2 | Š | 19.1 | 19.1 | 19.1 | |
| ECIMENS | Diagonal | Size (mm) | 12.7 | 12.7 | 12.7 | 12.7 | 14.3 | 14.3 | 14.3 | 14.3 | 14.3 | 15.9 | 15.9 | 15.9 | 15.9 | 15.9 | 15.9 | |
| ICED SP | Leg | Oize (mm) | 38.1 | 38.1 | 38.1 | 38.1 | 50.8 | 50.8 | 50.8 | 50.8 | 50.8 | 6.69 | 6.69 | 6.69 | 6.69 | 6.69 | 6.69 | |
| 6-PANEL CROSS-BRACED SPECIMENS | Face Width | (mm) | 914.4 | 914.4 | 914.4 | 914.4 | 914.4 | 914.4 | 914.4 | 914.4 | 914.4 | 914.4 | 914.4 | 914.4 | 914.4 | 914.4 | 914.4 | |
| 6-PANEL | Panel | (mm) | 762 | 762 | 762 | 762 | 762 | 762 | 762 | 762 | 762 | 762 | 762 | 762 | 762 | 762 | 762 | |
| | Span | (mm) | 4572 | 4572 | 4572 | 4572 | 4572 | 4572 | 4572 | 4572 | 4572 | 4572 | 4572 | 4572 | 4572 | 4572 | 4572 | |
| | Specimen | Ö. | S1A | SZA | S2B | S2C | S3A | S3B | S4A | S4B | S4C | S5A | S5B | SSC | S6A | SeB | Sec | |
| | Test | ġ | 9 | 4 | 8 | 23 | 7 | 25 | - | 9 | 2 | 2 | 5 | 12 | = | 13 | 24 | |
| | Serial | Š | - | ဇ | 4 | သ | စ | 7 | 80 | 6 | , | = | 12 | 13 | 4 | 15 | 16 | |



CROSS-SECTION

Figure 3.2.1a: DIMENSIONS OF 6-PANEL SPECIMEN

Table 3.2.1b: DETAILS OF TEST SPECIMENS

| | | • | | (8-PANE | 8-PANEL CROSS-BRACED SPECIMENS | 3RACED | SPECIMEN | (S) | |
|----------|-----------|--|--------|-----------|--------------------------------|---------------|----------|----------------|--------------------------|
| 10:00 | 1 25 | - C. | Span | Panel | Face | Leg | Diagonal | | |
| Serial | | | Length | Length | Width | Size | Size | Horizontal | Fabricator |
| o Z | 2 | | (mm) | (mm) | (mm) | (mm) | (mm) | | |
| - | 22 | P1A | 2690 | 711.2 | 914.4 | 38.1 | 15.9 | Yes | PIROD Inc., Plymouth, IN |
| 7 | 31 | P1B | 2690 | 711.2 | 914.4 | 38.1 | 15.9 | Yes | PIROD Inc., Plymouth, IN |
| 9 | 21 | P2A | 2690 | 711.2 | 914.4 | 38.1 | 15.9 | No | PIROD Inc., Plymouth, IN |
| 4 | 27 | P2B | 2690 | 711.2 | 914.4 | 38.1 | 15.9 | No | PIROD Inc., Plymouth, IN |
| 2 | 90 | P3A | 2690 | 711.2 | 914.4 | 50.8 | 19.1 | Yes | PIROD Inc., Plymouth, IN |
| 9 | 32 | P3B | 2690 | 711.2 | 914.4 | 8.03 | 19.1 | Yes | PIROD Inc., Plymouth, IN |
| 7 | 29 | P4A | 2690 | 711.2 | 914.4 | 8.03 | 19.1 | No | PIROD Inc., Plymouth, IN |
| 80 | 20 | P4B | 2690 | 711.2 | 914.4 | 8.03 | 19.1 | S _O | PIROD Inc., Plymouth, IN |
| 6 | 26 | P5A | 2690 | 711.2 | 914.4 | 57.2 | 22.2 | Yes | PIROD Inc., Plymouth, IN |
| 01 | क्ष | P58 | 2690 | 711.2 | 914.4 | 57.2 | 22.2 | Yes | PIROD Inc., Plymouth, IN |
| - | 28 | P6A | 2690 | 711.2 | 914.4 | 57.2 | 22.2 | N _o | PIROD Inc., Plymouth, IN |
| 12 | 15 | P6B | 2690 | 711.2 | 914.4 | 57.2 | 22.2 | No No | PIROD Inc., Plymouth, IN |
| 13 | 18 | P7A | 2690 | 711.2 | 914.4 | 38.1 | 22.2 | Yes | PIROD Inc., Plymouth, IN |
| 14 | 17 | P7B | 2690 | 711.2 | 914.4 | 38.1 | 22.2 | Yes | PIROD Inc., Plymouth, IN |
| 15 | 33 | P8A | 2690 | 711.2 | 914.4 | 38.1 | 22.2 | No | PIROD Inc., Plymouth, IN |
| 16 | 19 | P8B | 2690 | 711.2 | 914.4 | 38.1 | 22.2 | No | PIROD Inc., Plymouth, IN |
| ₹ | | | | 5689.6 mm | - mm | | | * | |
| 3 | | | | | _ | | | | |
| Z | | 2848.8 mm | s mm | | | | /11.2 mm | | * |
| | | | | | | | | | 914.4 mm |
| 914.4 mm | < | < | < | < | < | < | < | | \ <u></u> |
| | | | | | | \times | | | |
| | | | | | | | | | |

Figure 3.2.1b DIMENSIONS OF 8-PANEL SPECIMEN

3.2.2 Single-Braced Specimens

Two six-panel single-braced specimens were tested in the investigation. They also have a triangular cross-section with all legs, horizontals and diagonal members welded together. The specimens have a total length of 6096 mm (one panel length of 1016 mm). The details of the specimens are given in Table 3.2.2 and Figure 3.2.2.

3.3 Test Set-up

3.3.1 Specimen Set-up

The tests of specimens were carried out in the Structural Laboratory, University of Windsor, with the specimens tested as horizontal simply supported beams, loaded with a central concentrated load which was provided by a hydraulic jack attached to the steel test frame. A laboratory crane was used to set up the test specimens in proper position. i.e. the specimens were seated on the two end supports with the middle of the specimen just under the load jack.

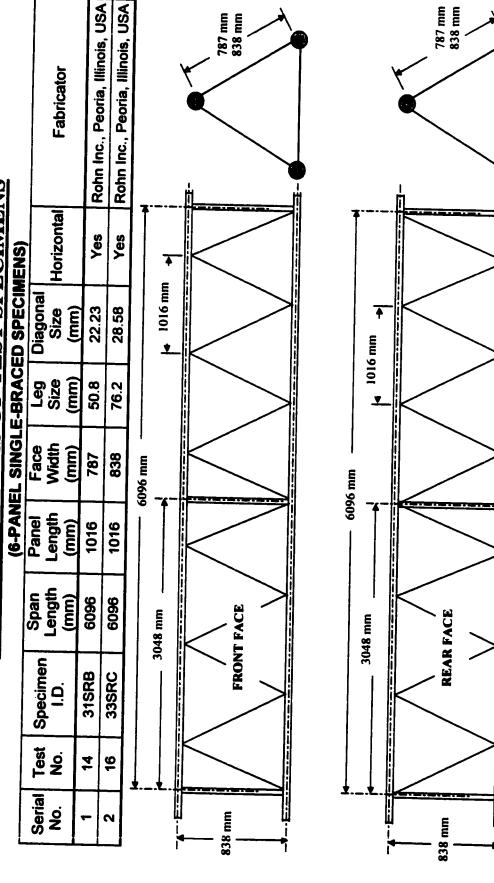
3.3.2 Reinforcement of Compression Diagonals

All compression diagonals in panels, other than the one under investigation, were reinforced with four U-bolted angles to make sure that the diagonals of interest would buckle. Details of specimen reinforcement are given in Figures 3.3.2a and b.

3.3.3 Strain Gauges

Electric resistance strain gauges, fabricated by KYOWA, JAPAN, type KFG-5-120-c1-11, with a gauge length of 5 mm and a gauge factor of 2.12 were used to measure the strain in the members of the test panel of the specimen.

Table 3.2.2: DETAILS OF TEST SPECIMENS



CROSS-SECTION

Figure 3.2.2 DIMENSIONS OF 6-PANEL SINGLE-BRACED SPECIMEN

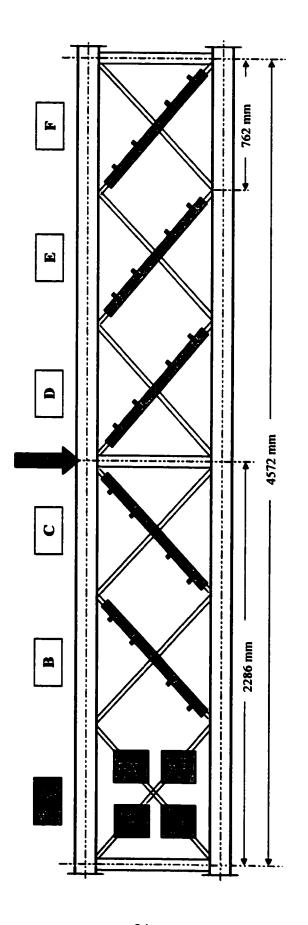


Figure 3.3.2a Test Panel A (strain gauges attached). Compression Diagonals in panels B, C, D, E and F were Reinforced with Angles as Shown

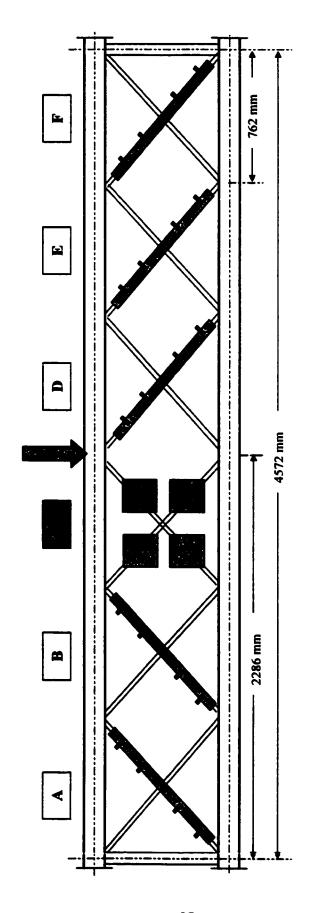


Figure 3.3.2b: Test Panel C (strain gauges attached). Compression Diagonals in Panels A, B, D, E and F were Reinforced with Angles as Shown

The strain gauges were fixed to individual members of the test specimen at the proper position after the surface was properly polished, cleaned with chemicals, and dried with Q-tips.

Based on previous experience of buckling of diagonal members, all the strain gauges were located at one-third the diagonal length, measured from the leg. For the first specimen, each panel was tested with 18 strain gauges to determine the force distribution in the diagonals and legs of the specimen whereas 14 strain gauges are used for each panel of the second specimen. For all other specimens, only the one pre-selected failure panel was tested with 16, 24 or 32 strain gauges fixed on both the compressive and tensile diagonals (strain gauges were put on legs for a few cases). Details of strain gauge location and numbering for each specimen are shown in Appendix A (Strain gauge location on specimens).

3.3.4 Data-Acquisition System

Readings of load cell and strain gauges were recorded automatically in the hardware of the computer as a text file with Datascan data acquisition system. The load cell and strain gauges were connected to the Datascan channels twelve hours after the strain gauges were fixed to the specimens. Microsoft Word and Excel programs were used to transfer the text file into Excel table for the convenience of data output and axial force calculations.

3.3.5 Load Application

The load was applied with a mechanical pump through a hydraulic jack attached to the beam of the steel test frame. Previously calibrated 445 kN (100 kip) and 890 kN (200 kip) load cells were used to measure the applied load. Details of load application are shown in Figures 3.3.5a and b.

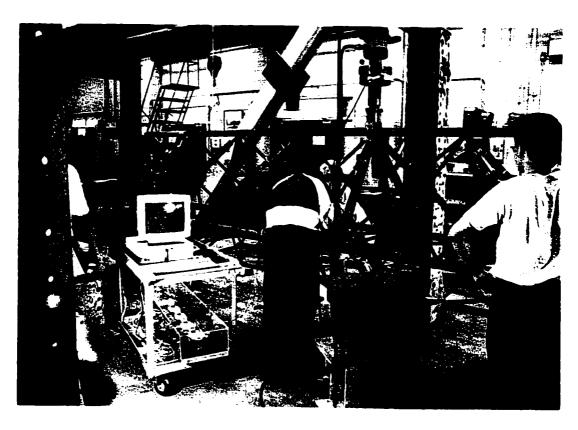
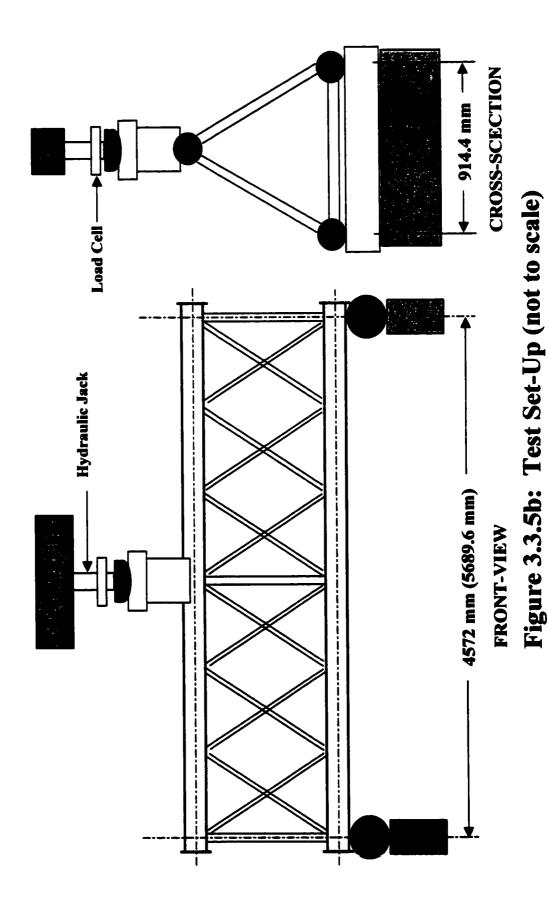


Figure 3.3.5a: Photograph of Test Set-up



Before starting the test, a Tinius Olsen Universal Testing Machine and a strain indicator were used to calibrate the load cells. Calibration data and curves are shown in Tables 3.3.5a and b and Figures 3.3.5c and d.

In order to get an accurate value of the axial forces based on the readings of strain gauges, care was taken in positioning the strain gauges to ensure that they are diametrically opposite.

3.4 Experimental Results

3.4.1 Structural Response

With the application of a central concentrated load, the axial forces and bending moments in the tested diagonals increase until the tested diagonals buckled. During the tests, the buckled diagonals and their buckling sequences were noted and are presented in Table 4.1.1. The load increments towards the end were kept small by monitoring the maximum strain readings of the test diagonals. The strain readings and axial forces are shown in Appendix B (Load-Strain Data and Axial Forces).

3.4.2 Material Properties

A total of 132 diagonal tensile specimens were cut from the compression diagonals (four tensile specimens for each tower), and tested in the Tinius Olsen Universal Testing Machine. The yield load and maximum failure load were obtained and the yield stress and tensile strength for each specimen were determined. The values of yield stress and tensile strength for each tower are given in Tables 3.4.2a, b and c.

Table 3.3.5.a: Calibration Data for 445 kN (100 kip)Load Cell

| OADVENIL | | MICRO-STRAIN READINGS | UN READING | 2 |
|----------|----------|-----------------------|------------|---------|
|) | READING1 | READING2 | READINGS | AVERAGE |
| 0 | 0 | 0 | 0 | 0 |
| 9 | 351 | 367 | 358 | 359 |
| 8 | 702 | 720 | 710 | 711 |
| 120 | 1059 | 1073 | 1062 | 1065 |
| 991 | 1405 | 1421 | 1412 | 1413 |
| 200 | 1762 | 1771 | 1762 | 1765 |
| 240 | 2098 | 2118 | 2109 | 2108 |
| 280 | 2448 | 2464 | 2454 | 2455 |
| 320 | 2797 | 2812 | 2801 | 2803 |
| 360 | 3147 | 3162 | 3148 | 3152 |
| 400 | 3500 | 3506 | 3497 | 3501.00 |

Figure 3.3.6c: Calibration Curve for 100 kip Load Cell
(gauge factor 2.062)

CALIBRATION CURVE

450

A 200

C 50

100

100

2000
3000
4000
MICRO-STRAIN

Table 3.3.5.b: Calibration Data for 890 kN (200 kip)Load Cell

Figure 3.3.5d: Calibration Curve for 200 kip Load Cell

900 200 CALIBRATION CURVE **4**00 (gauge factor 2.062) LOAD (KN) 300 200 2 0 2500 2000 1500 1000 1000 200 MICRO-STRAIN MICRO-STRAIN READINGS 00 30 108 108 108 108 108 11724 11724 11844 11844 11844 LOAD(KN)

Table 3.4.2a: YIELD STRESSES AND TENSILE STRENGTHS OF DIAGONALS

(6-PANEL CROSS-BRACED SPECIMENS)

| TEST SERIAL NO. | SPECIMEN I.D. | DIAMETER OF DIAGONAL (mm) | AVERAGE MEASURED YIELD STRESS (MPs) | AVERAGE MEASURED TENSILE STRENGTH (MPs) |
|-----------------|---------------|---------------------------|--|---|
| • | SIA | 12.7 | <i>1</i> 9¢ | # |
| • | \$18 | 12.7 | 960 | 203 |
| + | 82A | 12.7 | 378 | 84 |
| • | 828 | 12.7 | 696 | 84 |
| 23 | 820 | 12.7 | 596 | 478 |
| 7 | 83A | 14.3 | 996 | 632 |
| 25 | 838 | 14.3 | 260 | 632 |
| 1 | 84A | 14.3 | 378 | 3 |
| 3 | 978 | 14.3 | 378 | 236 |
| 9 | 246 | 14.3 | 367 | 2 |
| 23 | 86A | 16.9 | 386 | 902 |
| 10 | 858 | 16.9 | 386 | 702 |
| 12 | 86 C | 16.9 | 378 | 3 |
| + | 86A | 16.9 | 386 | 602 |
| 13 | 868 | 16.9 | 382 | 502 |
| 26 | 3 6 C | 16.9 | 385 | 602 |

Table 3.4.2b: YIELD STRESSES AND TENSILE STRENGTHS OF DIAGONALS

(8-PANEL CROSS-BRACED SPECIMENS)

| TEST SERIAL NO. | SPECIMEN 1.D. | DIAMETER OF DIAGONAL (mm) | AVERAGE MEASURED YIELD STRESS (MPs) | AVERAGE MEASURED TENSILE STRENGTH (IMPs) |
|-----------------|---------------|---------------------------|-------------------------------------|---|
| 22 | * | | | |
| | | 16.9 | 363 | |
| 35 | 7.0 | 16.9 | 376 | |
| 21 | 774 | | | 300 |
| 2 | | | 373 | 603 |
| | 28 | 16.9 | 373 | 603 |
| 8 | F3A | 19.1 | 407 | |
| 22 | P38 | 19.1 | 4 | |
| R | P ** | | | 696 |
| 8 | Ped | | 410 | 769 |
| * | | 12.1 | 607 | 692 |
| | *** | 22.2 | 437 | 673 |
| * | 22 | 22.2 | 457 | |
| 2 | 2 | 22.2 | | 55 |
| 16 | 2 | | # | 676 |
| | 1 | 7-79 | 442 | 678 |
| | | 22.2 | 361 | ** |
| 17 | 8.6 | 22.2 | 36 | |
| 33 | PISA | 22.2 | | |
| • | 874 | | | 436 |
| | | 7:77 | 346 | 687 |
| | | | | |

Table 3.4.2c: YIELD STRESSES AND TENSILE STRENGTHS OF DIAGONALS

| | AVERAGE MEASURED YIELD STRESS AVERAGE MEASURED TENSILE STRENGTH | (# GP) | 067 | 810 |
|-----------------------------------|---|----------------|-----|--------|
| D SPECIMENS) | AVERAGE MEASURED YIELD STRESS (MPs) | | 328 | 384 |
| (6-PANEL SINGLE-BRACED SPECIMENS) | DIAMETER OF DAGONAL (mm) | ä | | 23.6 |
| | SPECIMEN I.D. | 315RB | | Divers |
| | TEST SERIAL NO. | ** | \$ | |

CHAPTER 4

ANALYSIS OF RESULTS

4.1 Failure Pattern of Tower Members

4.1.1 Cross-Braced Specimens

Thirty-one cross-braced specimens were tested in this investigation; fifteen of the specimens were with horizontals while the others were without horizontals. For the specimens with horizontals, the left-most panel was tested with all other panels reinforced and it was observed that the tested compression diagonals had buckled out-of-plane with an almost S-shape or an unsymmetrical S-shape. For the specimens without horizontals, left middle panel was strain-gauged while all other panels were reinforced. The tested diagonals had buckled with one half-sine wave failure shape due to very small tensile force in the tensile diagonals. (The failure pattern of all the compression diagonals are given in Table 4.1.1).

4.1. 2 Single-Braced Specimens

Two single-braced towers 31SRB and 33SRC were tested during the investigation. For tower 31SRB, the top leg of right middle panel buckled first due to the small leg-diagonal size ratio and no diagonals buckled. For tower 33SRC with a large leg-diagonal size ratio, two of the tested diagonals buckled out-of-plane almost at the same time with a one half sine wave shape.

4. 2 Calculation of Axial Forces in Tested Members

The finite strip method was used to determine the axial forces, assuming a linear variation of strain across the cross-section. The cross-section of each tested member was divided into 1000 strips, and the axial force in each strip was determined from the strain in the strip.

Table 4.1.1: FAILURE PATTERN OF ALL BUCKLED COMPRESSION DIAGONALS

| L | | L | | | | | | • |
|------------|------------------|--|------------------------------------|------------|------------------|---|------------------------|---|
| 2 8 | Specimen I.D. | Location of Buckled Diagonal | Failure Pattern | 2 8 | Specimen I.D. | Location of Buckled Diagonal | Failure Pattern | |
| 9 | S1A | | half-sine inside | 22 | P1A | test panel did not buckle; panel H buckled first | panel H buckled first | |
| | | parrei C Tear Diagoriai | ON THU DUCKIE | | | | | |
| 4 | S2A | panel A front diagonal | s-shape top half outside | 7 | 810 | panel A front diagonal | bottom half outside | |
| | | panel A rear diagonal | s-shape bottom half inside | | | panel A rear diagonal | top half inside | |
| α | 828 | panel A front diagonal | s-shape top half inside | 24 | 024 | panel A front diagonal | did not buckle | |
| <u>.</u> | 2 | panel A rear diagonal | s-shape bottom half outside | - | 5 | panel A rear diagonal | top half outside | |
| 23 | 200 | panel A front diagonal | s-shape top half inside | 27 | aca | panel D front diagonal | top half outside | |
| <u>:</u> | 250 | panel A rear diagonal | s-shape top half inside | 7. | 120 | panel D rear diagonal | top half outside | |
| , | A12 | panel C front diagonal | top half outside | 30 | AEG | panel A front diagonal | top half inside | |
| • | | panel C rear diagonal | bottom half inside | 3 | ا ا | panel A rear diagonal | bottom half outside | |
| 25 | S3B | panel A front diagonal | s-shape top half outside | 32 | 920 | panel A front diagonal | top half inside | |
| 3 | 999 | panel A rear diagonal | s-shape top half inside | 35 | LOD | panel A rear diagonal | bottom half outside | |
| • | 644 | panel A front diagonal | s-shape top half inside | 30 | DAA | panel D front diagonal | not buckle | |
| - | | panel B front diagonal | s-shape top half inside | 22 | V | panel D rear diagonal | top half inside | |
| ۳. | S4B | panel A front diagonal | s-shape top half inside | 20 | 979 | panel D front diagonal | top half inside | |
| , | | panel A rear diagonal | s-shape bottom half inside | در | | panel D rear diagonal | top half outside | |
| ζ. | 273 | panel A front diagonal | s-shape top half inside | 96 | DEA | altoin to his lange toot | of bushle | |
| , | | panel A rear diagonal | s-shape bottom half inside | 60 | 5 | ופפו הפונים חום ו | ioi bucare | |
| 2 | S5A | panel C front(rear) diagonal | half-sine outside(inside) | 25 | PSB | panel A front diagonal | did not buckle | |
| | | panel D front(rear) diagonal | half-sine outside(inside) | 5 | 20. | panel A rear diagonal | top half inside | |
| <u></u> | S.58 | panel C front diagonal | half-sine outside(inside) | 28 | DRA | panel D front diagonal | half-sine inside | |
| 2 | 200 | | did not buckle | 20 | 5 | panel D rear diagonal | half-sine outside | |
| 2 | SSC | front diagor | haff-sine inside | 15 | BAR | panel D front diagonal | did not buckle | |
| | | rear diagon | half-sine outside | : | | panel D rear diagonal | top half inside | |
| 11 | S6A | | s-shape top half inside | ξ. | D7.4 | panel C diagonalf did not buckle; panel D top leg | uckle; panel D top leg | |
| : | | panel A rear diagonal | s-shape bottom half inside | 2 | | buckled first | lirst | |
| 13 | S6B | panel A front diagonal | s-shape top half inside | 17 | PZR | panel A diagonal did not buckle; panel E top leg | uckle; panel E top leg | |
| 2 | | | s-shape bottom half inside | : | 2 | buckled | first | |
| 24 | Sec | | panels C and D buckled first after | 33 | PAA | panel D front diagonal | top half outside | |
| | | the horizon | orizontal buckled | 3 | 3 | panel D rear diagonal | did not buckle | |
| <u>‡</u> | 31SRB | no digonal buckled due to the right middle panel top leg | ie right middle panel top leg | 19 | P88 | | top half inside | |
| | | | guill | | | panel D rear diagonal | did not buckle | |
| 9 | 33SRC | | half-sine out-of-plane | | | | | |
| | | panel c rear diagonal | • | 7 | 1 | 1 | | |

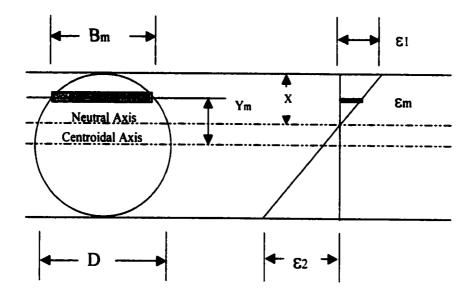


Figure 4.2.1. Diagram of Axial Force Calculation from Strains

The detailed calculation procedure is as follows:

Case 1: Strains at Top and Bottom are of Opposite Sign (Fig. 4.2.1)

The distance Y_m measured from the center of slice to centroidal axis of the cross-section is:

$$Ym = \frac{D}{2} - (m-1)dy - \frac{dy}{2}$$
 (4.1)

where dy = D/1000, and m = 1 to 1000 (from top to bottom)

The width of slice "m" is given by

$$B_m = 2\sqrt{(\frac{D}{2})^2 - (Y_m)^2}$$
 (4.2)

The depth of neutral axis X measured from the strain ε_1 is calculated as:

$$X = \frac{\left|\varepsilon_{\perp}\right|D}{\left|\varepsilon_{\perp}\right| + \left|\varepsilon_{\perp}\right|} \tag{4.3}$$

The strain ε_m in the center of slice "m" is given by

$$\varepsilon_{m} = \frac{\varepsilon_{1}}{X} \left[Y_{m} - \left(\frac{D}{2} - X \right) \right] \tag{4.4}$$

The stress for slice "m" is calculated according to Hooke's law:

$$\sigma_m = \varepsilon_m E \tag{4.5}$$

The actual force in slice "m" is

$$\text{If} \quad \sigma_m < F_y \qquad \qquad \text{then} \; \; F_m = \sigma_m \; B_m \; dy \qquad \qquad (4.6)$$

If
$$\sigma_m > F_y$$
 then $F_m = F_y B_m dy$ (4.7)

The axial force in the total cross-section of the member is the sum of all the slice forces:

$$F = \sum F_m \tag{4.8}$$

Case 2: Strains at the Top and Bottom are of Same Sign (Figure 4.2.2)

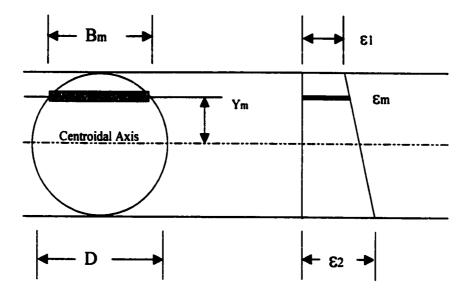


Figure 4.2.2. Diagram of Axial Force Calculation from Strains

The distance Y_m measured from the center of slice to centroidal axis of the cross-section is:

$$Y_{m} = \frac{D}{2} - (m-1)dy - \frac{dy}{2}$$
 (4.9)

where dy = D/1000, and m = 1 to 1000 (from top to bottom)

The width of slice "m" is given by

$$B_m = 2\sqrt{\left(\frac{D}{2}\right)^2 - \left(Y_m\right)^2} \tag{4.10}$$

The strain ε_m in the center of slice "m" is given by

$$\varepsilon_{m} = \frac{D(\varepsilon_{1} + \varepsilon_{2}) - 2Y_{m}(\varepsilon_{2} - \varepsilon_{1})}{2D} \tag{4.11}$$

The stress for slice "m" is calculated according to Hooke's law:

$$\sigma_m = \varepsilon_m E \tag{4.12}$$

The actual force in slice "m" is

$$\text{if} \quad \sigma_m < F_y \qquad \qquad \text{then} \;\; F_m = \sigma_m \; B_m \; dy \qquad \qquad (4.13)$$

$$\text{If} \quad \sigma_m > F_y \qquad \qquad \text{then} \; \; F_m = \; F_y \; B_m \; dy \qquad \qquad (4.14)$$

The axial force in the total cross-section of the member is the sum of all the slice forces:

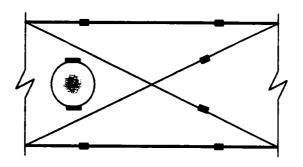
$$F = \sum_{m} F_{m} \tag{4.15}$$

4.3 Specimen Equilibrium Check

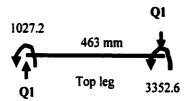
Accuracy of the axial forces based on the strain readings was verified with the tower's equilibrium check. In this investigation, a vertical equilibrium check was conducted on one tower (S5C) by calculating the axial forces and shears in the tension and compression diagonals and the shear forces in the three legs at one cross-section. The location of strain gauges are given in Appendix A. The equilibrium was checked as shown below:

Specimen S5C equilibrium check (applied load level 106 kN):

1) Diagram for strain gauge location (front-view)



2) Shear forces in three legs (from Table S5C of Appendix B)



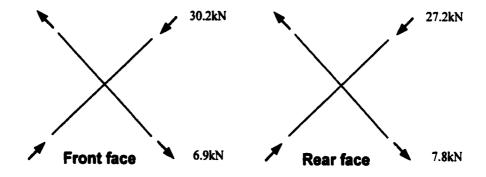
$$Q1 = (3352.6 + 1027.2)/463 = 9.46 \text{ kN}$$

$$Q2 = (649.1 + 388.1)/463 = 2.24 \text{ kN}$$

$$Q3 = (459.2 + 368.1)/463 = 1.79 \text{ kN}$$

$$Q_{leg} = Q1+Q2+Q3 = 9.46-2.24-1.79 = 5.43 \text{ kN}$$

3) Vertical component of axial forces in diagonals (from Table S5C of Appendix B)



$$Q_{diagonal} = (30.2+6.9+27.2+7.8)*sin (41.71°) = 47.97 kN$$

- 4) Vertical component of shear forces in diagonals (ignored)
- 5) Total shear force in the cross-section

$$Q_{total} = Q_{leg} + Q_{diagonal} = 5.43+47.97=53.40 \text{ kN}$$

6) Support reaction

$$R = Load Level/2 = 106.0/2 = 53.0 kN$$

7) Error

Error =
$$(Q_{total} - R)/R = (53.4-53.0)/53.0 = 0.75\%$$
.

4.4 Determination of Experimental Buckling Loads and Effective Length Factors

The buckled diagonals were noted during each tower test. The maximum axial force that occurred in the tested diagonal was taken as the buckling load. Only for specimen S5A, there was a large variation in the buckling loads of the front and rear diagonals (38.9 kN and 21.6 kN). This is probably due to the possibility of the strain gauges not being located diametrically opposite to each other on one of the diagonals. In this investigation, a total of 44 buckling loads were used and the corresponding effective length factors based on CSA-S37-94 Standard and AISC-LRFD Specifications were calculated, The details of the buckling loads and effective length factors are shown in Tables 4.4a to 4.4g.

The leg member of specimen 31SRB failed before any diagonal failed. The maximum axial compressive force recorded in the diagonals was 51.6 kN. This corresponds to an effective length factor of 0.64 according to CSA-S37-94 and 0.71 according to AISC-LRFD. Though it is not possible to determine the actual effective length factors of diagonal members based on this test, it can be stated that they will be less than the above values.

4.5 Effect of Axial Forces in Tension Diagonals on Effective Length Factors

Examining Tables 4.4a to 4.4f, it can be seen that although the ratio of forces in the compression diagonal and tension diagonal varied significantly, the effective length factors varied from a minimum of 0.296 to a maximum of 0.403. There is no definite relationship between the force in the tension diagonal and the resistance of the compression diagonal. The tension diagonals of the middle panels of specimens with no horizontals carried very little tensile forces. Still they were able to provide the necessary support to the compression diagonal. It can therefore be stated that even a small tensile force is able to provide the necessary support to the compression diagonal.

Table 4.4a: EFFECTIVE LENGTH FACTORS USING CAN/CSA-S16.1-94

| | | | d-9) | (6-panel cross-braced specimens) | aced specir | nens) | | | |
|------------|------------------|---------------------------|--------------------------------|-----------------------------------|-----------------------|--------------------------------------|-------------------------------|-------|------------------------------|
| 2 5 | Specimen I.D. | Diegonal Diameter (mm) | c/c Length of Diag. Ld (mm) | Measured Yield Stress Fy (MPs) | Buckling Load (kN) | Force in the Teslon Diagonal (kN) | Compression/T ension Ratio | γ | Effective Length Factor K |
| • | S1A | 12.7 | 1190 | 357 | 14.1 | 2.6 | 5.42 | 1.640 | 0.325 |
| | | | | | 12.4 | 3.3 | 3.76 | 1.778 | 0.352 |
| • | STB | 12.7 | 1190 | 396 | Did not buckle | | | | |
| _ | • 65 | | | | | | | | |
| • | 500 | 12.7 | 1180 | 378 | 24.8 | 15.0 | 0.80 | 1.649 | 0.318 |
| • | 100 | | | | 14.3 | 16.0 | 0.89 | 1.685 | 0.325 |
| • | 970 | 12.7 | 1100 | 696 | 13.7 | 13.6 | 1.01 | 1.706 | 0.333 |
| ŝ | 38 | | | | 13.7 | 13.4 | 1.02 | 1.706 | 0.333 |
| 2 | 35 | 12.7 | 1180 | 353 | 14.5 | 16.6 | 0.87 | 1.598 | 0.319 |
| • | 3 | | | | 14.8 | 14.0 | 1.06 | 1.578 | 0.315 |
| • | 50 | - T-3 | 1190 | 388 | 21.3 | 4.6 | 4.63 | 1.537 | 0.331 |
| " | ٤ | | | | 19.4 | | | 1.633 | 0.351 |
| Q — | 920 | 14.3 | 1190 | 386 | 28. | 9.1 | 2.52 | 1.617 | 0.342 |
| Ŀ | | | | | 20.1 | 4.6 | 4.37 | 1.633 | 0.345 |
| _ | ≸ | 14.3 | 1190 | 376 | 2 | 16.9 | 1.19 | 1.578 | 0.343 |
| ľ | 3 | | | | | | | | |
| າ | 3 | F. 9 | 1180 | 378 | 24.9 | | | 1.365 | 0.296 |
| • | 973 | | | | | | | | |
| 9 | ر ا | 4.3 | 150 | 287 | 21.4 | 19.3 | 1.11 | 1.485 | 0.327 |
| , | | | | | 22.8 | 22.0 | 1.04 | 1.422 | 0.313 |
| N | ₹ co | 15.9 | 1180 | 385 | 21.6 | 1.9 | 11.37 | 1.741 | 0.416 |
| , | 5 | | | | 50.6 | 8.1 | 2.58 | 1.778 | 0.424 |
| 2 | ace | 9.0 | 1190 | 385 | 33.2 | 10.4 | 3.19 | 1.306 | 0.312 |
| 12 | Sec | 15.9 | 1190 | 384 | 29.0 | 6.9 | 4.30 | 4430 | 0.242 |
| | | | | | 30.2 | 8.6 | 3.08 | 1 300 | 23.5 |
| - - | ≤ | 15.0 | 1190 | 385 | 27.3 | 23.9 | 1.14 | 1.498 | 0.358 |
| | | | | | 29.2 | 13.8 | 2.12 | 1.431 | 0.342 |
| 2 | 99% | 15.0 | 1180 | 382 | 25.4 | 17.3 | 1.47 | 1563 | 0.375 |
| | | | | | | | | | |
| 2 | 280 | 15.0 | 1190 | 385 | Did not buckle | | | | |
| | | | | | | | | | |
| | | | | _i_ | | | | | |
| | | | | | | | | | |

Table 4.4b: EFFECTIVE LENGTH FACTORS USING CAN/CSA-S16.1-94

Table 4.4c: EFFECTIVE LENGTH FACTORS USING CAN/CSA-S16.1-94

| | | | (6-panel si | (6-panel single-braced specimens) | nens) | | |
|-----|------------------|--|-----------------------------------|--|-----------------------|------|------------------------------|
| - 1 | Specimen 1.D. | Test No. Specimen Diagonal Diameter (mm) | c/c Length of Diegonal Ld (mm) | c/c Length of Diagonal Messured Yield Stress Fy Buckling Load (kN) | Buckling Load (KN) | γ | Effective Length Factor K |
| | 31SRB | 22.2 | 480 | 328 | | | |
| ŀ | | | | | | | |
| | 33SRC | 28.6 | 976 | 798 | 148.6 | 0.93 | 0.502 |
| ı | | | | | 150.5 | 0.92 | 0.495 |

Table 4.4d: EFFECTIVE LENGTH FACTORS USING AISC-LRFD SPECIFICATIONS

| į | | | F-9) | (6-panel cross-braced specimens) | raced speci | mens) | | | |
|----------|------------------|---------------------------|-----------------------------------|-----------------------------------|-----------------------|--------------------------------------|-------------------------------|-------|------------------------------|
| Test No. | Specimen 1.D. | Diagonal Diameter (mm) | c/c Length of Diagonal Ld (mm) | Measured Yield Stress Fy (MPs) | Buckling Load (kN) | Force in the Tesion Diagonal (kN) | Compression/T ension Ratio | γ | Effective Length Factor K |
| • | SIA | 12.7 | 1190 | 357 | 14.1 | 2.6 | 5.42 | 1.677 | 0.325 |
| | | | | | 12.4 | 3.3 | 3.76 | 1.788 | 0.352 |
| <u> </u> | SIB | 127 | 0011 | 304 | Did not buckle | | | | |
| | | | | 222 | | | | | |
| - | ACS. | 164 | 1100 | 378 | 14.8 | 15.0 | 88.0 | 1.684 | 0.318 |
| | 5 | | | 310 | 14.3 | 16.0 | 0.89 | 1.713 | 0.325 |
| • | SZB | 12.7 | 1190 | 340 | 13.7 | 13.6 | 1.01 | 1.731 | 0.333 |
| ١ | | | | 3 | 13.7 | 13.4 | 1.02 | 1.731 | 0.333 |
| 23 | SSC | 12.7 | 1180 | 353 | 14.5 | 16.6 | 0.87 | 1.643 | 0.319 |
| | | | | | 14.8 | 14.0 | 1.06 | 1.627 | 0.315 |
| _ | S3A | 14.3 | 1180 | 35 | 21.3 | 4.6 | 4.63 | 1.595 | 0.331 |
| | | | | | 19.4 | | | 1.671 | 0.351 |
| 25 | 838 | | 1190 | 308 | 20.4 | 8.1 | 2.52 | 1.658 | 0.342 |
| | | ï | | | 20.1 | 4.6 | 4.37 | 1.671 | 0.345 |
| - | SAA | 14.3 | 1190 | 378 | 20.1 | 16.9 | 1.19 | 1.627 | 0.343 |
| | | | | | | | | | |
| 6 | SAB | 14.3 | 1190 | 378 | 24.9 | | | 1.459 | 0.296 |
| | | | | | | | | | |
| 9 | SAC | 14.3 | 1180 | 367 | 21.4 | 19.3 | 1.11 | 1.554 | 0.327 |
| | | | | | 22.8 | 22.0 | 1.04 | 1.506 | 0.313 |
| 8 | SSA | 9.51 | 0811 | 385 | 21.6 | 1.9 | 11.37 | 1.759 | 0.416 |
| | | | | | 20.0 | 8.1 | 2.58 | 1.788 | 0.424 |
| 9 | SSB | 15.9 | 1190 | 385 | 33.2 | 10.4 | 3.19 | 1.409 | 0.312 |
| ! | | | | | Coc | 0 | ١ | | |
| 12 | သူ့ | 30.0 | 1190 | 382 | 200 | P. C | 200 | 1.010 | 0.043 |
| ; | | | | | 27.3 | 23.0 | 3 - | 199 | 2000 |
| | Š | 20.00 | 3 | <u>.</u> | 292 | 13.8 | 252 | 1 512 | 0.342 |
| | | | | | 25.4 | 47.3 | - | 700 | 27.6 |
| 2 | 900 | 15.6 | 961 | 382 | | | | 616.1 | 0.373 |
| , | 200 | | | | Did not buckle | | | | |
| • • | 300 | 15.8 | 0911 | 88 | | | | | |
| 14 | 31SRB | 22.2 | 240 | 328 | Did not buckle | | | | |
| : | | | 100 | 970 | | | | | |

Table 4.46: EFFECTIVE LENGTH FACTORS USING AISC-LRFD SPECIFICATIONS

| | | | | (8-panel cross-braced specimens) | -braced spec | imens) | | | |
|------------|------------------|---------------------------|-----------------------------------|-----------------------------------|-----------------------|--------------------------------------|-------------------------------|-------|------------------------------|
| Test No. | Specimen I.D. | Diagonal Diameter (mm) | c/c Length of Diagonal Ld (mm) | Messured Yield Stress Fy (MPs) | Buckling Load (kN) | Force in the Tesion Diagonal (kN) | Compression/Te naion Ratio | ٧ | Effective Length Factor K |
| 22 | P1A | 15.9 | 1158 | 363 | | | | | |
| 31 | PfB | 15.9 | 1158 | 375 | 26.3 | 27.6 | 0.95 | 1.574 | 0.375 |
| 21 | P2A | 15.9 | 1158 | 373 | 29.7 | 79 | 2 79 7 | 1474 | 375 |
| 27 | P28 | 15.9 | 1158 | 373 | 23.5 | 7.2 | 3.26 | 1.660 | 0.403 |
| 30 | P3A | 19.1 | 1158 | 407 | 55.0 | 44.6 | 1.23 | 1361 | 0.351 |
| 32 | P38 | 19.1 | 1158 | 400 | 60.0 | 53.2 | 1.13 | 1.305 | 0.327 |
| 5 0 | P4A | 19.1 | 1158 | 410 | 48.7 | 7.0 | 98.9 | \$45 | 385 |
| 20 | P48 | 19.1 | 1150 | 409 | 51.5 | 11.9 | 4.33 | 1.397 | 0.369 |
| 8 | PSA | 22.2 | 1156 | 437 | | | | | |
| * | P5B | 22.2 | 1158 | 437 | 88.2 | 89.6 | 88.0 | 1 250 | 28.0 |
| 28 | PeA | 22.2 | 1158 | 442 | 91.3 | 21.4 | 4.27 | 1.226 | 0.356 |
| 15 | P68 | 22.2 | 1158 | 442 | 101.5 | 12.7 | 7 96 | 1118 | 0.323 |
| 18 | ∀24 | 22.2 | 1158 | 351 | | | | | |
| 44 | 8/d | 22.2 | 1158 | 343 | | | | | |
| 33 | PBA | 22.2 | 1158 | 346 | 75.4 | 12.5 | 6.03 | 1.172 | 0.363 |
| 19 | P88 | 22.2 | 1158 | 349 | 82.0 | 19.6 | 4.18 | 1.093 | 0.355 |

Table 4.4f: EFFECTIVE LENGTH FACTORS USING AISC-LRFD SPECIFICATIONS

| | | | (6-panel | (6-panel single-braced specimens) | mens) | | |
|----------|---------------|--|----------|--|-----------------------|-------|------------------------------|
| Test No. | Specimen 1.D. | Test No. Specimen Diagonal Diameter (mm) | 8 | Length of Diagonal Messured Yield Stress Fy Buckling Load (MPa) (kN) | Buckling Load (kN) | γ | Effective Length Factor K |
| | | | | | Did not buckle | | |
| ‡ | 31SRB | 22.2 | 937 | 875 | | | |
| | | | | | 148.6 | 1.039 | 0.502 |
| \$ | 33SRC | 28.6 | 979 | 364 | 150.5 | 1.025 | 0.485 |

Table 4.4g: AVERAGE EFFECTIVE LENGTH FACTORS

| | Single-Braced Diagonal | | Cross-Braced Diagonal | nal |
|---|------------------------|---------|-----------------------|---------------|
| Effective Length Factor | | 6-Panel | 8-Panel | Average value |
| Effective Length Factor Using CAN/CSA -\$16.1-94 | 0.50 | 0.37 | 0.34 | 0.35 |
| Effective Length Factor Using AISC-LRFD | 0.56 | 0.39 | 0.35 | 0.37 |

CHAPTER 5

CONCLUSIONS AND RECOMMENDATIONS

5.1 Conclusions

The following conclusions are based on this experimental investigation:

The distribution of forces in compression and tension diagonals and the force distribution in top half and bottom half of the compression or tension diagonals are not the same. No definite conclusions about the force distribution can be drawn.

- For identical specimens of each type, the compression diagonals for the same panel would not have the same buckling load due to minor fabrication differences.
- Diagonals in the end panels of specimens with horizontals at mid-span buckle suddenly at a high load, while the specimens without horizontals at mid-span would buckle at the middle panels at a much smaller load.
- Specimens with small leg-diagonal size ratio buckle due to the buckling of top leg, not due to the buckling of compression diagonals in any panel.
- For cross-braced specimens without horizontals, the tested compression diagonals buckle out-of-plane inside or outside with one almost half-sine wave due to the small axial force in the tension diagonals. On the other hand, for cross-braced specimens with horizontals, the tested compression diagonals buckle out-of-plane inside or outside with a symmetrical S-shape or an unsymmetrical S-shape due to the large force in the tension diagonals. For single-braced specimens, the compression diagonals buckle out-of-plane with one half-sine wave.
- The axial forces in the tension diagonals don't have a big effect on effective length factors for cross-braced compression diagonals.

The average effective length factor for single-braced diagonals is 0.50. The
effective length factor for cross-braced diagonals is 0.35, as compared to an
effective length factor of 0.75 as given by CSA-S37-94 that is much too
conservative.

5.2 Recommendation for Further Research

- To know the distribution of forces in the members, tests should be carried out on towers with loads applied at each panel point (instead of one load at midspan of top chord as in the current investigation) to simulate the actual distributed wind load.
- Tests should be carried to study the effect of fabrication differences on the effective length factor.

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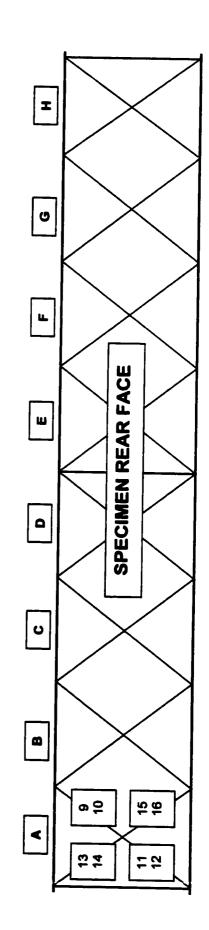
APPENDIX A

STRAIN GAUGE LOCATION

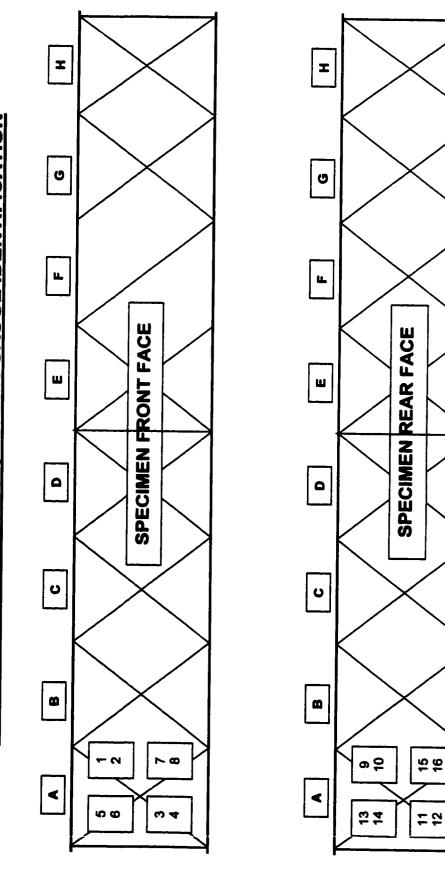
TABLE OF CONTENTS

| Specimen | | Page |
|----------|---|------|
| P1-A | | |
| P1-B | •••••• | וס |
| P2-A | | 02 |
| P2-B | ••••• | 63 |
| P3-A | •••••• | 64 |
| P3-B | •••••• | 65 |
| P4-A | ••••• | 66 |
| P4-B | •••••• | · 67 |
| P5-A | *************************************** | . 68 |
| P5-B | •••••• | 69 |
| P6-A | *************************************** | · 70 |
| P6-B | *************************************** | · 71 |
| P7-A | *************************************** | · 72 |
| P7-B | *************************************** | · 73 |
| P8-A | *************************************** | 74 |
| P8-B | *************************************** | 75 |
| S1-A | *************************************** | 76 |
| S2-A | *************************************** | 77 |
| S2-B | •••••• | 78 |
| S2-C | •••••• | 79 |
| S3-A | *************************************** | 80 |
| S3-B | *************************************** | 81 |
| S4-A | ••••• | 82 |
| S4-B | *************************************** | 83 |
| S4-C | *************************************** | 84 |
| S5-A | | 85 |
| S5-B | •••••• | 86 |
| S5-C | ••••••••••••••••••••••••••••••••••••••• | 87 |
| S6-A | •••••• | 88 |
| S6-B | | 89 |
| S6-C | *************************************** | 90 |
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| 33SRC93 | | |

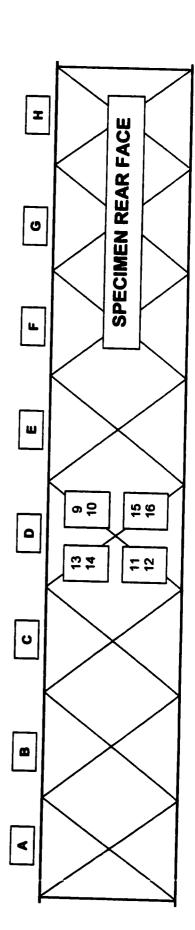
I SPECIMEN P1-A (TEST # 22) STRAIN GAUGE IDENTIFICATION O **L** SPECIMEN FRONT FACE ш ۵ ပ 0 ~ ∞ ⋖ မှ မ



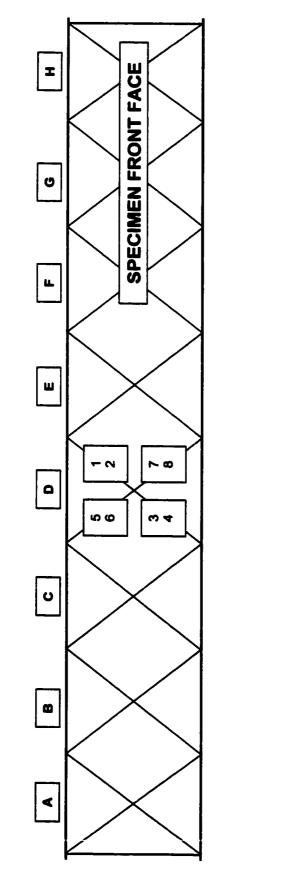
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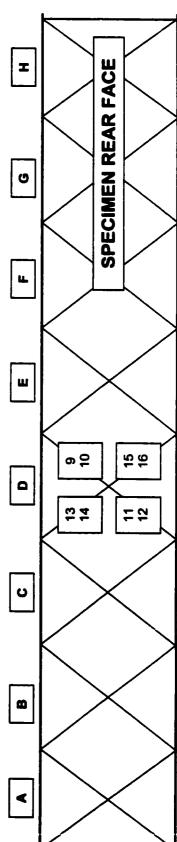


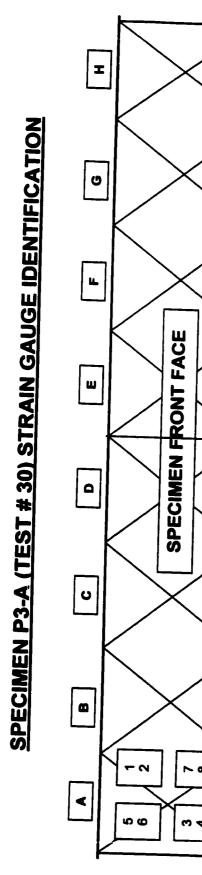
I SPECIMEN FRONT FACE SPECIMEN P2-A (TEST # 21) STRAIN GAUGE IDENTIFICATION Ø L Щ ~ @ Q ပ ပ ပ 0 ⋖

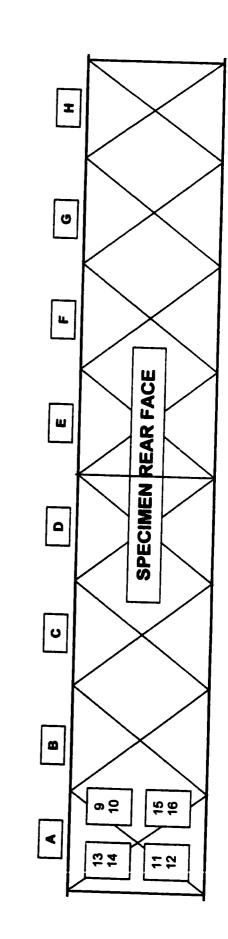


SPECIMEN P2-B (TEST # 27) STRAIN GAUGE IDENTIFICATION

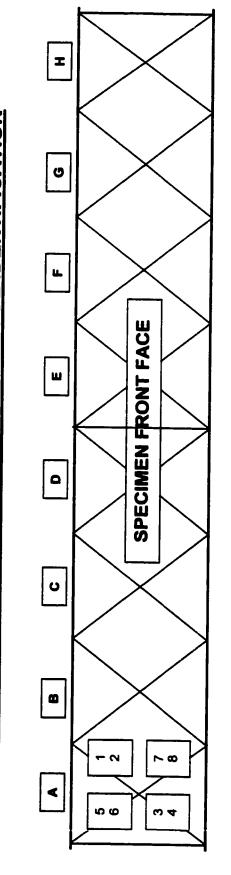


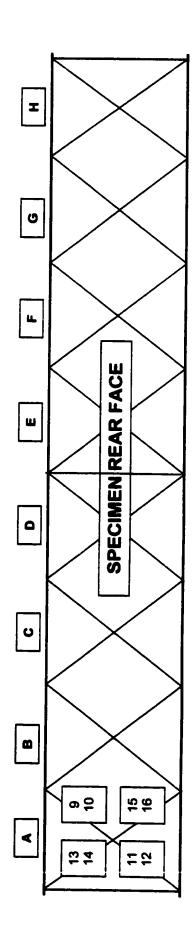




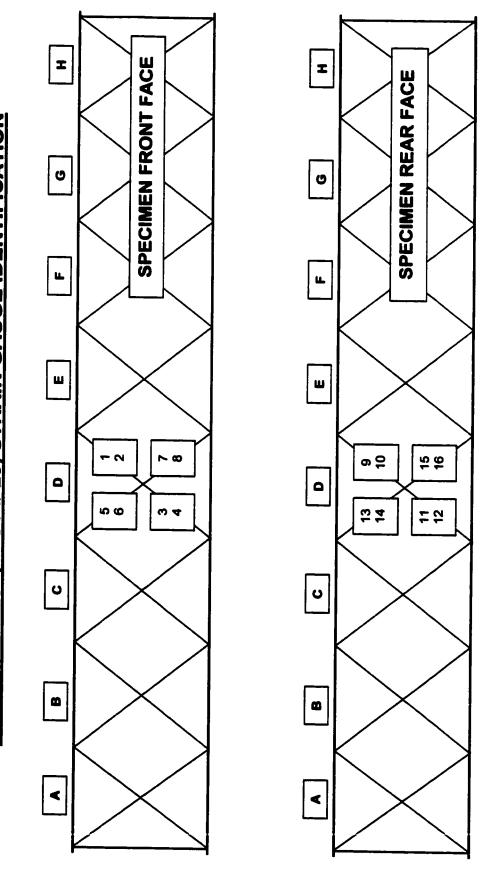


SPECIMEN P3-B (TEST # 32) STRAIN GAUGE IDENTIFICATION

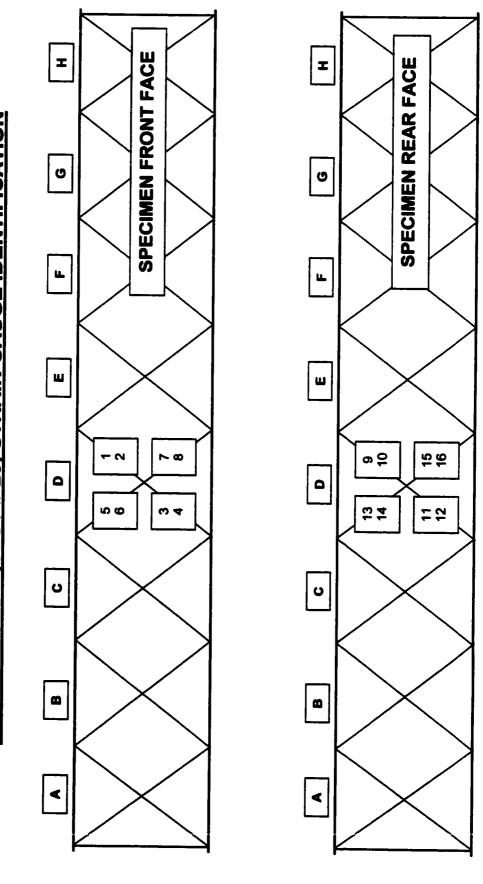


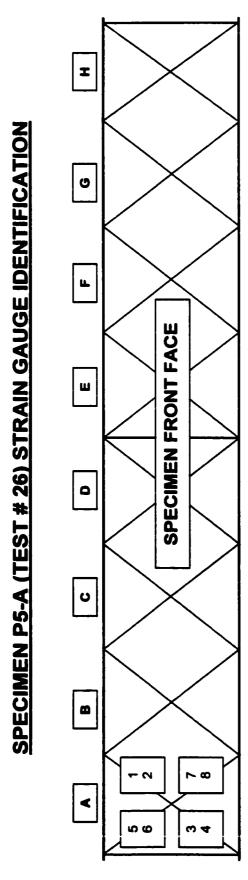


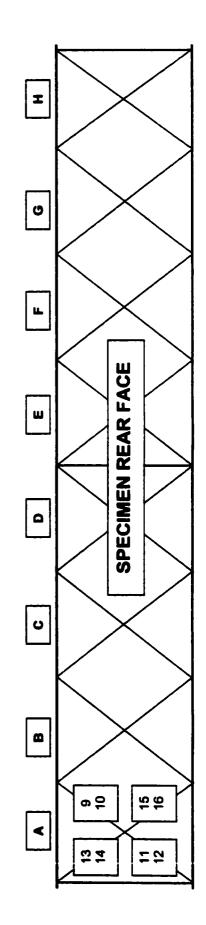
SPECIMEN P4-A (TEST # 29) STRAIN GAUGE IDENTIFICATION

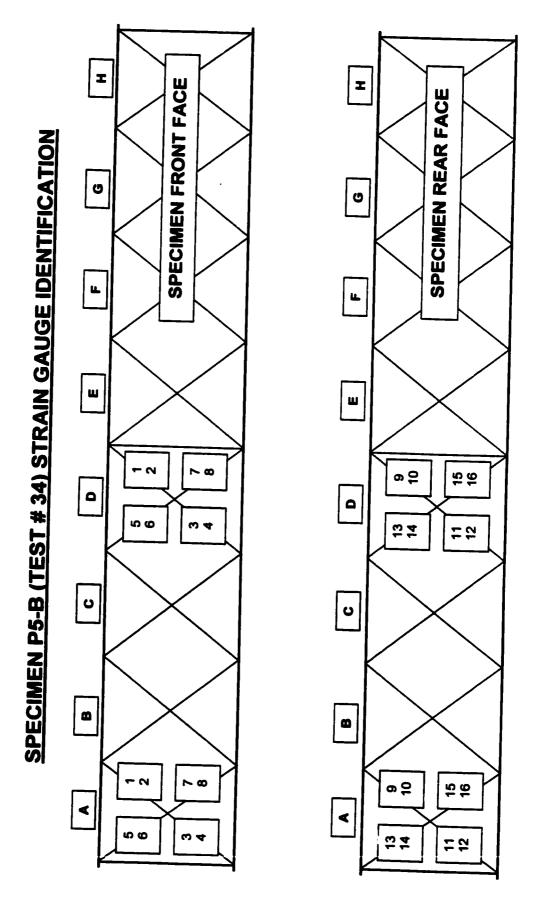


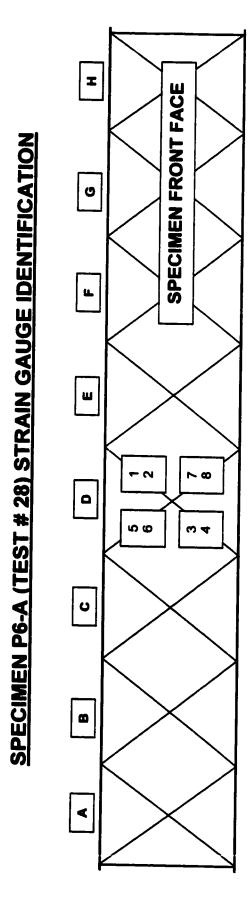
SPECIMEN P4-B (TEST # 20) STRAIN GAUGE IDENTIFICATION

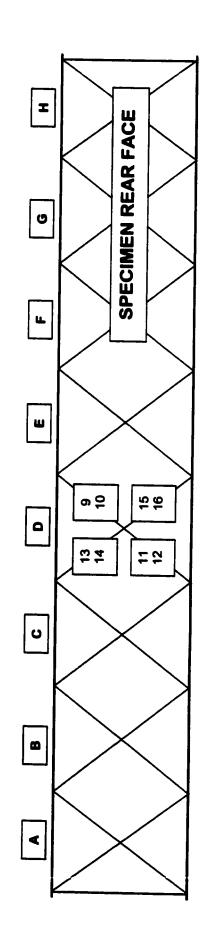




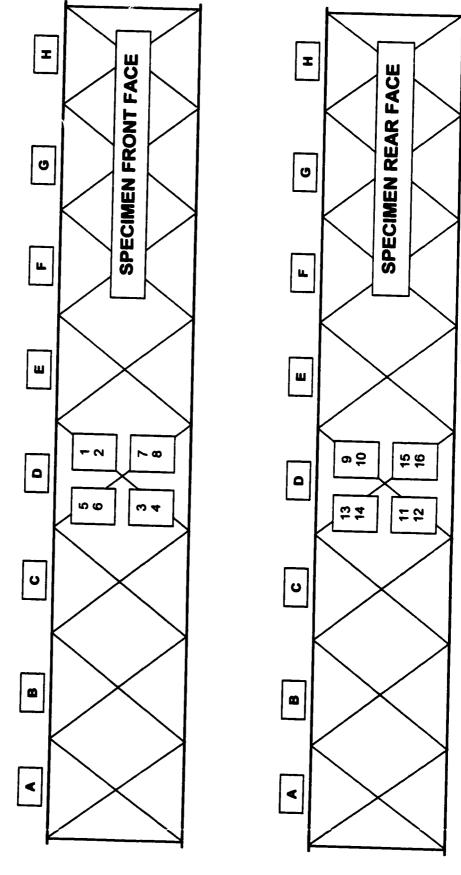


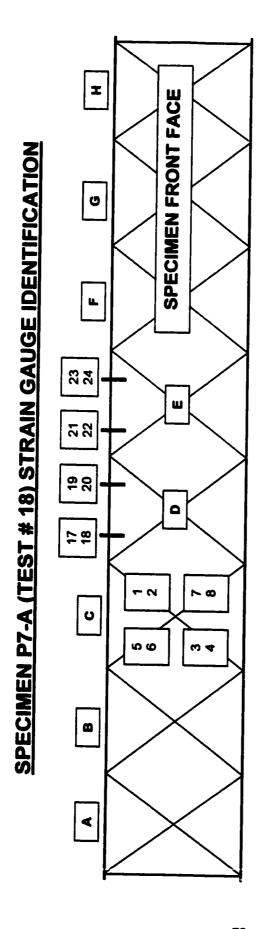


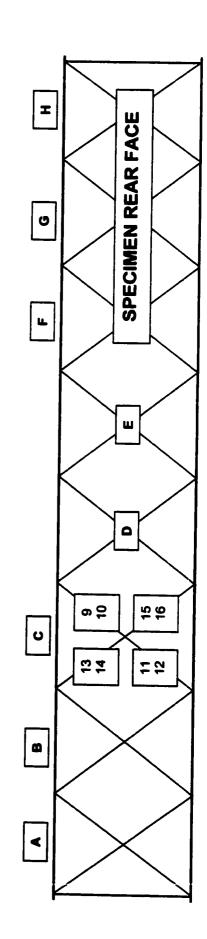


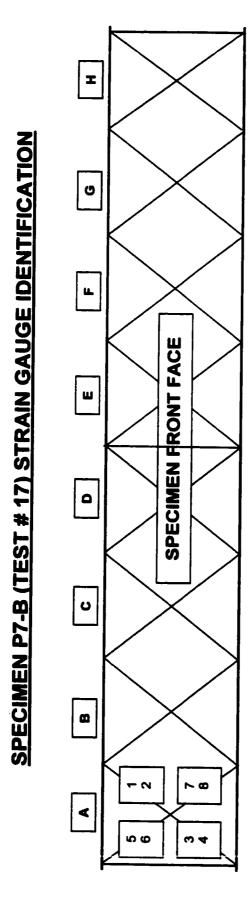


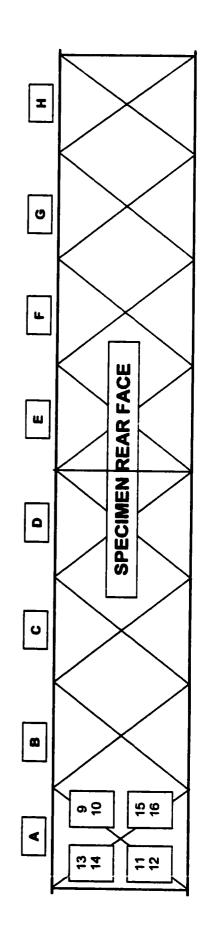
SPECIMEN P6-B (TEST # 15) STRAIN GAUGE IDENTIFICATION

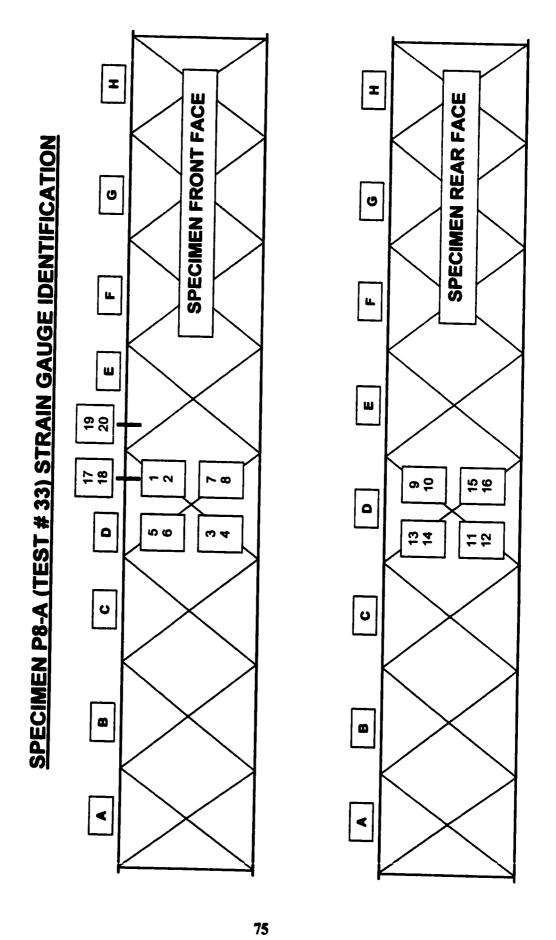


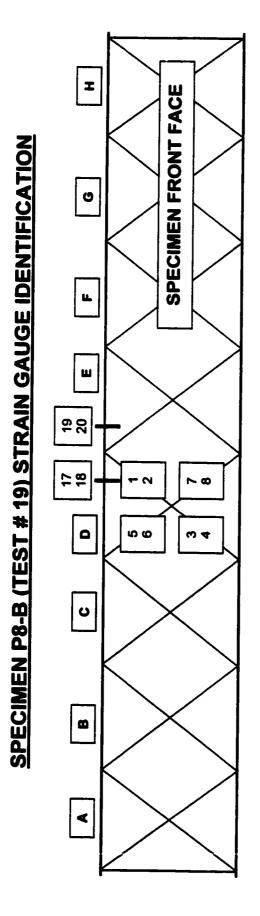


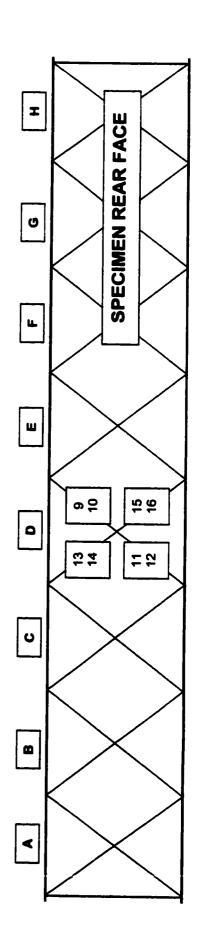


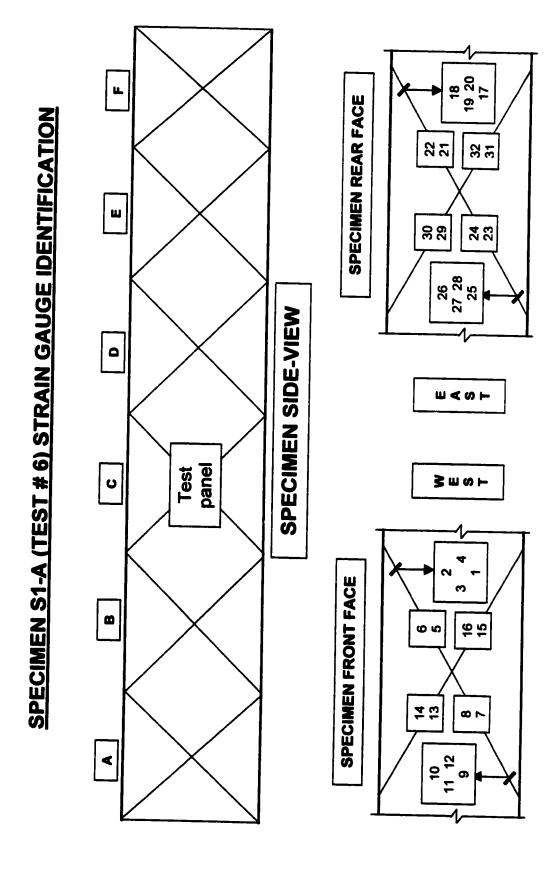








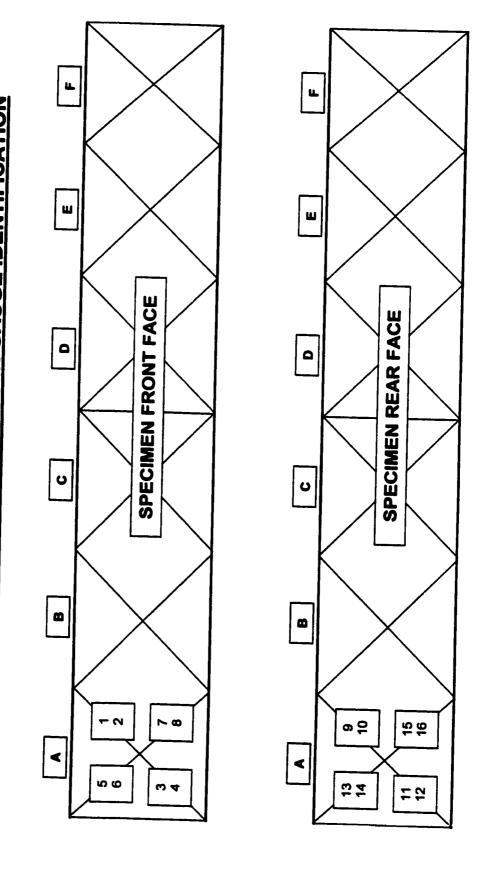




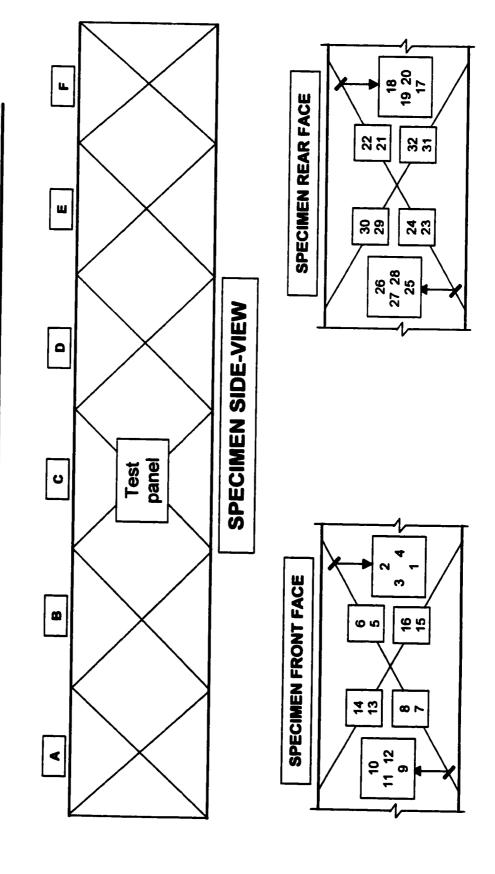
18 19 20 17 **L** SPECIMEN REAR FACE SPECIMEN S2-A (TEST # 4) STRAIN GAUGE IDENTIFICATION 22 32 ш 30 23 26 27 28 25 **SPECIMEN SIDE-VIEW** ۵ ပ SPECIMEN FRONT FACE 8 16 တ မာ <u>4</u> € 1 00 Test panel <

18 19 20 17 щ SPECIMEN REAR FACE SPECIMEN S2-B (TEST # 8) STRAIN GAUGE IDENTIFICATION 22 32 ш 30 24 23 26 27 28 25 **SPECIMEN SIDE-VIEW** 0 ပ SPECIMEN FRONT FACE 8 15 5 တ က **4€ &** r panel Test <

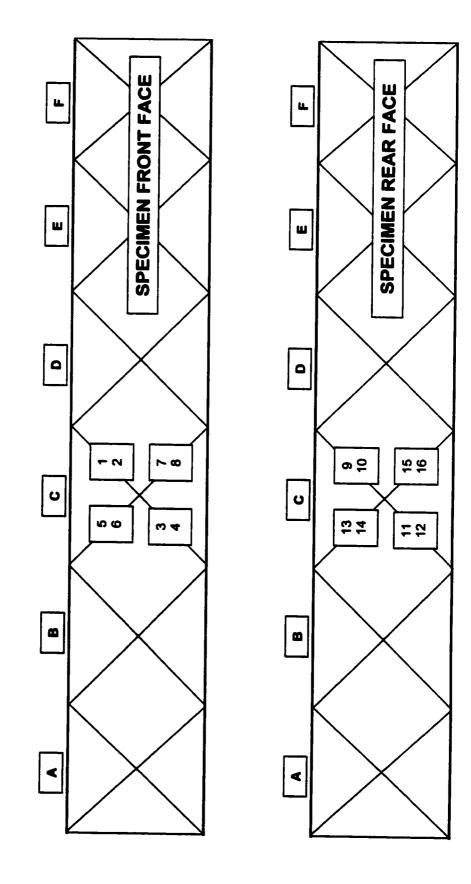
SPECIMEN S2-C (TEST # 23) STRAIN GAUGE IDENTIFICATION



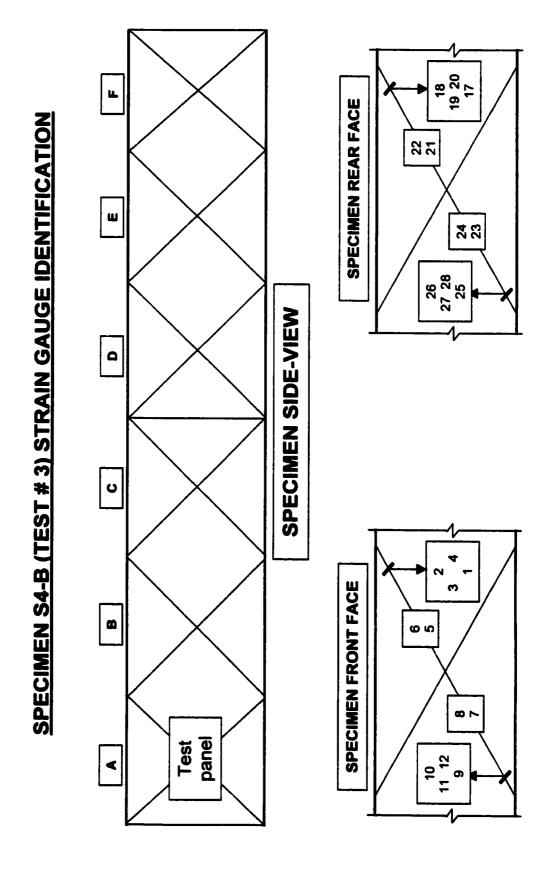
SPECIMEN S3-A (TEST # 7) STRAIN GAUGE IDENTIFICATION

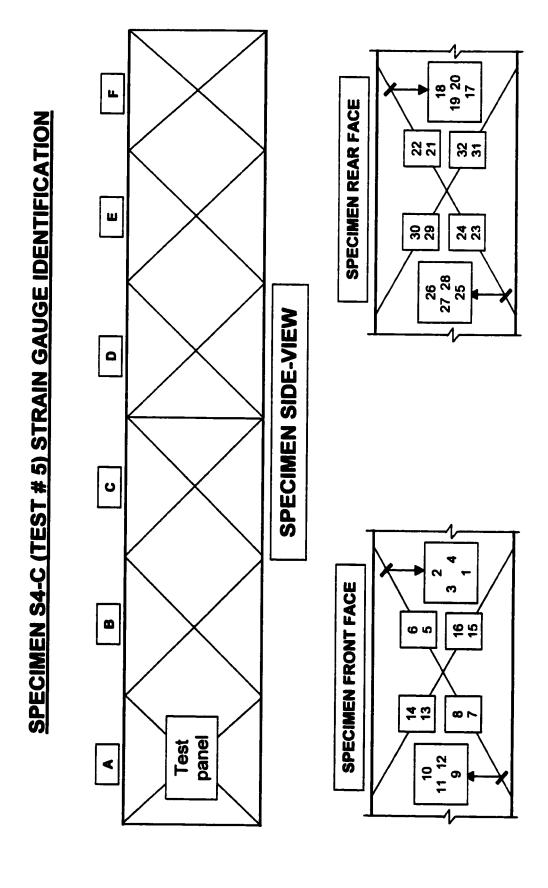


SPECIMEN S3-B (TEST # 25) STRAIN GAUGE IDENTIFICATION

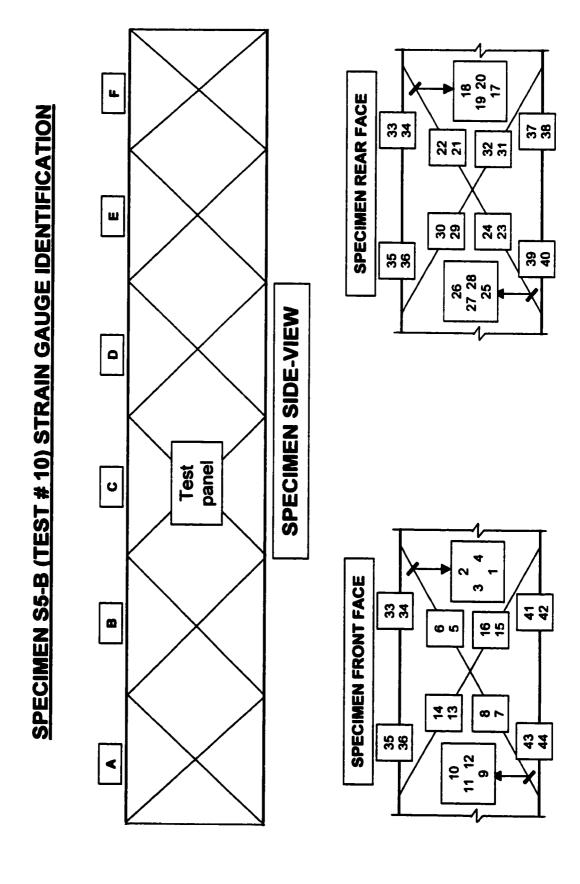


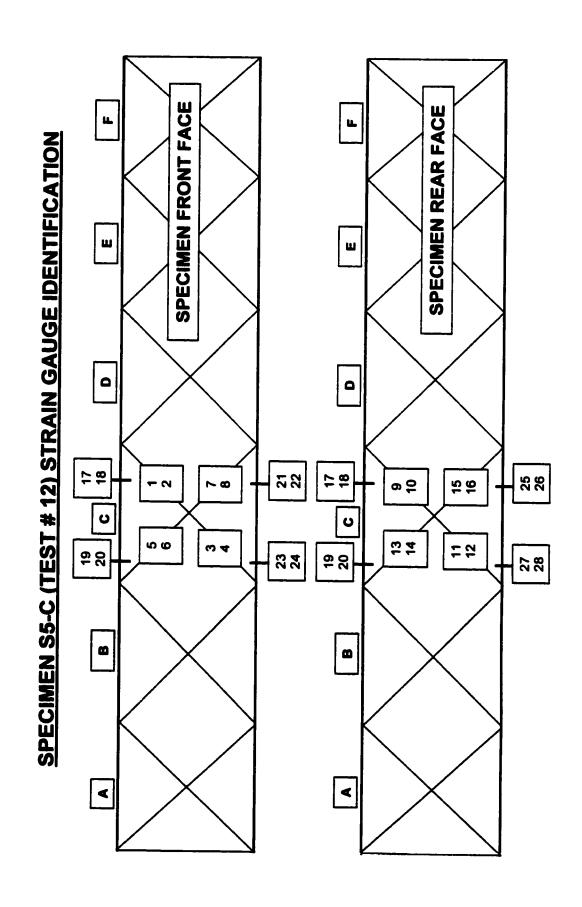
BOTTOM FACE FOR EACH PANEL test section **~** ∞ 5 e 4 5 5 4 ıL SPECIMEN S4-A (TEST # 1) STRAIN GAUGE IDENTIFICATION test section ш test section **SPECIMEN SIDE-VIEW** REAR FACE FOR EACH PANEL ۵ တ လ ~ 8 test section ပ test section FRONT FACE FOR EACH PANEL 8 17 18 2 9 13 test section ⋖

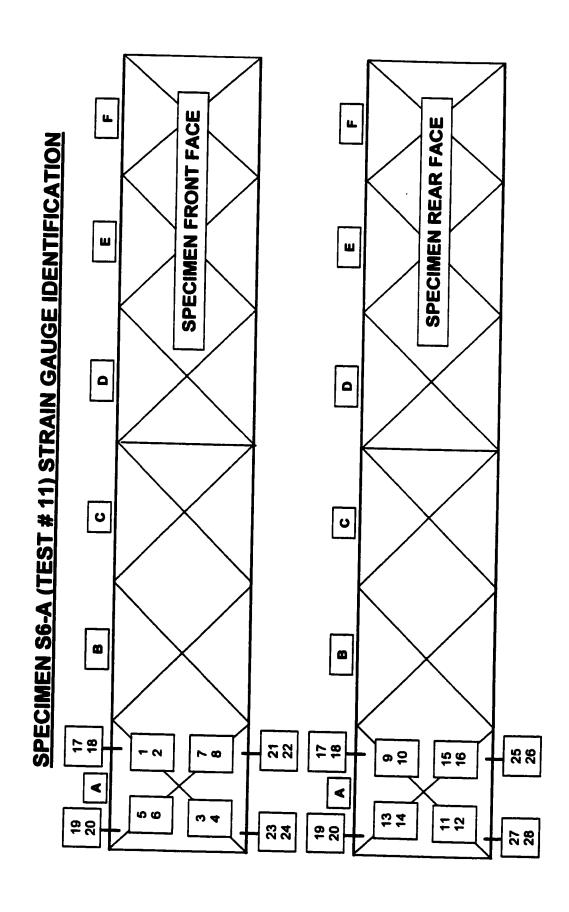


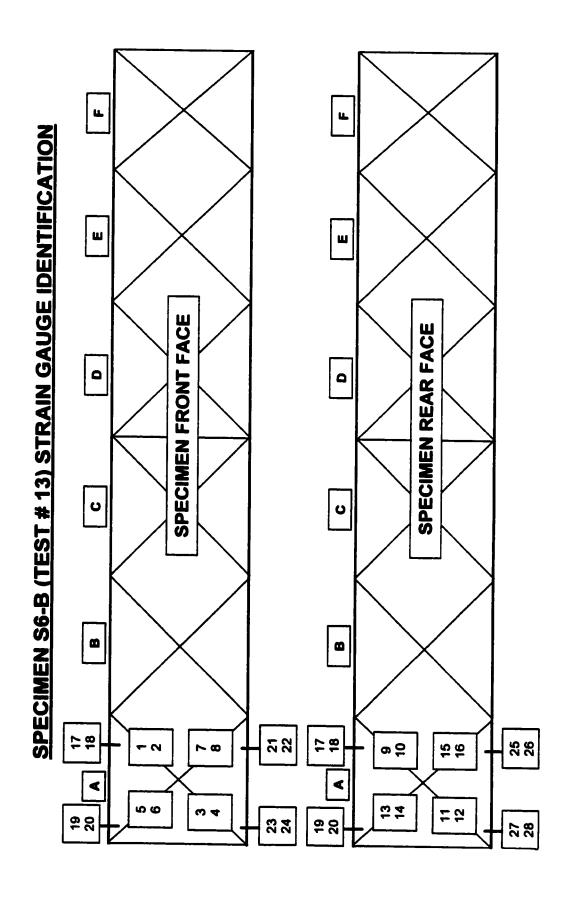


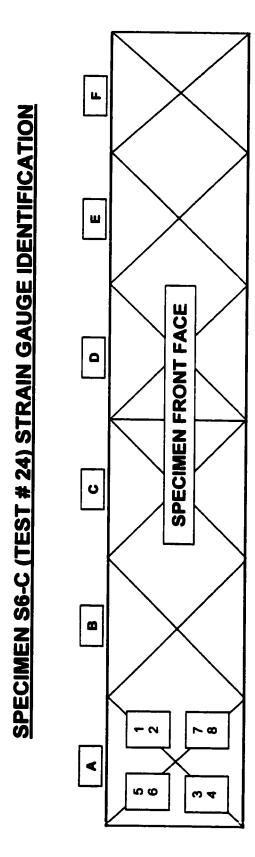
test section REAR FACE FOR EACH PANEL Ľ SPECIMEN S5-A (TEST # 2) STRAIN GAUGE IDENTIFICATION - 0 သ လ ~ @ test section ш test section **SPECIMEN SIDE-VIEW** ٥ test section v FRONT FACE FOR EACH PANEL test section 8 6 4 **⊕** 2 test section <

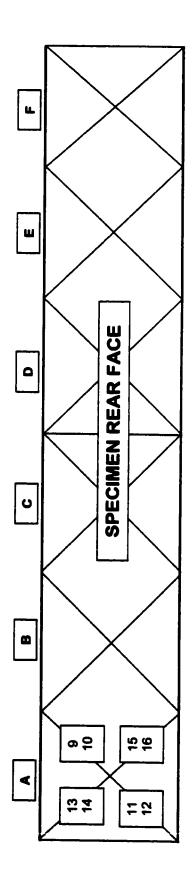




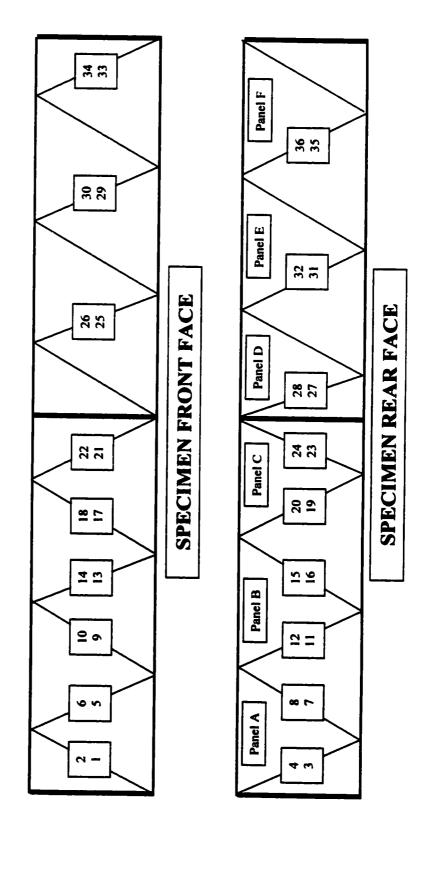




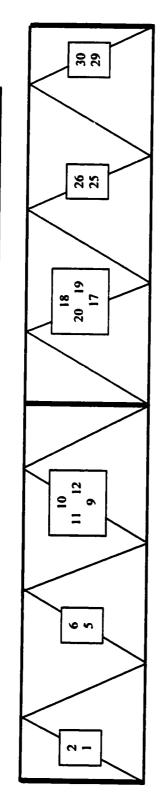




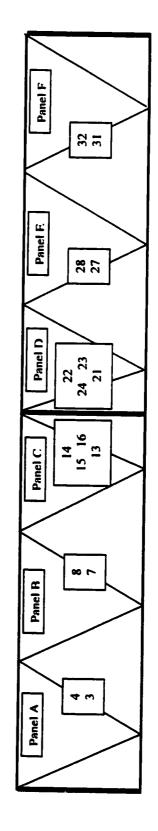
SPECIMEN 31SRB (TEST # 14) STRAIN GAUGE IDENTIFICATION



SPECIMEN 33SRC (TEST # 16) STRAIN GAUGE IDENTIFICATION



SPECIMEN FRONT FACE



SPECIMEN REAR FACE

APPENDIX B

LOAD-STRAIN DATA AND AXIAL FORCES

TABLE OF CONTENTS

| SPECIMEN | PAGE |
|----------|------|
| P1-A | |
| P1-B | 30 |
| P2-A | 90 |
| P2-B | 100 |
| P3-A | 102 |
| P3-B | 10- |
| P4-A | 100 |
| P4-B | 100 |
| P5-A | 110 |
| P5-B | 112 |
| P6-A | 110 |
| P6-B | 110 |
| P7-A | 120 |
| P7-B | 124 |
| P8-A | 120 |
| P8-B | 127 |
| S1-A | 150 |
| S2-A | 133 |
| S2-B | 130 |
| \$2-C | 139 |
| S3-A | 142 |
| S3-A | 144 |
| S3-B | 147 |
| S4-A | 149 |
| S4-B | 155 |
| S4-C | 159 |
| S5-A | 165 |
| S5-B | 171 |
| S5-C | 175 |
| S6-A | 178 |
| S6-B | 101 |
| S6-C | 194 |
| 31SRB | 196 |
| 33SRC | 189 |
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AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P1-A

| | T PANEL A (T | TEST PANEL A (TEST PANEL NOT BUCKL | | ed be cau se panel e buckled first.) | NCKLED FIRST. | (- | | Test | Test No. 22 |
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| • | -281 | -18 | 349 | | -274 | | 23 | | |
| 2 | 41.4 | | 272. | | | | | | |
| 3 | 995 | -24 | -514 | | 895 - | | | | 3 |
| 1 | 0.00 | | 329 | 11 | | | | | |
| S | 7.08- | Z. | 167. | 105 | | | | | |
| 9 | 980 | | 787 | | | | | 2 | |
| 2 | 1.69 | -19 | -643 | | | | | | |
| • | .102.3 | 71. | -625 | | | | | | |
| 9 | 2.701. | -15 | | | | | | | |
| 5 | 107.2 | -10 | 176- | | | | | | |
| 11 | 1142 | -15 | 1001 | | 1121- | | | | |
| 12 | 120.1 | -11 | -1088 | 249 | | | 21 | | |
| 13 | 120.5 | 11. | -1086 | 350 | | | | | |
| 14 | .127.0 | 01- | 1141 | | | | | | |
| 15 | 7.821. | • | -1100 | | | | 9 | | |
| 9 | .133.5 | 9 | 1195 | | 1483 | | 202 | | |
| 2 | .146.3 | .7 | 1200 | 443 | 9991- | 1112 | 822 | | |
| 65 | 152.0 | • | .1355 | 512 | -1812 | | 282 | | |
| 21 | | -4285 | 3124 | 18857 | 26715 | 965 | 95 | | |
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AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P1-A

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| | 1 -28.1 | 91- | , | | | | | | = | 7 |
| | 41.4 | 12. | | | | | | * | 202 | 8 |
| | 989 | | | | | 2/0 | 8 | 2 | 588 | 55 |
| | 0.00 | | | - | 2 | | | 8 | 407 | 2 |
| " | 504 | | | | | | | 118 | 460 | 97 |
| | | | | | | | 6 | 136 | 200 | 115 |
| | | | | | | | 2 | 148 | 613 | |
|] | | 46 | | 89. | | | • | 157 | 73 | - |
|] | | 8 | 288. | | | 9 665 | | Ē | 210 | 3 |
| 1 | | 22 | | 105 | | | | 20 | 75.5 | |
| 2 | | 52 | | | -860 | 769 | | 181 | 76.1 | |
| = | | 74 | | | | | _ | Ē | | <u> </u> |
| 2 | 120.7 | 8 | | 511. | | | | 2 2 | | 0/1 |
| 13 | 1205 | 100 | | | 198 | | | 3 2 | 1 | |
| 2 | .127.0 | 128 | | | | | | | 8 | 181 |
| 15 | 133.7 | 981 | | | | | | | 8 | 28 |
| 16 | -133.5 | 204 | | | | | | 127 | 88 | 902 |
| 16 | | 7 | | | | | | 238 | 9038 | × |
| 9 | | | | | | | | 245 | 1030 | 22 |
| 1 | | 210 | | | 1203 | 1017 | | 252 | 1076 | 24 |
| 1 | 28 | 21001 | -30280 | -2462 | 1622 | 200 | | 22 | 822 | 275 |
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| T | | | | | | | | | - | |
| 7 | | | | | | | | | - | |
| 3 | AXIAL FORCE (kN) | | | | | | | | | |
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AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P1-B

| 2 .367 3 .542 4 .657 5 .758 | • | | | | | | | |
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| | | | 2 | | | | | |
| | -18 | .237 | 7. | į | | • | - | • |
| | -21 | 38. | | | | 22 | 278 | -37 |
| | 2. | 1 | | | | 37 | 406 | \$ |
| | 2. | 202 | | | | 57 | 552 | 38. |
| | | PRO. | | | 534 | 74 | 2962 | 5 |
| | 3 | | 8 | 786 | 618 | 28 | 764 | 1 |
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| | 91. | -961 | 164 | • | 277 | 911 | 20 3 | ż |
| | 7. | -924 | | | - | 871 | 3 | કં |
| 1 201 | 1 | -824 | | | orno or | 8 | 200 | 7 |
| 11001. | -14 | 286- | | | 876 | 92 | 788 | 97 |
| 12 .1150 | 01. | 7801. | | | 653 | 151 | 1042 | 43 |
| 131148 | ę | , tm. | | | 986 | 2 | 1005 | 6 6. |
| 14 .120.9 | ē | 1001 | | | 200 | 163 | 1093 | 9 |
| 15 .127.4 | 9 | 200 | 8 | | 3 | 177 | 1144 | 85 |
| 6 221. | • | | | | Š | 180 | 1.96 | 8 |
| A. 00.1. | • | On the | | 1483 | 1027 | 202 | 1246 | 1 |
| | P | 1246 | 95 | 1506 | 1070 | 217 | 1207 | |
| | + | 887 | 3 | .1689 | 1112 | 228 | ar. | |
| | 1 | | | -1012 | 1148 | 232 | ğ | |
| | | 2 | 545 | -1873 | 1166 | 1 | | |
| 603 | 4285 | 3124 | 16657 | -26715 | 988 | 3 | | * |
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| AXIAL FORCE (KN) | -27.5 | | -26.3 | 6 | 27.7 | | 27.6 | |
| | - | | | | | | | _ |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P1-B

| Column C | | | | | - | | | | | | |
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| 1.00 | | | | | | | Strain. | 9train | | Sfrie | L |
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| 1.0 | | | | | | | | | | | 8 |
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| 10 10 10 10 10 10 10 10 | | | | | | | | | | | 8 |
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| 102 | | 4.79. | | | | | | | | | 8 |
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| 1150 9-4 | _ | | | | | | | | | | ; ; |
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| 120 122 123 124 | | | | 211. | | | | | | | 3 |
| 120 122 1297 118 1901 190 |] | | | 1175 | | | | | | | Ē |
| 13.5 150 150 151 | * | | | .1287 | | | | | | | 2 |
| 135 256 1460 132 1103 6130 226 | | | | £7£1- | .123 | | | | | | 3 |
| 136 8 254 | = | | | 0891- | 13 | | | | | | \$ |
| 146.3 343 -1722 -169 -1150 973 243 1520 515 -2210 -2210 -220 -1207 1017 243 463 21061 -3266 -326 -1207 1017 243 463 21061 -30080 -3462 1622 966 76 463 226 1622 966 76 76 1622 966 76 76 1622 966 76 76 1622 966 76 76 1622 966 76 76 1622 966 76 76 1622 966 76 76 1622 966 76 76 1622 1622 1623 76 1622 1622 1622 1623 76 1622 1622 1622 1623 76 1622 1622 1623 1623 | ٦ | | | 9181. | | | | | | | 8 |
| 152 | = | | | | * | | | | | | ž |
| 14.0 642 -2240 -1287 1017 252 1018 1018 1018 1018 1018 1018 1018 1018 1018 1018 1018 1018 1018 1018 1018 1018 1018 | 16 | | | | 3 | | | | | | 1 |
| 100.3 21001 -30200 -342 1022 1022 1009 244 75 1000 242 1002 1002 1002 1002 1002 1002 | * | | | DIZZ | .230 | | | | | | <u>و</u> |
| -34.5 1601 -3020 -3462 1622 000 76 | [*] | | | 22 | 250 | | | | | | |
| -34.5 -29.0 -25.6 | 1 | | | -30280 | -2462 | | | | | 246 | 31 |
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| 34.5 -29.0 25.6 | | | | | | | | | | | _ |
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| | AM | FORCE (KN) | 35 | <u> </u> | -29 | 0. | 25 | 9: | ** | | _ |
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AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P2-A

| | ST PANEL A (| TEST PANEL A (FRONT DIAGONAL NOT | BUCKLED | | | | | Tag See | 26 ON 101 |
|---------|------------------|----------------------------------|---------|--------|--------|--------|--------|---------|-----------|
| į | Lead (LIP) | | 1 | Dérain | Strain | Strain | Strain | Strate. | Sérais |
| | 1 .276 | 424 | | | | | | 7 | |
| | 24.3 | | | /85 | | 8 | 167 | 7 | 140 |
| | | | | -476 | | .118 | 222 | | |
| | . 9 | | | 285 | 901- | 151 | | | |
| | 3 | | | 077. | 89 | -202 | | | |
| | | | | 999 | -52 | | 107 | | |
| | | | 2 | 1204 | | | | | |
| | | | | 1305 | 90 | | 707 | 136 | 200 |
| | | | | 1407 | 97 | | | | |
| 9 | | | 287 | .1480 | | 420 | 929 | | |
| | | | | 1529 | | | 296 | | |
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| ٦ | | | | -1623 | | | | | 23 |
| 13 | 788 | 1175- | | | | | | | 3 |
| 14 | 995 | 3023 | | | ş | 470 | 3 8 | | 588 |
| 15 | .503 | .2616 | 1154 | S | 77 | | | | 915 |
| 16 | .59.1 | | | Š | | | 206 | 375 | 656 |
| 17 | 1.66 | | | | 986 | | 128 | 38. | 675 |
| 10 | | | | 90 | | | 096 | | 663 |
| 9 | | | | 8 | | | 980 | 38 | 700 |
| 8 | | 7807. | | 38 | 000 | 99 | 996 | | 707 |
| 2 | | | | 906 | -075 | 675 | 1017 | | 713 |
| 2 | | | | -218 | 788- | -704 | 10501 | | 77.4 |
| 1 | 8 | | | .167 | 1016 | .710 | 1065 | W. | |
| 7 | | | | 45 | 1207 | .769 | 1115 | OVY | 997 |
| 1 | | | | 286 | -1344 | -902 | 0511 | | 25. |
| 9 | | | 2300 | 339 | 1475 | 168- | 100 | | |
| R | | 0196 | 1222 | 35 | 1450 | 15.67 | 9970 | B : | 732 |
| 77 | | 3436 | 2064 | 361 | 1468 | | 900 | | 713 |
| 2 | ÷22.4 | 3290 | 1981 | \$ | 7831. | | 91.1 | 88. | 673 |
| 1 | | | | | | 220 | 3 | 378 | 2 |
| | | | | | | | | | |
| | | | | | | | | | |
| AXIAL F | AXIAL FORCE (KN) | -28.5 | 3.5 | -28.9 | 6 | 4.6 | | - 6 | |
| | | | | | | | | | |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P2-A

| | | Strate Strate | | Some of sec | | | | Test Se | Test Serial No. 21 |
|-----|------------------|---------------|-------|-------------|-------|--------|--------|---------|--------------------|
| ! | (arm) | | | | | Strain | Strate | Strain | Strate |
| | 1 .27.6 | 905- | | | | | | 2 | • |
| | -34.3 | | 23 | | | | | 501. | 162 |
| | 3 -41.1 | | | | | | | 351. | |
| | -503 | | | | | | | 101- | |
| | 1.0% | | | | | 982 | | | |
| | 002. | | 27 | | | 196. | | 326 | |
| | 74.5 | | | | | 437 | | | |
| | 9 | | 908 | | | -477 | | | |
| | | | | | 199 | -519 | | | |
| 9 | | | | | 437 | | 759 | | |
| | | | | -1508 | | | | | |
| | | | | .1462 | 360 | | 906 | | |
| | | | | -1316 | | | | | Ž |
| 2 | | -5067 | 2490 | 418 | | | | | |
| - | | 9869 | | 159 | | | | | |
| 2 | | -21360 | 15566 | 908 | | | | | |
| 92 | 1.96.1 | -22941 | | 3 | | | | | 920 |
| 17 | .96.1 | | | 900 | | 8 | | 900 | 171 |
| = | 50.8 | | | 230 | | | | -610 | |
| 91 | | | | Bir | 1782 | | 707 | -626 | |
| 8 | | | | 622 | 7691- | | | | |
| 12 | | | | 1274 | .1862 | | | | |
| 22 | | | | 1370 | 1972 | 006- | | | 814 |
| 23 | | | | 1426 | 2019 | -697 | 1050 | | 914 |
| 24 | | | 31502 | 1629 | .2202 | 666 | 1050 | 819- | 710 |
| 25 | | 14621 | | 87/2 | 7327 | 700 | 1000 | | 616 |
| 8 | | AEADA | | 1860 | -2452 | 690- | 1066 | | 613 |
| 27 | | 46346 | | 1913 | .2464 | -862 | 1042 | | 706 |
| 28 | | 48410 | | 2045 | .2803 | 986 | 1074 | | AUK |
| | | | 2000 | 2282 | -2785 | -974 | 1073 | | 788 |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| MAC | ANIAL PUNCE (KN) | -28 | -29.7 | -21.2 | 7 | 6.5 | 2 | 6.4 | |
| 1 | | | | | | | | | |
| | | | | | | | | - | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P2-B

| | | OI TOURS | | Caled Outside | SUCKLED OUTSIDE . BOTTOM INSIDE: | | | | |
|----------|------------------|----------|---------|---------------|----------------------------------|------|--------|-----------|--------------------|
| į | Lead (Mar) | 4 | Strate. | Otrada | 1867 | ioe) | | Test Sort | Test Serial Ma. or |
| | 10. | | * | | | | Strate | - Otrafe | Print. |
| .7 | 2 | | -505 | 8. | | | | | _ |
| | | | -009 | | | 2 | | 8 | |
| | 9 | | -772 | | | 236 | | | |
| | | | 920 | | | | | | 711. |
| | | 245 | | 3 5 | | | | | 150 |
| | | 8 | | | | | | | -212 |
| | | | | | | | | | -274 |
| | | | | S | | | | | 15 |
| | | 250 | 6 | | | 747 | | | 196. |
| 2 | | | | | -1646 | | 917 | | 416 |
| | 70.7 | | | | -1418 | | | 110 | 4 |
| 2 | 7.67. | 9111 | | 238 | | | | | |
| 2 | 200 | 400 | | 140 | | 976 | \$ | | 1 |
| 2 | 6.19 | 161 | | 12 | | | | | 8 |
| 15 | 707 | E/CL | -2780 | 6 | | 916 | 8 | | \$ |
| 4 | | 3566 | -5456 | 6340 | | 636 | 705 | | 43 |
| 1 | - 1785 | 5005 | | COM. | 8 | 1901 | | | 476 |
| † | 8 | 0110 | | BZNZ- | 1194 | 900 | | 673 | S. |
| | 42.3 | 10444 | | -2131 | 1308 | 300 | = | 983 | ALF. |
| 2 | 28 | | 20/91 | -2298 | 8071 | 200 | 410 | 3 | |
| 8 | 9.58 | | 17860 | -2408 | 96.93 | 950 | 686 | 200 | |
| 21 | 141 | 1000 | C0061- | -2496 | | 1107 | .379 | 970 | Rei |
| - | | 14788 | .17180 | 8971 | 8771 | 1115 | 8 | | .277 |
| | + | | | | 1003 | 815 | 242 | 723 | 787 |
| + | 1 | | | | | | | 716 | 981 |
| + | | | | + | | | | | |
| + | | | | | | | | | |
| + | | | | | | | + | | |
| + | | | | | | | + | | |
| + | | | + | | | | + | | |
| + | | | | | | | | | |
| 1 | | | | | | | | | |
| AXIAL FC | AXIAL FORCE (KN) | -23.8 | | | | | | | |
| | | | | -23.5 | | 7.3 | | | |
| | | | | | 1 | | | 7.2 | - |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P2-B

| | T PANEL D (A | 1831 PANEL D (REAK BIAGONAL TOP | - 1 | IALF BUCKLED OUTSIDE, BOTTOM INSIDE) | BOTTOM INSIDE | £ | | Test Serial No. 27 | al No. 27 |
|---------|------------------|---------------------------------|--------|--------------------------------------|---------------|---------|--------|--------------------|-----------|
| e de | Lead (till) | | 4 | i i | Strain. | Strain. | Strain | Ofreis | Strate |
| | | | • | | 12 | 13 | 14 | 7 | |
| 7 | .20.5 | .186 | -286 | 17. | ** | 8 | | | |
| 2 | -34.3 | .186 | | | | | | | 501. |
| 9 | 41.0 | -211 | | | | | | | 191. |
| • | -49.5 | -224 | | .30 | | | | | 186 |
| S | -57.5 | 712. | | | -808 | 306 | | | MC. |
| 0 | 8 99- | 981. | | | | | 332 | | 126. |
| 7 | -60.5 | .155 | 5 -975 | | | | | 7.7 | |
| • | .73.5 | | | 230 | | | | | |
| • | .TT.2 | | 71195 | | | | 470 | 909 | 450 |
| 9 | 1.11. | -56 | | | -1540 | | | | 458 |
| = | .782 | 9 | 0221- | | | | | | * |
| 12 | 7.67 | -13 | | | 1654 | | 105 | | YUT |
| 2 | 7.08 | • | | | | 699 | | | 5 |
| 2 | 619 | | 1343 | | -1730 | | | | 510 |
| 2 | -78.4 | 103 | | | | | | | -512 |
| 2 | -70.5 | 136 | | | | 783 | | 772 | 828. |
| 1 | 7.00- | 162 | | | | | | | 75 |
| = | -623 | 161 | | | | | | | 575 |
| = | 1.3 | 63 | -1618 | | | | Ş | Ē | 1 |
| ଥ | 9.59- | .167 | | | -3215 | 188 | | 288 | 438 |
| 2 | 7.44 | 1968 | 1435 | | | | | 878 | 250 |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| 1 | | | | | | | | | |
| 1 | | | | | | | | | |
| | | | | | | | | | |
| AXIAL F | AXIAL FORCE (KN) | -21 | -28.2 | ب | -30.2 | 6.1 | - | 6.3 | |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P3-A

| 163 | T PANEL A (F) | TEST PANEL A (FRONT DIAGONAL TO | MAL | BUCKLED INSIDE, | | , BOTTOM A LITTLE INSIDE,FIRST) | - | Test Ser | Test Seriel Mo. 30 |
|---------|------------------|---------------------------------|---------|-----------------|--------|---------------------------------|----------|----------|--------------------|
| ŧ | Load (MIN) | Strain | Strain. | Strate | Strate | Btrate | Strate | 9train | Strate |
| | | • | 2 | - | 4 | | - | • | |
| - | | 270 | 11. | .247 | .37 | 53 | 210 | | 245 |
| 2 | .560 | 436 | -15 | | | | | | |
| 9 | -63.5 | 25 | • | | | | | 16 | |
| 7 | 102.6 | .770 | | | | | | | |
| \$ | 1282 | 798- | | | | | | | 200 |
| • | .1483 | 1126 | | | | | | | |
| 7 | .175.6 | 1351 | | • | | | | | 400 |
| • | 1881 | 1534 | 133 | | | 265 | 1022 | 136 | |
| • | .200.6 | 1981- | | .1377 | | | | | |
| 01 | -215.4 | 5271- | | | | | | | 957 |
| = | .223.9 | 1101- | | -1460 | | | | | |
| 12 | -223.4 | 1812 | | | | | | | |
| 13 | | 1981- | | 1480 | | | | | |
| 7 | 232.0 | .1900 | | | -121 | | | | |
| 2 | .236.6 | 1981 | | .1532 | | | | | |
| 2 | -235.0 | 9561- | 286 | 1517 | | | | | |
| 17 | .230.7 | 1967 | | 1541 | | | | | |
| = | .244.5 | -2066 | | 1563 | .153 | | | | |
| 9 | -2490 | .2147 | | | | | | | |
| ଥ | 1.253.1 | 2922 | | .1573 | | | | | 1473 |
| 21 | | .2331 | 515 | 1544 | | | 1300 | | 1470 |
| 22 | | | | | | | | | |
| 2 | | -3101 | | -1448 | | | | | |
| 24 | 234 8 | 1882: | 16772 | | .2910 | | | 97. | |
| 52 | -2354 | -27108 | 17440 | 1790 | -3044 | * | | | |
| 2 | -235.4 | -27752 | 18075 | 1666 | 3066 | 57. | 1486 | | |
| 27 | -235 7 | .20135 | 18456 | 1954 | | 95- | | | 1379 |
| 2 | 1 562. | .28466 | 16792 | 2002 | -3110 | .37 | 1474 | • | 1362 |
| 8 | 2015 | .26632 | 19340 | 2101 | -3086 | 25 | 1991 | | 1307 |
| | | | | | | | | | |
| | | | | | | | | | |
| AXIAL ! | AXIAL FORCE (KN) | -55.0 | 6.0 | . | -53.2 | 1 | 44.6 | 8.74 | •• |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P.A.

| | I CAMPLE A (| THE LANGE A (REAK DIAGONAL TOP M) | 3 | FUCKLED A LITTLE | INSIDE, BOTTOM OUTSIDE, SECOND | # OUTSIDE, SECL | (QNC) | Track Co. | |
|---------|------------------|-----------------------------------|--------|------------------|--------------------------------|-----------------|--------|-----------|------------------|
| į | Lead (P.17) | Į. | Strate | Strate | - Strate | Strate | Bernie | 100 | TOTAL CONTROL SO |
| | | | - | 44 | 12 | | | | |
| - | 33.7 | 110 | -19 | 951- | 15 | | | | |
| 2 | -56.0 | -218 | -37 | | | | | | 200 |
| 3 | -63.5 | 357 | 42 | | | | | | |
| 1 | .102.6 | 453 | | | | | | | |
| 9 | 126.2 | .578 | 8. | | | | | | |
| 5 | -148.3 | 989 | • | | | | | | |
| 7 | .1756 | -642 | | | | | | | |
| 9 | 1981. | | | | | | | | |
| 8 | | | | | 1/2 | | | \$- | 1030 |
| 10 | | | | | | 3 | | 7 | 2012 |
| = | | | | | | | | 0 | 1141 |
| 12 | | | | | | | | 4 | |
| Ē | | | | | 350 | | 1053 | 4 | 1187 |
| | | | | | | 112 | 1075 | | |
| | | | | | | 116 | | | |
| 2 | | | 151- | 0571. | | | | | |
| 2 | | | -149 | | | | 1124 | | |
| | | 1614 | 151 | .1783 | | | 441 | | |
| = | .244.5 | .1217 | .153 | | | | | | |
| 2 | -249.0 | -1242 | | | | | | | |
| 8 | .253 1 | 1265 | | | | | g : | | |
| 21 | -251.9 | | | | 70 | 3 | 122 | 8 | 1367 |
| 22 | | | | | | 131 | 1224 | 72 | 1366 |
| 22 | | | | | 3 | 137 | 1250 | 28 | 1363 |
| 24 | 2346 | | | COOP. | 3 | 141 | 282 | 36 | 1433 |
| * | 236. | | | 19/2: | 862 | 2 | 1425 | 0 | 1507 |
| 8 | 235.4 | 3677 | | | 1101 | 992 | 1473 | 8 | |
| Ē | i a | 9700 | | INC. | 1330 | 142 | 1527 | -10 | |
| * | 236.4 | | *** | | 1982 | ŝ | 1500 | 82: | 1787 |
| 1 | 1000 | 4701 | 423 | | 7227 | 132 | 1625 | 02- | 1063 |
| | C.IS. | 1831 | -2424 | -2362· | 15192 | 94- | 6971 | 2 | 7805 |
| | | | | | | | | | |
| | | | | | | | | | |
| AXIAL F | AXIAL FORCE (KN) | 47.0 | 9. | -52.0 | 0.9 | 49.0 | 0 | 50.1 | - |
| | | | | | | | | | |
| | | | | | | | _ | _ | - |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P3-B

| į | Cond Billion | | Strain | Strain | Strate | Strate | 1 | l | |
|-----------|------------------|---------|--------|-------------|--------|--------|------|--------|---------|
| | | | | | | | | | |
| - | -37.5 | 5 .273 | -45 | 5. 270 | | | | | |
| 2 | -67.6 | -483 | | | | | | | 216 |
| 9 | -66.3 | | | | | | | 2 | 164 374 |
| • | -1192 | | | | | | | | 209 479 |
| ** | | | | | | 121 | | 749 21 | |
| - | | | | | | 156 | | | 333 786 |
| 1 | | | | | 981 | 200 | | | |
| | C ZDZ | | | 1396 | 138 | | | | |
| | -213 1 | | | | | | | | 201 |
| * | -2226 | | | 1517 | | | | | |
| | -228 4 | | 71 | 1552 | | 248 | | 95 | |
| 1 | 7 233 7 | | | | .155 | | | | 2 |
| * | 230 1 | | | 1508 | .166 | | | | |
| 2 : | 234.2 | | | | | 247 | | 510 | |
| : | 2635 | | | | | | | | |
| 1 | 1767 | | | 1620 | | | | | |
| 1 | 700 | | | | | | | | |
| 1 | 27.0 | | | | | | | | |
| † | 122 | -24877 | 16540 | 1986 | 1082. | | | | |
| = | -221.6 | .24863 | 18544 | | AIRC. | | | | |
| 8 | .225 0 | -25004 | | | - | | 200 | | |
| 21 | -229 5 | | | | 2002 | | 1500 | 300 | |
| 22 | 232.5 | | | | CIA? | | 1507 | 315 | 1249 |
| 2 | -2342 | | | | -282 | 02. | 1605 | 330 | |
| 24 | £ 60%. | 76090 | | | 2800 | 25. | 1607 | 346 | |
| × | 5 | SECONO. | | | 2838 | 7 | 1629 | | |
| * | | | 1 | | -622 | 197 | 512 | | |
| | | | 6// | 205 | 693 | 460 | 298 | | |
| \dagger | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| H | | | | | | | | | |
| VXIAL FO | AXIAL FORCE (KN) | 0.09- | 0.0 | 0.45 | | | | | |
| - | | | | 5 - | | 7.66 | 7 | 55 | 55.2 |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P3-B

| | in contract | THE PARTY DIAGONAL | HOLLOS, | KLED OUTSIDE, | SUCKLED OUTSIDE, TOP A LITTLE INSIDE ; | | | | |
|-------|------------------|--------------------|-------------|---------------|---|--------|--------|---------|--------------------|
| ź | Cood filth | 9train | Strate | Strate | Strate | Shale | | 1 | rest Serial No. 32 |
| | | | 40 | | _ | | | | |
| | 1 .37.5 | 5 | 3 | 61. | | | | | |
| | -67.6 | 385 | 3 6- | | | | | | |
| | 3 | .362 | | | | | | | |
| 4 | -110.2 | -511 | | | | | | | |
| 41 | 5 .146.5 | | 2 | | | | | | 492 |
| , | 0.481- | | | | | | | 8 | 622 |
| , | 7 .202.5 | | | | | | | 151 | |
| | 8 | | | | | 8 | 98 | 162 | |
| | | | | İ | | 107 | 1861 | | |
| 1 | | | | | | 116 | | | 671 |
| | | | 8 | | 82 | | | | 600 |
| | | | | 1203 | | | 5901 | | |
| 2 | | 9011- | | -1228 | | | 9000 | | |
| 2 | 277. | 1134 | | -1280 | 8 | | 9017 | | |
| = | | .1180 | | | | | | | |
| \$ | 522.4 | -1243 | | | | | | | |
| 5 | .260.4 | | | | | B | | | |
| 17 | .267.9 | | | | | | | | 1175 |
| 16 | | | | | | | 1284 | Ŕ | 1218 |
| 10 | | | | | | 228 | 1491 | 202 | |
| 2 | | | | | | 225 | 1493 | | 1448 |
| 21 | | 2001. | | | 725 | 230 | 1522 | 300 | 1475 |
| 22 | | | | | 783 | 235 | 1557 | 306 | 1506 |
| R | | | | | 673 | 241 | 1505 | 312 | 1545 |
| | | | | 2774 | 1642 | 246 | 1637 | 313 | 1680 |
| X | | | | .25676 | 16790 | 001 | 1570 | 96 | 1567 |
| × | | DY STATE | 18/ | 944354 | 944212 | 943679 | 943975 | -835361 | 4084 |
| | | | | 411 | 369 | 9 | 134 | 116 | 379 |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| AXIAL | AXIAL FORCE (KN) | -50.7 | 7.0 | -47.3 | .3 | 53.6 | 9 | 54.2 | 2 |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P4A

| 10 10 10 10 10 10 10 10 | Ė | | | Strain. | | | | | • | |
|--|---------|-----------|------|---------|------|--------|--------|---------------|------|-------------|
| 1.00 | | | | | | Strate | Strate | - Ofrein | 1 | rial No. 29 |
| 1.00 | | | | | | | | | | |
| 1.02 | | | | | | | | | | |
| 1.12 | | | | | | | | | | |
| 1.10 | | 427 | | | | | | | | |
| 1.12 | | | | | | | | | | |
| 1.102 1.10 | | | | | | | | | | |
| 1,12, 1,12 | 7 | | | | | | | | | |
| 12 12 12 12 12 12 12 12 | | | | | | | | | | |
| 1.12 | | | | | | | | | | |
| 1.12 | | | | | | | | | | |
| 1.15 | 2 | | | | | | | | | |
| 136 145 145 1752 227 1752 | = | | | | | | | | | |
| 152 | 12 | | | | | | | | | |
| 144 115 115 125 | 13 | | | | | | 915 | | | |
| 144 204 194 204 194 204 194 204 194 204 194 204 | 1 | 1 631. | | | | | | | | |
| 152 250 1504 2504 1151 2505 1151 2505 1151 2505 1151 2505 1151 2505 1151 2505 1151 2505 25 | 15 | | | | | | 910 | | 118 | |
| 155 256 158 | = | | | 1842 | | | 553 | | 3 | |
| 155 0 280 1905 | 1 | | | 1881- | | | 984 | 197 | | 7 |
| 132 143 | 1 | 1550 | 8 | 100 | | | 1064 | | 0/10 | 5 |
| 13.5 61.6 23.6 19.5 116.7 | 7 | 159.8 | 404 | 93.6 | | | 1103 | 170 | 3 | 3 |
| 132 5 604 -3280 151 -151 <th< td=""><td>=</td><td>.164.3</td><td>819</td><td></td><td></td><td></td><td>1905</td><td>žį.</td><td>8</td><td>7</td></th<> | = | .164.3 | 819 | | | | 1905 | žį. | 8 | 7 |
| 133 5 644 2382 -194 -1214 1021 466 1127 466 1127 466 1127 466 1127 466 1127 462 | 2 | -132.5 | - | | 1 | | 78.7 | //e: | 1049 | \$ |
| 133 8 620 -2473 -28 -1420 1140 -521 682 132 9 971 -260 37 -1501 1171 -550 982 133 0 113 0 -260 50 -1512 1170 -551 987 134 0 1134 -2702 120 -1512 1170 -551 1013 134 0 1162 -2605 120 -1512 1182 -556 1012 134 0 120 -2605 136 -1616 1226 -576 1040 135 1 -2605 171 -1562 -574 1047 20 0 1071 -1562 -1562 -1562 -1047 20 0 1071 -1563 -1663 -1616 -1542 -1542 -1047 20 0 1071 -1563 -1663 -1663 -1673 -1674 -1674 40.0 -1071 -1672 -1672 -1673 -1674 -16 | 2 | .133.5 | | ZNCZ. | 261- | 1214 | | 1 | 1127 | 8 |
| 132 9 WAZE -2566 37 -1501 1144 -339 962 133 0 1001 -2603 50 -1512 1171 -546 607 133 0 1001 -2643 66 -1520 1170 -551 1003 134 0 1134 -2772 122 -1567 1182 -556 1012 134 0 1260 -2803 163 -1607 1226 -570 1040 134 0 1200 -2823 166 -1616 1224 -572 1040 20 0 1071 -2820 171 -1616 1243 -572 1050 20 0 1071 -2820 171 -1365 1241 -572 1047 49.0 -48.0 -48.4 -17.8 -17.8 -17.8 -18.5 | 22 | 1333 | | 2473 | ×. | 0271. | 8 | 125 | 296 | |
| 133 | 23 | 0 061. | 200 | 2566 | 37 | 3 | 141 | 988 | 286 | |
| 13.04 1001 2.843 0.06 1.526 1170 .551 1003 13.4 | 22 | | 146 | 2808 | S | inci. | 171 | 975 | 700 | 7 |
| 133 1134 1132 1236 1132 1132 1133 1134 1132 1134 1 | × | | 1001 | .2843 | 1 | 7161- | 1179 | 58. | ė | X |
| 1344 1162 -7805 126 -1567 1226 -570 1012 1340 120 -2830 163 -1616 1236 -574 1040 206 1071 -2827 166 -1616 1243 -574 1050 206 1071 -2845 177 -1365 1047 -616 -48.0 -48.0 -48.4 17.8 17.8 18.5 | 1 | -133 | 138 | 2772. | 3 8 | 9891 | 1192 | 8 5. | 3 | * |
| 1204 | e : | 134 | 1162 | yan. | 77 | 1587 | 1226 | 063 | 1012 | 78. |
| 1210 | * | 012 | 120 | 9.00 | 8 | 1607 | 1236 | | 000 | .350 |
| 1208 1671 1681 1651 1651 1651 49.0 48.4 17.8 17.8 1651 | 2 | 133.4 | 1210 | | 3 | -1616 | 1247 | \$\frac{1}{2} | 9501 | 996 |
| 49.0 | 8 | 120.6 | 101 | /282. | 92 | .1812 | | 578 | 1051 | 198 |
| 49.0 48.4 17.8 18.5 | | | | -2458 | 171 | 2001. | | .578 | 197 | 1 |
| 49.0 48.4 17.8 18.5 | H | | | | | | 1063 | .907 | 36 | 316 |
| 49.0 | IIAI EC | 1000 | | | | | | | | 200 |
| 17.8 | | UNCE (KN) | 7.07 | | 4 | 4 | | | | |
| | 1 | | | | - | | 17.8 | | 18.5 | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P4.A

| | TO THEE DIRECT DIAGONAL TOP | | | DOCKER INSIDE AT LEA FAMEL-E BUCKLED FIRST | LIER FANEL-E | COLLED FIRST) | | Teet Sec | de Mo Se |
|---------|-----------------------------|-------|--------|--|--------------|---------------|--------|----------|--|
| į | [E86 (E8) | 4 | Strate | Strain | 96rate | Strain | Strate | Strate | Service Control of the Control of th |
| | | | 10 | 11 | 12 | | | | |
| | .203 | \$ | 961. | 10 | 174. | 5 | | | |
| 2 | 40.4 | 67. | 382 | | | | | | |
| 2 | -51.6 | 8 | | | | 70, | | | |
| 1 | -62.7 | 08 | | | | | | | |
| 5 | -74.9 | * | | | | | | | |
| • | 999 | | | | | | | | -215 |
| 7 | 886. | | | | | | | | |
| | a 404 | | | | | | | | |
| a | | | | | | | | 371 | |
| 9 | | | | | | | | | |
| | | | | | 1102 | 528 | | | |
| | | | | 167 | 1141 | 554 | | | |
| 12 | | 166 | 1553 | .155 | 1224 | | 475 | | |
| 5 | 1307 | 200 | 2291- | | | | | 465 | |
| = | 143.1 | 230 | .1666 | .146 | | 198 | | | |
| 15 | 1461 | 280 | .1748 | | | | | | |
| 9 | .152.2 | 340 | -1867 | | | | | 200 | |
| 47 | 155.0 | 98 | 1967 | - | | | | | |
| 18 | 150.8 | 501 | | | | | | | |
| 40 | .104.3 | 711 | | | | 71.0 | | | |
| 02 | .132.5 | 5180 | | | | /M | | | |
| 21 | - 133 S | 12861 | | | 88 | 1180 | | | |
| 2 | 0.00 | 10.00 | | | | 1253 | 9901 | 1153 | -1131 |
| ۶ | 200 | 10101 | | | | 1253 | .1070 | | .1136 |
| | | 1/24/ | | | | 1250 | -1067 | | 9011. |
| | a rr. | 17761 | | | 1067 | 1262 | -1075 | | 9711. |
| 8 1 | BSS1. | 21300 | | -2139 | 1247 | 1271 | 1001- | | 1149 |
| 8 2 | 134 | 21825 | | -2173 | 1282 | 1282 | -1067 | | 9611. |
| 1 | 0 57. | 24275 | | .2265 | 1400 | 1269 | -1007 | | 201- |
| ę | 1334 | 25108 | 31330 | -2285 | 1442 | 1287 | -1065 | | 911- |
| 2 | 1208 | 28203 | 35787 | .2431 | 1626 | 1302 | 1073 | | CF11. |
| | | | | | | | | | |
| | | | | | | | | | |
| AXIAL F | AXIAL FORCE (KN) | 7 | 48.7 | 7 | 46.1 | 8.9 | 6 | 7.0 | 0 |
| | | | | | | | | | |
| | | | | | | | | _ | - |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P4-B

| | ST PANEL D (F | TEST PANEL D (FRONT DIAGONAL TO | | HALF BUCKLER INCIDES | | | | | |
|----------|------------------|---------------------------------|----------|----------------------|-------------|--------|--------|-----------|--------------------|
| ź | Load (hily) | Strate | | ٦ſ | -1 | | | Test Seri | Test Serial No. 20 |
| | | 1 | | | | Bérain | Strate | 9trate | Brate CO |
| | | 273 | | | | | | 4 | |
| | 41.1 | COP | | | 8 | 26 | 901 | | |
| 7 | 9895 | | | | 125 | | | | |
| 1 | 577. | | | 205 | .160 | | | | |
| • | | | | 287. | 191 | | | | • |
| • | | | | 958 | 281- | | | 20. | |
| | | | 110 | | 101 | | | 102 | • |
| | 201 | | 190 | | 5 | | | 75. | 3 |
| | | | 245 | | 781. | | | | 677 |
| | | 9281· | 306 | | AL. | | 647 | | |
| | 135.0 | -2025 | 385 | | .210 | 335 | 289 | Ž | |
| | 130.5 | -2119 | 0.7 | 13/8 | \$22: | 35. | 22 | | 2 |
| 12 | -142.9 | 222 | | <u>\$</u> | -239 | .371 | 76.1 | | 633 |
| 53 | 1.001 | CU9C. | 3 1 | | .278 | 10% | | | 670 |
| 44 | | | | -1362 | 028 | \$ | 8 | | 5 |
| 15 | | | 2 | -1360 | 3 | | 814 | -445 | 8 |
| : | | 7005 | 1100 | 2001. | | | 246 | | |
| : | 686 | -4781 | 2150 | | 80.7 | 452 | 878 | | Cant |
| 1 | e Rei | -0190 | 4662 | 200 | | 1897 | 916 | 905 | |
| | 154.0 | 14026 | 0942 | 3 | 22 | 480 | 928 | | |
| 2 | -156.3 | a1071. | 27.00 | 100 | 1913 | 8 | 26 | | 1216 |
| 8 | 9751. | rocot. | | 28 | -2108 | 457 | 770 | | 1262 |
| 21 | 8 981. | | 25 | 9 | .2268 | 377 | | | 1200 |
| 22 | 98.3 | ///R | 12738 | 1018 | 2384 | 2 3 | 258 | -467 | 1329 |
| 2 | | 9/6777 | 14043 | 2211 | 7,96 | 00 | 3 | 450 | 257 |
| 1 | / 781. | 7882 | 14816 | 1280 | 100 | 777 | 788 | \$\$ | 07.1 |
| † | 163.4 | 24364 | 15782 | 1416 | /nev. | 412 | 673 | 437 | |
| 3 1 | .1663 | .25040 | 16717 | 6 | al./Z· | 985 | 976 | 422 | 200 |
| e | .165.5 | .28673 | 16674 | 710 | 2807 | -375 | 296 | CQ# | 0101 |
| 12 | -1863 | 27177 | V 80 V A | 20/1 | 5005 | 359 | S | | 1430 |
| 2 | .1663 | -27861 | 1017 | 75 | .3163 | 796. | ā | S | 1465 |
| 82 | .165.5 | | 264/1 | 1952 | -3274 | 20.0° | | PUS: | 1477 |
| 90 | C 181. | D/Mey. | 17707 | 2065 | 3362 | 700 | | 78. | 1469 |
| | | BS1/2: | 17019 | 1973 | 30 % | *** | 8 | 351 | 1493 |
| | | | | | | 8 | 218 | 7967 | 1363 |
| AXIAL FI | AXIAL FORCE (KN) | -51.5 | - | 28.5 | | - | | | |
| 1 | | | | | | 8.11 | | 15.2 | |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P4-B

| - 2 6 4 | -24.1 | • | | | | | | Strate | Strate |
|----------|------------------|--------|------|-------|-------|-------|------|--------|--------|
| - 0 6 4 | -24.1 | | | | | | | | |
| 7 7 | | | | | | 2 | | 16 | |
| n T | | | | | 22. | .29 | 6 | £. | |
| 7 7 | | | | 270 | 119 | -56 | | 14 | |
| • | 9 | | 82 | 413 | .163 | | | | |
| | :77.5 | 426 | .162 | -561 | 981- | | | 200 | |
| 8 | -82.6 | .791 | 0.1. | | | | | | |
| • | -107.0 | 716- | | | | | | | 115 |
| 7 | 9811- | | | | | | | 167 | 177 |
| • | 128.1 | | | | | | | 628- | 723 |
| • | | | | | 991. | 340 | | | |
| 9 | | | | | -139 | 976- | 303 | | |
| 1 | 8021 | | | 1331 | .119 | 4 | | | |
| = | 130.5 | | Ş | 2961- | 8. | | | | |
| 2 | -142.9 | 1524 | | 1458 | | | | | |
| 1 | 1001- | .1563 | | | | | | | 8 |
| 14 | -149.3 | 7991- | | | | 2 | | -561 | 465 |
| 15 | c 521. | | | | | | 25 | -566 | 208 |
| 5 | 3 630 | | | | 8 | | | | |
| : | 000 | 20/1- | | 90/1 | 4 | | 543 | | |
| ; | erei. | 88 | 3 | 1760 | 28 | | | | |
| | 8 | 1842 | 117 | -1805 | 1001 | | 610 | | |
| | 6961 | 9981 | 147 | 1636 | 110 | | | | |
| 2 | .157.8 | -1037 | 186 | 18581 | 127 | | | | |
| = | -169.6 | 1961- | 622 | | *** | | | | |
| 2 | 2.181.3 | F906- | 100 | | | | | | 874 |
| 2 | 7 581. | 2000 | \$ 8 | | 901 | | 910 | 616- | PEB . |
| 72 | 181. | 200 | 8 | /201: | 8 | 110 | 873 | 199. | 986 |
| × | | CORES. | 8 | 8891 | 37 | 178- | 78 | | 0501 |
| 1 | 5 501. | 9#/Z: | 3 | 1286 | 300 | 979- | 1124 | , | 1163 |
| 1 | 0 0 | 3180 | 1256 | 984 | -653 | -1035 | 1222 | | 1218 |
| 1 | 2001 | 3 | 253 | 902- | 188 | .1073 | 1293 | | 1280 |
| 1 | 68 | 2786 | 1015 | 194 | .1050 | 1011- | 1351 | | 100. |
| 8 3 | 5 591 | 4442 | 2200 | -214 | -1242 | 1136 | 1071 | | |
| Q, | 1312 | 1500- | 2000 | 382 | 1502 | 1440 | 0171 | | 9761 |
| 1 | | | | | | | | | 000 |
| AXIAL FC | AXIAL FORCE (KN) | -50.2 | 7 | 49.7 | 7. | 0.5 | 2 | 6 | - |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN PS-A

test panel a (front horizontal buckled first ,then front panel dre diagonal buckled outside FRONT DIAGONAL NOT BUCKLED)

| | | | | | | | | I OST SOUTH NO. | M No. 26 |
|---------|------------------|-------|-----|-------|------------|--------|------|-----------------|----------|
| į | Lead (ILN) | | | | 7 | Strain | • | | Strate |
| 1 | .353 | 179 | | 1. | 2. | | 136 | | 143 |
| 2 | .953 | -460 | 16 | | | | | | 4 |
| c | .127.6 | -633 | | 106- | | 149 | | | 225 |
| 7 | -161.4 | -607 | | | | | | | 250 |
| \$ | 1981 | 786 | | | | | | | 786 |
| 6 | -230.9 | .1186 | | | | | | | 128 |
| 7 | .265.3 | 1407 | | | .167 | | | | 1062 |
| • | -289 4 | 1674 | | -1159 | | | | | 501.1 |
| • | .3216 | .1893 | 311 | | | | | | 1380 |
| 01 | .343 2 | -2137 | | | | 421 | | 205 | 1357 |
| = | .354 0 | 1722. | | | | | | | 1401 |
| 12 | .357 4 | -2346 | | | | | | | 1418 |
| 13 | .365 0 | | | | | | | | |
| = | .376.0 | .2597 | 566 | | | | | | |
| 15 | .379.6 | .2007 | | | | | | | 9051 |
| ē | 7.000. | .2736 | | 1383 | -352 | | | 326 | 1525 |
| 2 | .382.3 | .2786 | | .1376 | -363 | | | | 1524 |
| 2 | 9108 | 1282 | 121 | | 363 | | | | 1560 |
| 2 | 384.5 | 2880 | | .1400 | | | | | 1572 |
| 8 | 986. | -3125 | 618 | | | | | | 1581 |
| 21 | 0.000 | 1716- | 099 | 1390 | -425 | 209 | | | 1595 |
| 22 | 402.6 | 8233 | 8 | 1386 | 967 | | 1407 | 351 | 16091 |
| 23 | 405.9 | ACCC. | 916 | 1383 | -453 | | | | 1622 |
| 24 | -408.2 | 2386: | 88 | 1363 | -473 | 523 | 1425 | | 1632 |
| \$2 | 6 80% | 3360 | 008 | 1362 | -473 | 523 | 1370 | SSE | 1575 |
| 8 | 404.3 | .341 | 808 | 1366 | -463 | 528 | 1376 | 950 | 1587 |
| 27 | 0.804 | | 916 | 1371 | -460 | 528 | 1379 | 956 | 1583 |
| 2 | 400-0 | .3474 | 628 | 1361 | -496 | 534 | 1391 | 956 | 1606 |
| 2 | -412.5 | | 176 | 1360 | -503 | 536 | 1386 | 956 | 1615 |
| 8 | 413.7 | 2585- | 756 | 1381 | -509 | 838 | 1386 | 310 | 1017 |
| | | | | | | | | | |
| AXIAL ! | AXIAL FORCE (KN) | -69.3 | .3 | -73.4 | 7 . | 75.0 | 0. | 7.9.7 | 7 |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN PS.A

| = | THE THEOLOGY WOLL WIL | | | | | | | | |
|-------|-----------------------|--------|------|------------|-------|--------|--------|------|--------|
| į | Lond (MM) | Į | į | Strate | 4 | Strate | Berain | a in | Strate |
| | | | = | + | 42 | 13 | | | • |
| | 353 | | 82. | -125 | -29 | 19 | 101 | | 111 |
| | | | | 185 | .78 | 88 | | | |
| | 3 .127.6 | | | 461 | .100 | | | | |
| | | | 821. | 459 | 121. | 104 | | | |
| | 1984 | 208- | .145 | .784 | | 131 | | | |
| | -230.9 | 796. | 291- | -636 | -147 | 951 | | | |
| | 7 2053 | 1110 | 121- | -1086 | 151. | 991 | | | |
| | 200.4 | 1282 | 571. | -1254 | P\$1· | 214 | | | |
| | | .1307 | 571. | 1361 | .150 | 233 | | | |
| | 10 343.2 | 1513 | 981 | -1469 | 143 | 192 | | | |
| | | 1574 | .163 | 1523 | | 182 | | | |
| | 12 .357.4 | 1567 | -150 | .1543 | | 382 | | | |
| | 13650 | -1642 | 156 | 1563 | | 98 | | | |
| | | 1703 | 151. | 1840 | .128 | 280 | | | |
| - | 379.6 | .1724 | 791. | 1666 | 123 | 283 | | | |
| | 7.000. | 1747 | .145 | .1860 | .120 | 286 | | | |
| - | | 1749 | 291. | 1676 | .120 | 787 | | 181 | |
| | | 1081- | 861. | -1725 | .113 | 283 | | | |
| | | | 201. | 9671- | 211. | 286 | | | |
| 7 | | | 921. | 0571. | -100 | 286 | | | |
| 7 | | | 621- | 1767 | 901- | 300 | | | |
| 7 | | | | .1786 | 101. | 304 | | | |
| 2 | | | 124 | 18081 | 101- | 306 | | | |
| 72 | | | | 7101. | .100 | 312 | | | |
| 7 | | | | 1786 | 901- | 332 | | | |
| | | | | 1921. | 20. | 343 | 1317 | | |
|) X | | | | -1803 | 101- | Sec. | 1324 | | |
| R | | | | 1822 | 8 | 351 | 1335 | | 1991 |
| 2 | | | | -1636 | 98- | 357 | | | 1512 |
| R | 437 | -1886· | 00% | 1943 | 50- | 363 | 1344 | | 1516 |
| | | | | | | | | | |
| AXIAL | AXIAL FORCE (KN) | -79.8 | 9.6 | -76 | • | 99 | 66.3 | 67.9 | 6. |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN PS-B

test panel a (front diagonal not buckled) ,panel H Horizonal and rear diagonal buckled first

| | | | | | | | | Test Ser | Test Serial No. 34 |
|----------|------------------|------|--------|-------|-------|-------|--------|----------|--------------------|
| <u>:</u> | | | | | | | Strate | State | Strata |
| | 100 | | | | | | | , | |
| | | | | | -214 | 165 | | 174 | |
| | | | | | .357 | 273 | | 284 | 15 |
| | 988 | | | | | 38 | | 397 | |
| | | | | | -685 | | | 524 | 8 |
| | | | | | 3511. | | | 946 | |
| | | | | | .1338 | | | | |
| | | | | 3 | 1516 | 10801 | | | |
| | | .213 | 1380 | | .1700 | | | | |
| | | -216 | 1535 | 167 | -1895 | | | | |
| 2 | | | 9861. | 191 | .1973 | | | | |
| = | | -216 | 1636 | 217 | -2046 | | | | |
| 12 | | -215 | 0071. | 252 | -2148 | | | | |
| 13 | | -216 | 22.11. | | .2202 | 1481 | 0 | | |
| 7 | -406 3 | -216 | 1790 | | | | e. | | |
| 15 | | -218 | 1881- | | | | 7 | | |
| 2 | | | | | | | 9- | | 170 |
| = | 433.6 | \$22 | 1981- | 422 | -2667 | 1630 | 91- | | 1 |
| = | | | 0081 | 057 | | 1668 | 01- | | 791 |
| 2 | | | 20. | 999 | | 1679 | -12 | | 80 |
| 8 | | | | 463 | | 1692 | -12 | | 187 |
| 21 | | | | Ş | 12731 | 17071 | .13 | | 180 |
| 7 | | | | 510 | .2750 | 1705 | 71- | | 184 |
| 2 | | | | 28 | -2764 | 1221 | -15 | | 167 |
| 22 | | | | 535 | .2787 | 1719 | -17 | | 186 |
| ę | | -246 | | 575 | -2867 | 1751 | .10 | 1673 | 182 |
| R | | | | 000 | .2627 | 1760 | -18 | | 162 |
| 7 | | | | 999 | 9006 | 1770 | -24 | 1699 | 100 |
| R i | | 285 | | 3 | -3051 | 1773 | -26 | 1663 | 163 |
| 2 | | .207 | | 202 | 1906. | 1769 | -28 | 1708 | 185 |
| R | 0.00 | 202 | 1216 | 335 | 9981- | 1035 | -19 | 0001 | 68 |
| | | | | | | | | | |
| AXIAL | AXIAL FORCE (KN) | 9 | -82.5 | -82.0 | 0.0 | 63.2 | r, | 68.1 | 1 |
| | | | | | | | | | |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN PS-B

TEST PANEL A (REAR DIAGONAL TOP HALF BUCKLED INSIDE,AND HORIZONTAL BUCKLED OUTSIDE INPLANE ND OUTPLANE)

| NE COLFEANE) | , remarks | | | | | | | Test Serial No. 34 | Mo 34 |
|--------------|------------------|-------|---------|--------|--------|--------|--------|--------------------|--------|
| į | Lead (LIX) | | atria. | Strate | Strate | Strain | Strate | Strain | Strate |
| ľ | | | | = | 12 | 13 | 14 | • | _ |
| | | | | -14 | 124 | 129 | 72 | | |
| 7 | | | -298 | | -222 | | | | |
| | | | 946 | 8. | | | | | |
| 1 | | | 633 | -49 | | | | | |
| S | | 252 | 7011- | | | | | 8 | |
| 9 | 2812 | 323 | 3 .1426 | 501. | | 200 | | | |
| 7 | 2806 | | | | | | 777 | | 791 |
| • | .323.5 | | | | | | | | 8 |
| • | 356.4 | | | | | | | | 233 |
| 9 | -365.0 | | | | | | | | 278 |
| = | 0 776- | | | | | | | | 2 |
| 12 | 300 6 | | | | | | 200 | | 314 |
| 2 | -307.3 | | | | | | 23 | | 32 |
| 2 | -408.3 | | | | | | 45 | | 354 |
| 15 | -422.6 | 9001 | | | | | 199 | | 95 |
| 10 | 426.8 | 1477 | | 519. | | 0861 | 512 | | 416 |
| 17 | 433.6 | 1441 | | | | | Ŕ | | Ş |
| 10 | 240.3 | 1825 | | 467 | | | 3 | | # |
| 10 | | 2105 | | | | | 575 | | 462 |
| 2 | | uu | | | C/A: | | 283 | | 495 |
| 2 | | 242 | | | Š | | 985 | | 206 |
| Z | 100 | 2740 | | | 006 | | 613 | | 521 |
| 2 | 183 | | | | -907 | 1839 | 129 | 2007 | 532 |
| 7 | 7400 | 1007 | | | 797. | 1857 | 632 | 2022 | 25 |
| * | | 79/07 | | | 787 | 1867 | 632 | 2022 | 543 |
| 1 | 2 | 3000 | | | 121. | 1696 | 959 | 2060 | 899 |
| 8 2 | A 100 | 7 | | | -633 | 6161 | 676 | 2079 | 106 |
| | 6.50 | 4318 | | 1165 | 967 | 1940 | 704 | 2086 | 616 |
| 1 | 0.00 | 4807 | 10862 | 1251 | 990 | 1942 | 121 | 2002 | 617 |
| 2 | -463.7 | 9036 | 11108 | .1285 | 348 | 1963 | 732 | 2111 | 640 |
| R | 0.000 | 9620 | 16662 | 9981 | 452 | 2063 | 546 | 1222 | See |
| 1 | | | | | | | | | |
| AXIAL F | AXIAL FORCE (KN) | -88.2 | 1.2 | -64.6 | 9: | 89.6 | 9 | 92.7 | |
| 1 | | | | | | | | | |
| | | | | | | | | - | - |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN PS-B

| ! | TEST PAREL D (PRORT DIAGONAL N | | | | | | | | |
|-------|--------------------------------|--------|--------|--------|-------------|-------------|--------|----------------|----------|
| į | Lond (LM) | Strate | Strate | Strate | Strate 1 | Orașia 1 | Sereis | Office Control | Series . |
| | | | 2 | • | • | | | | |
| | | 8. | 2 | 571- | 55- | 15 | 170 | | |
| | | | ,2 | 785 | -82 | 20 | | | |
| | 986 | | | 89 | -129 | * | | | |
| | | | | .546 | 171 | 71 | | | 765 |
| | | | | | -262 | 151 | 23 | 20 | |
| | 201.2 | 980 | | | ZX: | 181 | | | |
| | 7 | . 180 | | | Ŗ | 521 | | 200 | |
| | 323.5 | .207 | | | 20\$ | 3 | | | |
| | . 354. | V2. | 16.6 | | | 22 | | 3 | |
| - | 10.385.0 | -244 | | | | 2.0 | | | |
| | 977.0 | | | | 477 | 177 | 767 | | |
| | 12 .360.6 | -271 | | | 79. | 56 | | | |
| | 13 .307.3 | -278 | | | 719- | | | | |
| - | 14 -408.3 | | | | 25. | | | | |
| 15 | 422.6 | 910- | | | 199 | 3 | | | |
| 16 | 429.0 | 82T- | | | | 3 | | | |
| 47 | 433.6 | 757 | | | | | | | |
| 10 | | | | | | | | | 162 |
| | | 920 | | | | 320 | | | 9591 |
| | | 9/6- | | | 217. | CR. | 1580 | | |
| | |) A | | | 287. | 338 | | | |
| 1 | | -401 | | | 192. | 343 | | | 1704 |
| 2 2 | | -421 | | | 790 | 345 | | | |
| | | 429 | | 2770 | 210 | 349 | | | |
| 2 | | 957 | | 1981 | 810- | 348 | | | |
| e : | | 453 | | | \$ | 380 | | | 1756 |
| 8 7 | | 2 | | 202 | 628 | 369 | | | 1781 |
| 1 | | 585 | | 2821- | | 360 | 1704 | 348 | 18061 |
| | | 8 | | 2111- | 9011. | 384 | 17071 | 252 | 1812 |
| 2 | | 129- | | 1911. | .1135 | 390 | 121 | 257 | 1001 |
| R | 000 | 706- | 1463 | * | 910 | -82 | 1190 | .128 | 1216 |
| | | | | | | | | | |
| AKIAL | AXIAL FORCE (KN) | • | 8.8 | -86.0 | 0; | 72 | 72.3 | 71.1 | - |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN PS-B

| £ | | | _ | 1 | Strate | Strain | Strain | Strate | Strate |
|------------|------------------|-------|-------|-------|--------|--------|--------|--------|--------|
| | | | | 41 | 12 | 13 | | * | |
| | 402 | 981. | 22 | .143 | 98. | | | | |
| | | | 31 | .257 | | | | | |
| | 978 | | 7 | .379 | 89- | | | | 20 20 |
| | | | | -526 | | | | | |
| | 226.7 | 1207 | 114 | -960 | | | | | |
| | -201.2 | 1434 | 153 | 1128 | 181. | | | | |
| - | 7 -293 6 | 1666 | | 1286 | 872 | | | | |
| 7 | .323.5 | | 28 | WY. | | 3 | | | |
| - | -354.4 | | | 1574 | 22 | 5 0 | | | |
| 10 | | | | 90.90 | 177. | /c | | | 1143 |
| 11 | | | | 1000 | 177. | 0 | | | 1186 |
| 12 | | | | 6/01. | 197 | 3 | | | 1226 |
| - | | | | 2211: | Ž. | 8 | 1450 | 189 | |
| | | | | 1571- | -274 | 88 | 1481 | | |
| | | | | 1759 | -324 | 8 | | | |
| | | | 992 | 1001- | .350 | 74 | | | |
| 9 | | | | -1707 | 376 | | | | |
| ? [| | | 1001 | -1780 | -437 | | | | |
| = | 440.3 | 3778 | 1001 | 1784 | 994 | | | | |
| 2 | | .3963 | | 7571- | 499 | 8 | | 177 | |
| 8 | | -4074 | 1252 | 1621- | 615- | 2 | | | |
| 21 | - 49 | -4281 | 1350 | 1001. | \$69· | 2 | | | |
| 22 | | -4565 | 1512 | -1633 | 909 | 2 | | | /7G1 |
| 2 | | -4679 | 1560 | 1634 | 029- | 8 | | | |
| 24 | | -4715 | 1579 | 9291 | 929- | 96 | | 243 | |
| R | | -5023 | 1740 | 1611 | 42.5 | 26 | | | CLY |
| 8 | | 949° | 1960 | .1550 | .743 | 8 | | | 2030 |
| 27 | | -6332 | | -1415 | 198- | 100 | | | ace |
| 2 | | 9802- | | .1283 | 558- | 103 | | | QU94 |
| 8 | | .7253 | 2010 | 1275 | 096- | 901 | | | aca: |
| R | 0000 | 10045 | 8215 | -672 | 1531 | 752 | 5050 | | 4771 |
| | | | | | | | | | |
| AXIAL | AXIAL FORCE (KN) | ğ | -86.8 | -85.3 | 6 | 67. | * | 65.2 | 2. |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN PGA

| = | ST PANEL D (F | TEST PANEL D (FRONT DIAGONAL | | KLED INSIDE TOTALLY | | | | Test Se | Test Serial No. 28 |
|------|------------------|------------------------------|------|---------------------|-------|--------|----------------|---------|--------------------|
| ž | | | | | 1 | Strain | S train | Strate | Otrata |
| | 1 .34.7 | 7237 | | | | | | • | |
| | 2 -640 | | | | | -73 | 2 | 30 | 100 |
| | 3 | | | | | 98 | 207 | | |
| | | | | | .160 | 0 | | | |
| | 8 | | | | 991. | -192 | 374 | | |
| | | | | ş | -209 | .250 | | | |
| | 961 | | 31. | 9511- | | | | | |
| | | | | 1360 | | | | | |
| | | 1171. | | 1522 | | | | | |
| | | .1973 | 3 22 | | | | 700 | | 740 |
| | 10.230.7 | -2113 | | | | | | | 672 |
| | 236.0 | -2280 | | | | | | 989 | 82 |
| | 12 .243.3 | | | | | | | | 1030 |
| _ | 251.0 | | | | | | 2011 | 435 | 0701 |
| _ | 975. | | | | 255 | 192. | 1207 | | 971 |
| | | | | | | 787 | 1246 | | |
| | | | | | | -812 | 1277 | | |
| | | | | | | | 9081 | | 077 |
| | | | | | | | 1403 | | 6/71 |
| | | | 1163 | .1673 | | | **** | 3 | (S) |
| | | 9209- | | 1121- | | | | | 2 |
| ~ | 20 | 4132 | | | | | 1018 | | 1418 |
| 21 | .241.8 | -4240 | | | *** | | 1551 | 80 | 1432 |
| 22 | 237.6 | | | 900.1 | | | 1586 | -647 | 1440 |
| 23 | | | | -1028 | 1090 | 1120 | 1654 | -876- | 1496 |
| 98 | | | | 8 | 1188 | 1150 | 1669 | | 1525 |
| 25 | | | | 80 | -1312 | 1196 | 1720 | | 7951 |
| 92 | | 2704 | | 3 | 1434 | -1213 | 1756 | -822 | 1585 |
| 27 | | 2000 | | 524 | 1504 | .1234 | 1785 | 200- | 1614 |
| 20 | | MOCOL. | | 8 | 1885 | 4721. | 1841 | 978 | SEAR |
| 2 | | 14/02 | | 8 | -2144 | -1306 | 1665 | 190 | 90 |
| 8 | | 27.01. | 200/ | 282 | -2307 | .1338 | 1921 | 90 | |
| | | /8/201. | 2059 | 83 | .2613 | 1369 | 1961 | 980 | 9469 |
| | | | | | | | | | 767 |
| AXIM | AXIAL FORCE (KN) | -91.3 | 1.3 | 84.8 | 97 | 21.4 | • | 24.0 | 6 |
| | | | | | | | | - | |
| | | | | | | | | | _ |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN PG-A

| F | ST PANEL D (| TEST PANEL D (REAR DIAGONAL BUCK | | LED OUTSIDE TOTALLY | | | | Test Se | Test Seriel Ma. 98 |
|----------|------------------|----------------------------------|----------------|--|----------------|--------|--------|---------|--|
| ŧ | [ess (2.10) | | eraje eraje | a de la composição de l | Strain | 9trata | Strain | Strate | Photo: Edition of the Control of the |
| | | | \$ | = | 12 | | | 7 | |
| | 28. | 702 | 7 -47 | u- | 2335 | 7 | | | |
| | 2 640 | | | | | 3 | | | |
| | 988 | | -96 | | | | | | |
| | | | 104 | | -859 | | | | |
| | | . 835 | | 40 | • | -230 | | | |
| | | 1142 | .79 | | | 286 | | 27. | |
| | | 7921- | | | | 296: | | | |
| | | 1556 | 5. | 200 | | -465 | | | |
| | | | | 386 | | .963 | 999 | 285 | |
| | | | | 450 | .2301 | 809 | | | |
| | | | | 510 | | -865 | | | 4// |
| | | | | 543 | -2512 | - 00 | | | |
| | | | | 610 | | 867. | 759 | | |
| | | | | 645 | | .763 | | | |
| | | | | 642 | -2719 | 817. | | | |
| | | | | 682 | -2814 | 509- | 1018 | | |
| 7 | | | 220 | 782 | | 980 | 1080 | | 90.55 |
| | | | | 912 | 9816- | 140- | 110 | | |
| 2 | | | | 1136 | 933 2 4 | -1233 | 1303 | | |
| R | | | | 1233 | -3420 | 1286 | 1341 | | |
| 7 | | | | 1320 | -3434 | -1315 | 1372 | | |
| 2 2 | | | | 1446 | .3463 | .1355 | 1427 | | |
| 1 | | | | 1520 | 3490 | -1360 | 1446 | | |
| 22 | | | | 1605 | 3536 | -1360 | 1486 | | |
| 2 | | | | 1713 | 3620 | .1353 | 1478 | | |
| 3,0 | | 0182 | | 1850 | .3740 | .1338 | 1486 | | |
| * | 0.000 | 2103 | | 2236 | 4236 | 1306 | 1499 | | |
| 8 | | egi. | \$ | 3960 | 4848 | 1284 | 1507 | 1324 | |
| 5 | | 1001 | | 3007 | .5369 | .1273 | 1520 | | 1614 |
| 1 | 1,777. | 9//1- | 30/ | 3808 | 6119 | .1249 | 1540 | | 1640 |
| | | | | | | | | | |
| AXIAL | AXIAL FORCE (KN) | -79.8 | 9.8 | 92 | -82.5 | 8.7 | | 9.6 | 4 |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN PG-B

| - 306 | į | Lond (Mar) | į | 1 | Strate | Strate | Strate | | 1 | Test Serial No. 15 |
|--|---------------|------------|------|-------|--------|--------|--------|------|------|--------------------|
| 145 | - | 286 | | | | | | | į | Strate |
| 196 | ~ | | | | | | | | | |
| 150 | - | | | | | | | | | |
| 118 | | | | | | | | | | |
| 1982 | | | | | | | | | | |
| 1982 | | | 71. | | | | | , | | |
| 1983 200 401 412 | • | .119.5 | | | | | 233 | | | |
| 1867 200 1175 120 1175 120 1215 121 | 7 | -1363 | 202. | | | | 277 | | | |
| 142 270 1175 1120 1122 1124 1125 11 | 0 | 7.881- | Sec. | | | | ACE | | | 90 |
| 1.00 1.150 | 0 | 0.001 | | | | | 02.0 | | | 135 |
| 150 | 01 | 1691- | Ş. | | | | | 1 | | 191 |
| 270 (2) 150 14450 550 -152 152 271 (2) -118 (1) | Ξ | 1 | S. | | | | | = | | |
| 2.71 a 189 1520 37 1612 573 161 2.72 a -181 -181 -181 -171 544 -210 2.72 a -172 -171 564 -210 2.72 a -172 -172 564 -210 2.72 a -172 -172 564 -210 2.72 a -162 -172 564 -210 2.72 a -162 -176 66 -210 2.72 a -162 -176 -216 -217 2.72 a -162 -164 -216 -216 2.72 a -162 -176 -216 -226 2.72 a -162 -216 -276 669 -276 2.72 a -162 -216 -276 -266 -276 2.72 a -162 -216 -276 -276 -276 2.72 a -162 -216 -276 -276 -276 2.72 a -1 | 2 | 7.600 | 81. | | | | 3 | 91- | | 11 C |
| 27.1 6 1.161 4.61 1.611 6.61 5.47 2.10 27.1 6 1.162 1.162 1.162 5.41 2.20 2.20 23.1 1.1 6 1.162 1.162 6.41 2.20 2.20 23.1 1.1 6 1.126 6.61 2.20 2.20 23.2 2.2 6 1.162 6.61 2.20 2.2 2.2 1.2 6 1.162 6.61 2.21 2.2 2.2 1.2 6 1.162 6.61 2.22 2.2 2.2 1.2 6 1.162 2.24 2.22 2.2 2.2 6 1.162 2.24 2.24 2.22 2.2 2.2 6 2.2 6 2.2 6 2.24 2.20 2.22 2.2 2.2 6 | 1 | an y | 3 | | | | 222 | 9 | | |
| -278 s -179 c -180 c -178 c -178 c -220 c -220 c -237 d -118 c -178 c -178 c -178 c -178 c -220 c -220 c -237 d -118 c -178 c -128 c -184 c -184 c -220 c | 1 | 6127 | 181 | | | | 3 | -21 | | |
| 253.4 -1126 4.2 -1733 606 -241 243.1 -1156 4.2 -1965 641 -262 243.1 -1156 6.3 -1965 641 -262 250.6 -128 -1647 144 -2745 690 -276 267.1 -120 -1647 144 -2746 690 -280 267.2 -120 -1647 144 -2746 690 -280 267.1 -166 -1667 176 -276 690 -383 267.2 -166 -276 690 -380 -380 -380 267.2 -166 -276 690 -380 -380 -380 268.1 -177 -278 -260 -241 -270 -270 269.2 -176 -276 -260 -270 -270 -270 269.2 -176 -276 -270 -270 -270 -270 269. | 1 | .228.9 | 971- | | | | 35 | 22 | | |
| 243.1 -151 -1780 6.5 -1865 641 -202 -205.5 -143 -1867 66 -276 66 -276 -205.6 -1867 -1867 144 -2176 66 -276 -205.6 -1867 -1867 176 -2246 60 -337 -275.7 -186 -186 176 -276 60 -337 -275 -103 -2016 216 -276 646 -357 -275 -276 -276 646 -350 -275 -276 646 -350 -275 -276 640 -360 -275 -276 640 -360 -275 -276 640 -360 -275 -276 640 -360 -276 -276 647 -478 -276 -276 -276 -276 -276 -276 -276 -276 -277< | | -237.4 | 291- | | | | 900 | 24 | | |
| 250 5 -1443 -1856 65 -1940 650 -273 251 6 -128 -1847 144 -2712 786 -283 227 1 -128 -1867 170 -2746 699 -283 227 1 -118 -276 -274 -284 -283 227 1 -118 -276 -284 -283 228 4 -118 -276 -283 -283 227 1 -118 -276 -284 -283 228 1 -118 -276 -284 -284 28 2 -214 -278 -284 -479 28 2 -214 -272 -284 -479 28 2 -216 -272 -284 -479 28 2 -178 -1779 -1776 -284 28 2 -178 -178 -179 -179 28 2 -178 -178 -179 -179 28 3 -178 -179 | 2 | -243.1 | 181- | | | | 2 | 18 | | |
| 287 6 -138 7 -148 7 144 7 -217 8 -78 9 -283 7 287 6 -138 7 -148 7 144 7 -217 8 78 9 -283 7 287 1 -138 7 -169 1 170 7 -224 8 86 9 -337 7 283 2 -160 3 -201 3 -278 9 86 9 -383 7 283 2 -201 3 -278 9 86 9 -383 7 283 1 -278 9 86 9 -380 7 284 1 -278 9 -247 9 86 7 -427 7 285 1 -278 9 -247 9 86 7 -427 7 286 2 -215 4 -278 9 1010 7 -427 7 286 3 -178 9 167 7 -250 7 1010 7 -420 7 287 3 -178 7 182 7 -250 7 -250 7 -251 7 288 3 -170 8 -170 8 -170 8 -251 7 -251 7 288 3 -170 8 -170 8 -170 8 -270 8 -170 8 -174 8 <t< td=""><td>=</td><td>-250.5</td><td>143</td><td></td><td></td><td>9761</td><td>986</td><td>4.6.</td><td></td><td></td></t<> | = | -250.5 | 143 | | | 9761 | 986 | 4.6. | | |
| 207 6 170 144 2178 789 337 212 1 116 2016 170 2240 302 302 212 4 110 2046 2016 2016 2016 302 222 4 100 2016 2016 2017 2010 407 222 5 201 2010 2010 407 407 202 1 2010 2010 407 407 202 1 2010 2010 407 407 202 2 2010 2010 407 407 202 2 202 3 1010 402 407 202 3 112 202 3 1010 402 202 3 112 202 3 1010 402 202 3 112 202 3 202 3 202 3 202 3 110 202 3 202 3 202 3 202 3 110 202 3 202 3 202 3 202 3 202 3 <th< td=""><td>2</td><td>-261.9</td><td>123</td><td></td><td></td><td>-2045</td><td>88</td><td></td><td></td><td>356</td></th<> | 2 | -261.9 | 123 | | | -2045 | 88 | | | 356 |
| 272.1 -116 -2246 600 -357 232.2 -100 -2015 180 -226 640 -383 232.2 -100 -2016 -2140 -2214 | 2 | -267.9 | 5 | | | -2178 | 92 | | | 585 |
| 228.4 -10 -2015 150 -2250 840 -350 252.5 -2016 -2713 840 -2733 840 -350 252.5 -2714 -2714 -2712 -2712 840 -350 252.1 -2714 -2714 -2712 867 -471 252.1 -2716 -2712 867 -472 252.2 -172 -2712 867 -472 252.2 -172 -2732 1010 -462 252.2 -172 -172 -2732 -400 19.2 -172 -172 -2732 -2703 19.2 -172 -172 -2732 -2712 10.0 -172 -172 -172 -2712 10.0 -272 -272 -2712 10.0 -272 -272 -272 10.0 -272 -272 -272 10.0 -272 -272 -272 | 8 | 122. | | | | 3248 | and a | 3 | | |
| 213 -100 -217 -2373 607 -350 255.7 -2416 -2446 607 -2421 -2422 -2421 -2422 | 21 | 2784 | | | | -2288 | 070 | 78. | | 457 |
| 2005.7 -2140 246 -2440 467 457 2017 -2140 281 -2472 867 447 2017 -2160 278 -2472 867 478 2017 -245 278 -245 867 478 2017 -275 317 -253 1010 -462 2017 -173 167 -253 1010 -462 2017 -174 182 -2043 779 -371 2018 -176 182 -176 257 -357 202 -176 217 -175 2043 779 -357 202 -176 246 -176 246 -176 -256 202 -172 -1340 248 -1705 540 -174 202 -172 -1340 248 -1705 540 -174 202 -172 -172 -174 -175 -174 -174 | Ħ | | Si | | | r727. | 2 2 | 96. | | |
| 457 2140 261 261 467 467 2621 -2160 -2160 -276 -2672 967 -479 2621 -2164 -276 -276 -2500 1010 -492 2627 -172 -172 167 -2550 1016 -492 2627 -172 167 -2043 779 -371 162 -172 168 -1776 627 -357 166 -17 168 -1776 627 -257 168 -176 246 -176 527 -276 168 -176 246 -176 527 -276 168 -176 246 -176 530 -176 168 -176 530 -176 -176 -176 168 -176 -176 530 -176 -176 168 -176 -176 530 -176 -176 168 | ž | | 1 | -2716 | | *** | | 127 | | 916. |
| 262 1 40 -2160 278 -2620 1010 -470 262 1 -56 -2154 317 -2550 1010 -462 262 1 -172 2 157 2 -2550 1010 -462 262 1 -172 2 157 2 -200 76 -371 262 2 -177 2 162 2 -204 776 -357 266 2 -17 2 162 2 -1776 227 -357 268 3 -17 2 176 2 246 -176 226 269 3 -17 2 -176 2 240 -176 -176 269 3 -17 2 -176 2 240 -176 -176 | 12 | / GB | 17. | -2140 | | | | 467 | | 13 |
| 282 1 -56 -7154 317 -7530 1010 -462 284 7 -102 -1734 167 -2530 1018 -46 115 2 -112 -1177 167 -2030 776 -371 115 2 -51 -1467 165 -2043 776 -357 100 6 -51 -176 627 -357 -216 100 6 -72 -1340 216 -1756 583 -174 -65.5 -72 -176 530 -174 | 1 | 1,782 | \$ | -2160 | | 7/87 | 298 | 479 | | |
| 248 7 -102 -1738 167 -2558 1016 -486 115.2 -1177 182 -2043 776 -371 115.2 -91 -1467 182 -2043 776 -357 100.6 -97 -1409 217 -176 527 -251 100.6 -72 -1340 217 -176 580 -174 100.7 -1340 246 -176 530 -174 100.7 -1440 -1440 -176 530 -174 100.7 -1440 -1440 -176 530 -174 | 6 1 | -282.1 | Ş | -2154 | | 2002 | 1010 | -482 | | ē : |
| 19.2 -11.2 -17.7 18.2 -20.9 79.5 -37.1 19.2 -17.6 -20.4 77.9 -35.7 19.2 -17.6 -20.4 77.9 -35.7 19.2 -17.6 -20.2 -20.7 10.2 -17.6 -20.2 -20.7 21.7 -17.6 -20.2 -20.7 21.7 -17.6 -20.2 -20.7 21.7 -17.6 -20.2 -20.7 21.7 -17.6 -20.2 -20.7 21.7 -17.6 -20.2 -20.7 21.7 -17.6 -20.2 -20.7 21.7 -17.6 -20.3 -17.4 20.2 -20.4 -20.2 -20.7 21.7 -20.2 -20.7 -20.7 21.7 -20.2 -20.7 -20.7 21.7 -20.2 -20.7 -20.7 22.7 -20.7 -20.7 -20.7 22.7 -20.2 < | e | -249.7 | 201- | 9771. | | 2538 | 1010 | 087 | | 8 |
| 115.2 -01 -1467 182 -2043 779 -357 106.6 -17 -1467 185 -1776 627 -357 96.9 -72 -1340 217 -1756 563 -216 -85.5 -84.9 -19.3 -174 | 12 | -247.7 | 211- | 4767 | | 9502- | 785 | 146 | | 95 |
| 1056 417 1140 1150 -1776 627 -257 968 -772 -1340 217 -1756 563 -257 -65.5 -65.5 -84.9 19.3 -174 -174 | 2 | -215.2 | 4 | | | -2043 | 977 | - | | 95 |
| | 8 | 208.6 | | /901: | 185 | 9771- | 7.63 | ice. | 979 | 9440 |
| -05.5 -1340 2449 -1705 530 -174 -05.5 -64.9 19.3 | 8 | 0.801. | | 9091 | 217 | 9521. | | /ci | | 335 |
| -65.5 -64.9 19.3 | | | 21: | 0861- | 248 | 1705 | 2 5 | -218 | | 304 |
| -85.5 -84.9 19.3 | | | | | | | | 221. | 613 | 797 |
| | 7 - L | JACE (KN) | -85. | n, | 48 | 6 | 407 | | | |
| | $\frac{1}{1}$ | | | | | | | | 18.1 | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN PG-B

| 1.1 1.2 | No. Lead (Lt) Strain Strain | Laged (BLH) | Strate | Strain. | | - | | | CL CALLET INC. 10 | |
|--|---|-------------|---------|---------|--------|--------|------|-------|-------------------|--------|
| 100 | | | | | | | | 4 | Strain | Strate |
| 144 145 | | | | | | | | | | |
| 190 239 230 | | | | | | | | | | .2 |
| 119 273 443 241 242 113 114 | | | | | | | | | | |
| 190 232 191 242 191 242 191 242 191 242 243 | | 436 | | | | | | | | |
| 1.19 2.00 | | | | | | | | | | |
| 190 | | | | | | | | | | |
| 150 | | | | | | | | | | |
| 190 | | 7.821. | | | | | | | | |
| 1902 1902 1902 1905 | | | | | | | | | | |
| 2012 4413 1155 -540 -1055 375 311 2102 430 -1300 -530 -1205 441 -250 221 6 434 -1307 -530 -1205 441 -250 221 6 434 -1367 -545 -1205 560 -200 221 6 442 -1546 -551 -1300 500 -200 221 6 442 -1564 -551 -1560 -200 -200 222 7 442 -1570 -551 -1570 -520 -200 222 8 -429 -1570 -520 -1570 -520 -200 222 8 -520 -1571 -520 -1572 -520 -520 222 8 -520 -1572 -520 -1572 -520 -520 222 8 -520 -1520 -1520 -520 -520 -520 222 8 -520 -221 -520 -520 | | | | | | 550- | | | | |
| 200 2 430 1350 450 450 450 451 451 210 2 430 1387 542 1256 441 250 221 4 448 1480 552 1526 450 250 227 4 448 1546 551 1430 552 250 227 4 448 1624 551 1430 552 250 227 4 445 1624 551 152 252 252 243 1 1624 552 157 252 157 252 250 1 160 1 730 662 250 167 252 250 1 252 167 756 442 157 157 250 1 252 187 187 187 187 187 252 1 185 2 187 188 187 188 187 188 187 188 252 1 186 2 186 2 186 2 </td <td> </td> <td></td> <td></td> <td></td> <td></td> <td>5901-</td> <td></td> <td></td> <td></td> <td>261.</td> | | | | | | 5901- | | | | 261. |
| 2210 434 -1387 -542 -1380 466 -250 221 -446 -1466 -552 -1380 466 -250 228 -44 -1356 -552 -1380 553 -250 228 -44 -1634 -551 -1510 532 -250 233 -445 -1701 -552 -1674 642 -250 243 -163 -552 -1674 645 -252 -252 240 -245 -1677 645 -252 -252 -252 -252 270 -254 -252 -1672 645 -252 -252 270 -254 -252 -1672 645 -250 282 -254 -252 -1672 645 -250 283 -254 -252 -1672 645 -250 282 -254 -254 -1672 652 -250 283 - | | | | | | 360 | | | | -210 |
| 221 0 4190 -1490 -1500 -200 228 0 -440 -1540 -550 -1140 533 -300 229 1 -442 -1584 -551 -1540 533 -302 240 2 -445 -1664 -547 -1570 533 -302 240 3 -445 -1664 -547 -1674 642 -320 250 4 -445 -1770 -536 -1674 642 -320 250 5 -445 -1770 -528 -1674 642 -320 250 5 -445 -1770 -529 -1877 642 -320 250 6 -250 7 -1877 -1872 -250 -443 250 7 -250 7 -1872 -1872 -250 -250 250 8 -250 8 -1872 -1872 -250 -250 -250 250 8 -250 9 -1860 -250 -250 -250 -250 -250 | | | | | | | | 52 | | |
| 228 0 444 0 1540 0 555 0 1962 0 590 0 200 0 < | | | | | | 1200 | 8 | 8 | | |
| 227. 4 442 1524 531 1430 532 305 243. 5 -1634 -531 -1516 532 -322 243. 5 -1634 -536 -1674 645 -325 240. 5 -445 -1770 -536 -1674 645 -326 250. 5 -445 -1770 -526 -1674 645 -375 270. 5 -366 -167 645 -736 -442 -442 270. 5 -366 -520 -1674 736 -442 -442 272. 6 -273 -523 -1872 622 -530 -442 272. 6 -273 -345 -524 -1872 622 -530 272. 7 -345 -345 -189 -189 -189 -189 272. 7 -1007 -366 -189 -189 -189 -189 -189 272. 7 -101. 6 -276 -276 -276 -276< | | | | | | 2001 | 85 | .28 | | |
| 250 1 -1924 -1510 574 -332 250 2 -450 -1670 -547 -1570 -357 250 2 -445 -1770 -520 -1606 642 -376 250 3 -445 -1770 -520 -1607 736 -442 267 3 -272 -522 -1607 736 -442 267 3 -273 -523 -1607 736 -442 270 4 -273 -523 -1607 736 -442 270 5 -2345 -523 -1627 -626 -530 270 5 -2345 -523 -1645 -1546 -530 280 7 -2445 -245 -1645 -1546 -530 280 7 -245 -1645 -1546 -1546 -1546 280 8 -245 -245 -1645 -1546 -1546 280 8 -246 -246 -246 -1546 -1546 280 | _ | | | | | 1430 | 535 | 35 | | |
| 20.5 44.5 -1770 -5.44 -1570 64.5 -35.1 20.6 -40.5 -1872 -5.26 -1674 64.5 -37.6 20.1 -40.5 -1872 -5.20 -1674 64.5 -37.6 20.2 -20.5 -5.21 -5.22 -1672 64.2 -37.6 20.2 -20.5 -20.5 -5.21 -1672 66.2 -5.20 20.2 -20.5 -21.6 -5.21 -167.7 7.6 -5.20 20.2 -22.4 -2.21 -5.21 -167.7 -5.21 -5.21 20.2 -2.24 -2.24 -2.24 -2.24 -2.24 -2.22 20.2 -2.24 -2.21 -2.21 -2.21 -2.22 -2.22 20.2 -2.24 -2.24 -2.24 -2.24 -2.24 -2.24 -2.24 20.2 -2.24 -2.24 -2.24 -2.24 -2.24 -2.24 -2.24 -2.24 -2.24 | - | | | | | 1516 | 574 | 28°- | | |
| 201 0 400 1970 -530 -1674 643 -576 207 0 -304 -520 -1900 736 -442 272 1 -307 -520 -1900 736 -442 272 1 -307 -521 -521 -522 -463 272 2 -303 -523 -1927 622 -530 272 2 -345 -521 -1627 622 -522 285 1 -345 -421 -1627 -522 -522 285 1 -345 -422 -1645 1300 -522 182 1 -4370 -1626 -364 -522 -522 182 2 -1620 -342 -364 -364 -364 24 3 2 -1624 -366 -366 -364 -164 -164 24 3 2 -1624 -366 -366 -366 -366 -366 -366 -366 -164 -164 -164 -164 -164 | - | | | IMD. | | 1576 | 602 | 35. | | |
| 272 272 202 2 | _ | | | 0//1: | | 1674 | 645 | 976- | | |
| 222.1 -300 -1677 1627 -465 222.4 -301 -521 -1627 662 -530 222.4 -205 -231 -1627 662 -530 165.7 -245 -245 -1627 662 -530 165.7 -245 -345 -628 -1645 1710 -628 165.7 -4370 -1029 -1645 1720 -1260 -1660 162.1 -4370 -1029 -1660 - | - | | | 2081- | 929 | 9061- | 736 | 27 | | |
| 22.04 -32.1 -1827 662 -530 183.0 -20.5 -32.4 -55.3 -1872 662 -530 183.0 60 -27.2 -43.7 -43.7 -1827 662 -530 182.1 45.9 -34.5 -43.7 -1020 -1660 -1660 -1760 -760 182.1 46.3 -11360 -1600 -36.1 415.0 -760 -760 182.1 102.1 -1030 -36.1 415.0 -10.6 -10.6 182.2 20160 -21.6 -36.1 -36.1 -36.1 -36.1 -36.1 182.2 20160 -21.2 -36.1 -36.1 -36.1 -36.1 -36.1 182.2 -20.1 -36.1 -36.2 -36.2 -36.2 -36.2 -36.2 -36.2 182.2 -36.1 -36.2 -36.2 -36.2 -36.2 -36.2 -36.2 -36.2 -36.2 -36.2 182.2 <td> *</td> <td></td> <td></td> <td>/soz.</td> <td>025</td> <td>7.1877</td> <td>795</td> <td>1</td> <td></td> <td></td> | * | | | /soz. | 025 | 7.1877 | 795 | 1 | | |
| 182.1 -254 -553 -1972 652 -552 182.2 -275 -421 -1977 663 -522 -522 182.1 -262 -345 -421 -1977 1964 -522 182.1 -156 -345 -426 -165 1210 -766 1 182.1 -463.8 -1136 -136 -136 -136 -136 -136 182.1 -1224 -2016 -201 -146 170 -104 1 182.2 -2016 -201 -141 171 -104 1 182.2 -201 -341 -104 1 -104 1 182.2 -201 -342 -342 -104 -104 1 182.2 -201 -342 -342 -104 -104 -104 182.2 -3465 -3665 -366 -102 -104 -104 182.2 -342 -342 -342 | ֓֓֓֓֓֓֓֓֓֓֓֟֟֓֓֓֓֓֟֟֓֓֓֟֟֓֓֓֟֟֓֓֓֟֟֓֓ | | | .2157 | .521 | 1927 | Cart | | | 284 |
| 1857 1862 1865 1865 1866 | ֓֟֟֓֟֓֟֟֓֓֓֟֟֓֓֓֓֟֟֓֓֓֟֓֓֟֟֓֓֓֟֓֓֟֓֓֟֟֓֓֓֟֓֓֟֓֓֓֟֓֓֓֟֓֓֓֟֓֓֓֟֓֓֓֟֓֓֓֟֓֓֡֡֟֓֡֡֡֡֡֡ | | | -2341 | ess. | .197 | 28 5 | 986 | | 539 |
| 182 1 1991 (102) -3455 (102) -3250 (102) -1685 (102) 1710 (102) -786 (102 | 1 | | | 87.73 | 1 | | 76 | 285 | | 285 |
| 187.1 1001 -4370 -1029 -1865 1210 -789 -1789 149.7 -1306 -11306 -1609 -1456 1306 -620 -1 147.7 12240 -26016 -2601 410 1706 -1046 1 152 20160 -31462 -3037 1171 1772 -1077 1 160 23361 -3465 -3037 1186 1786 -1243 11 160 28361 -38612 -3037 1632 1781 -1243 11 160 -38612 -3366 -386.5 1632 1604 -1331 11 11 -401.5 -36612 -368.5 1632 1604 -1331 11 | 7 | | | 3765 | | | 3 | \$ | | 473 |
| 1467 4638 1306 460 1306 460 | 7 | | 1001 | 4470 | | 1665 | 1210 | -769 | | M.T. |
| 140.7 120.0 -36.4 136.0 -36.4 136.0 -36.4 136.0 -36.4 136.0 -36.4 136.0 -36.4 136.0 -36.4 136.0 -36.4 136.0 -36.4 136.0 -36.4 136.0 -36.4 <th< td=""><td>~</td><td></td><td>15.00 P</td><td></td><td>Con .</td><td>957</td><td>1306</td><td>-626</td><td></td><td>740</td></th<> | ~ | | 15.00 P | | Con . | 957 | 1306 | -626 | | 740 |
| 15.2 122.40 -2106.5 -2201 410 1706 -1046 172 -1077 172 -1077 172 -1077 172 -1077 172 -1077 172 -1077 172 -1077 172 -1077 172 -1077 172 -1077 172 -1077 172 -1077 172 -1077 172 -1077 172 -1077 172 -1077 172 -1077 172 -1077 172 | * | | 1001 | 90000 | | \$. | 1560 | 256 | | 277 |
| 15.2 20106 | 23 | | 04021 | 2000 | 1002 | 418 | 1706 | 1048 | | |
| 06.6 23157 -1245 -3037 1171 1776 -1243 11 06.0 23157 -34655 -3065 1365 1761 -1722 | 7 | | 3016 | COMIT. | 1182 | 35 | 1732 | 101. | | |
| 1701 - 38412 - 3865 - 1522 - 1701 - 1311 - 1131 - 1 | 28 | | 23167 | 70016 | ,808; | 1171 | 1770 | -1243 | | 67.0 |
| -101.5 -98.5 15.5 | S | | 28381 | 578 | enx: | 1305 | 1791 | -1282 | | 7101. |
| -101.5 -98.5 15.5 | | | | | Barri. | 1632 | 1004 | -1331 | 1544 | 8401. |
| -101.5 -98.5 15.5 | AXIAL | FORCE (MA) | 707 | | | | | | | |
| | | (Aura) | TOT- | o. | -98. | | 15. | | 12. | |
| | | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN PT.A

| | | STANDART NOT BUCK | | THE PARKE TOP LEG CUTPLANE BUCKLED | | | | | |
|----------|------------------|-------------------|-------|------------------------------------|--------|------|------|--------------------|---------|
| ! | | | | Oftrain | Strate | 440 | 1118 | lest Serial No. 18 | Mo. 18 |
| | | | | 2 | 9 | | | | Ofrain. |
| | | .31 | 981. | | E1: | 175 | | | |
| | | \$ | -210 | | | | | | 28 |
| | .71.6 | .53 | | | | | | 51 250 | |
| | -90.2 | 8 | | | | | | 222 | |
| | 1001. | | | | | | | | 3 4 |
| ٦ | -1284 | | | | | | | 112 | |
| | 0.891 | | | | -557 | | | | |
| | . 167.3 | | 372 | -31 | 430 | 631 | | 1 2 | |
| | 0 900 | | | | -718 | | | | |
| | | | | | | | | | 149 |
| | | 711- | .750 | | | | | | 171 |
| | 205 5 | .120 | | | | | | | 186 |
| 12 | .2130 | 121 | | | | | 220 | | |
| 13 | .220 5 | | | | | | | | |
| 2 | -2242 | | | | | | | | |
| 15 | | | nce- | | 946 | | | | Z13 |
| 2 | | | | | | | | | |
| 41 | | | -673 | | | | | | |
| | | 2 | -400 | | 196 | | | | 228 |
| | | -122 | 472 | | | | | | |
| 2 | .163.6 | 45 | 196 | | | | | | |
| 8 | .164.6 | 36 | 434 | | | | | | |
| 21 | .1602 | ğ | 103 | | | | | | 200 |
| 22 | 1.56.1 | 167 | | | | | | | 2 |
| 23 | | 1 | S. S. | | 104 | | | 2 | 8 |
| 24 | 1 441. | 1 | 270 | 7 | Si | | 218 | | 6/5 |
| 25 | S | 2 | 2 | S. | \$- | | | | 8 |
| | | 38 | 7 | 71- | 53 | | | 20 | 104 |
| | + | + | | | | | 77 | | 416 |
| | | | | | | | | | |
| T | + | 1 | | | | | | | |
| 1 | + | | | | | | | | |
| T | 1 | | | | | | | | |
| 7 | + | | | | | | | | |
| AXIAL F | AXIAL FORCE (KN) | 386 | | | | | | | |
| | | | | * | -35.5 | 48.4 | • | 47.3 | |
| 1 | 1 | | | | | - | | | |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P7-A

| | ſ | | | | | | | | |
|----------|------------------|------|-------|---------------|--------|--------|--------|-----------|---------------|
| £ | | | | Strate | Strate | Béreio | Strate | Test Seri | al No. 18 |
| | 3 | | 2 | | 11 12 | | | | Strate |
| | 900 | =- | 141 | | | | | = | 10 |
| | | .13 | | | | | ** | 142 | 35 |
| 2 | -71.6 | -15 | | | | 202 | 33 | 3 | 27 |
| • | -80.2 | -16 | | | | | 44 | | |
| 2 | 1.001 | 71. | 900 | | | | 57 | 310 | 3 8 |
| 9 | 1284 | 91. | 200 | | | | 72 | | B |
| ^ | 148.0 | 71. | | | 383 | | 8 | 1 5 | 8 |
| 0 | | 9 | 96. | 3. | | 559 | 104 | | 110 |
| Ġ | | | 8 | | | | 122 | | 9 |
| 01 | | | 742 | | | | 130 | | 163 |
| - | | 9 | 780 | | -602 | 756 | 38 | | 8 |
| 2 | 95.6 | | -837 | 961 | | | | | 196 |
| - | 0613. | 2 | -876 | -208 | | | 2 | | 207 |
| | 6077 | S | -914 | | | | 183 | | 218 |
| 1 | 2242 | 8 | -936 | 122- | 1 | | 2,0 | | 228 |
| 2 | -2280 | • | 798- | | | | 2 | | 233 |
| 2 | -231.3 | 3 | 0.C. | | | | 111 | | 230 |
| -2 | -233.1 | 28 | w. | | | | 178 | | |
| = | -236.7 | 8 | 2007 | | | | 100 | | 200 |
| 9 | -163.6 | ş | | | | | 182 | | |
| 8 | -1646 | | aror. | -213 | | | Ě | | |
| 21 | con. | | -982 | 100 | | | ş | | 279 |
| Z | 2 2 | | 988 | 8 | 196: | 958 | 2 | 2 | 282 |
| 8 | | Book | \$ | .74 | | | | | 291 |
| 7 | 7.001. | 413 | 129- | 99- | 416. | 200 | 122 | | 282 |
| 1 | 3 | 422 | 795 | \$ | | 20 | 2 | 705 | 200 |
| 2 | 1380 | 635 | .763 | | | 927 | 130 | 662 | N. |
| † | | | | | 2/2: | 619 | 120 | 678 | 500 |
| 1 | | | | | | | | | 717 |
| 7 | | | | | | | | | |
| 1 | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| AXIAI E | AXIAI FORCE (LN) | | | | | | | | |
| | ONCE (AN) | -36 | | Ÿ | -35.8 | 43.2 | | - 66 | |
| 1 | | | | | | | | 14.0 | |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P7-A

| | ST PANEL C (P. | test pamel c (pamel dae legs,pamel d | | BUCKLED OUTPLANE | Î | | | Tent Started Min 48 | ***** |
|-------|------------------|--------------------------------------|--------|------------------|-------|-------|--------|---------------------|-------|
| 4 | - | 4 | į | į | 118 | Brede | Berata | - | - |
| | | 47 | 7 | _ | _ | 24 | | | * |
| | - 200 | .362 | 800 | | | 000: | OHE- | | |
| | 49.7 | | | | | | | | |
| | 37.0 | | | | | 243 | | | 6.9 |
| | -40.2 | | .797. | | | | | | |
| | 1 401. | | | | | | | | |
| | 1384 | | | | | | | | |
| - | 7 | | | | | • | | | |
| | 6 791. | | | .1414 | | | • | | • |
| | 0 861: | - | | | | 1433 | | | |
| ĭ | 581. | +631 | 1756 | | | | | | |
| | 3888 | | | 971. | 5201- | (36) | | 1062 | 121. |
| | 2 -2130 | 475 | | | | | | | |
| | 1022 | | | | | | 9861- | | |
| 7 | 2742 | | -3046 | | .1103 | | | | |
| = | 3280 | 1201 | | | | | | | |
| 7 | 6 162- | 1004 | | | | | | | |
| 7 | 1 665- | -1146 | | | | | | | 25 |
| 1 | 436.7 | ent). | | | | | | | |
| = | 1001. | | 0000 | | 1480 | 1991- | 0291 | | 9841- |
| 8 | 9 994 | = | | | | 1675. | | | 201. |
| 7 | 1,000 | | | | | | | 904 | 9- |
| 2 | 1991 | 929- | 5 | | | | | | 30. |
| 2 | 2001. | 7 | | | | | | | 181. |
| ٦ | - 282 | 468 | 7161- | | | 1282 | | | 721. |
| 7 | 0 00011- | 431 | 1521 | 1181. | 9021- | SP\$2 | | | 721- |
| | | | | | | | | | |
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| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| AXIAL | AXIAL FORCE (KN) | -36. | -359.5 | -387.3 | 7.3 | 7 | 371.7 | -357.2 | ĸ |
| | | 2.01.0 | 1.2 | A.2.A. | 7. | - | 777 | ¥44. | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P7-B

| į | Lead (B.M) | Strate | - Strate | Strate | | - Strain | Strate | Strate |
|-----------|------------------|--------|----------|----------|-----|-------------|--------|--------|
| 1 | | - | 7 | 3 | | | | _ |
| 7 | .307 | .20 | -125 | 56 | 391 | | .187 | |
| 7 | -40.5 | .37 | -165 | | | | | |
| 7 | 505 | -47 | 204 | | | | | 7.0 |
| 1 | -61.0 | -57 | .245 | | | | | |
| S | 7.70 | 43 | :1 | 132 | | | | |
| 9 | .70.5 | -71 | .316 | | | | | |
| 7 | -65.7 | π. | 345 | | | | | |
| - | 9.59 | -64 | | -60 | | | | |
| • | 9011. | ż | | | 547 | | | |
| 흳 | -121.7 | 101- | | | | | | |
| = | 7.221. | -110 | | 162 -610 | | | | |
| 2 | .1440 | -114 | -579 | | | | | |
| 2 | -158.5 | .122 | | | | | 240 | |
| 2 | 7.671. | 021- | 75 | • | | | | |
| 2 | .1850 | -135 | | | | | | |
| 2 | .1963 | .130 | | | | | | |
| = | -211.4 | .143 | 282 | | | | 8 | |
| = | -223.1 | -147 | 31 | | | | | |
| 2 | .173 9 | 971- | -736 | | 822 | | 2 | |
| 8 | -165.0 | 051- | | | | | | 51. |
| 1 | | | | | | | | |
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| † | † | | | | | | | |
| † | | | | | | | | |
| 1 | | | | | | | | |
| XIAL F | AXIAL FORCE (kN) | 9 | | 20.4 | | | | |
| | | | | | • | 41.1 | • | 41.0 |
| _ | | | | _ | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P7-B

| | 7.06. 6.02. 7.78. 7.78. 7.89. 9.89. 9.89. 7.121. 7.121. 7.121. 7.121. 7.131. | 23 23 37 41 44 44 44 47 66 66 | 100 110 110 110 110 110 110 110 110 110 | 25. 26. 27. 20. 20. 20. 20. 20. 20. 20. 20 | | | | 22 13 23 13 24 15 25 25 26 23 26 23 27 28 28 23 28 23 28 23 29 24 29 24 20 20 24 20 20 24 20 24 | 16 107 100 100 110 100 100 100 100 100 100 |
|---|---|--|--|--|--------------|-------------------|----|--|--|
| - 2 0 4 0 0 0 7 0 0 0 1 1 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 | 2002- 2002- 2003- 2004- | | | | | | | | |
| 2 2 4 4 2 9 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 205- 205- 207- 207- 201- 2011- | | | | | | | | |
| 0 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 202: 01:0 01:0 25:7: 26:0 20:1: 7:2: 7:2: 7:2: 7:2: 7:2: 7:2: 7:2: 7 | | | | | | | | |
| 4 0 0 7 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 010 07.7 080 080 011: 0112: 7 121: 7 121: 7 130: 7 | | | | | | | | |
| 0 0 0 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | -7.76 -7.85 -9.50 -11.00 -13.27 -13.27 | | | | | | | | |
| 0 | -78 5 -85 7 -95 9 -110 9 -121 7 -132 7 -156 5 | | | | | | | | |
| 10 6 6 7 | -85 0 -95 9 -110 9 -121 7 -132 7 -144 0 -150 5 | 57 69 7 80 80 80 80 80 80 80 80 80 80 80 80 80 | | | | | | | |
| 0 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | -85 9 -110 8 -121 7 -132 7 -144 0 -144 0 | 8 7 8 | | | | | | | |
| 9 01 11 12 12 13 13 13 13 13 13 13 13 13 13 13 13 13 | 110 9 7 121. 7 221. 7 2410 1440 | 8 2 8 | | | 982: 982: | | | | |
| 11 12 13 | 7 121 . 7 251 . 144 0 | 2 8 | | | 330 | | | | |
| 13 13 | 132 7 | 8 | | | 136 | | | | |
| 13 | 156 5 | | | | 186 | 520 584 053 | | | |
| 13 | 1565 | 8 | | | | 5620 | | | |
| | | | | | | 620 | | | |
| * | 7 671. | 91.0 | 52). | | 957 | | | | |
| 5 | 0.585 | 2 | | | 967 | 661 | | 117 | |
| ş | 8 | | | | 925 | 728 | | | |
| 12 | | 3 3 | | įį. | .576 | 786 | | 180 | |
| | | | | | -622 | | | | |
| | | | 989 | 3946 | 200 | | | 200 | |
| 2 | 922 | 35 | .743 | 202 | 17.9 | 100 | | | |
| 8 | .165.9 | 133 | -677 | Ual. | | | | | 356 |
| | | | | | Wr. | 673 | | 155 490 | |
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| | | | | | | | | | |
| AVIAL FORCE | 1 | | | | | | | | |
| MAL FORCE (RIN) | C (KK) | -34.2 | 2 | -35.6 | | 40.6 | 9. | 41.8 | |
| | 1 | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P8-A

| TES | T PANEL D (F | TEST PANEL D (FRONT DIAGONAL TOP | HALF | KLED OUTSIDE | Buckled Outside, Bottom Inside) | Ŷ | | Test Seri | Test Serial Mo. 33 |
|-------|------------------|----------------------------------|---------|--------------|---------------------------------|--------|--------|-----------|--------------------|
| į | Cond Cuto | Strain | Structo | 9train | Strafe | Strate | Strate | Strate | 41.6 |
| | | + | 2 | | | | | | _ |
| - | -336 | \$ | -323 | 80. | -269 | 116 | 21 | 107 | 9 |
| 2 | -51.5 | .57 | 497 | • | | 176 | u· | | |
| 3 | .703 | -57 | | | | | | | |
| • | 989- | 2 | 786 | -150 | | | | | |
| 9 | | 4 | | | | | | 355 | |
| 9 | 124.9 | 22 | 1281 | | -1083 | | | | |
| 7 | .140.6 | | | | | 595 | | | |
| • | .152.9 | | 1508 | | | | | | |
| • | 158.4 | 901 | .1660 | | | | | | |
| Ō. | .1633 | 126 | | | | | 60Ş- | 828 | |
| 1 | .168.6 | | 1842 | | | | 195 | | |
| 12 | 7.671. | 228 | | | | | 109 | 27.8 | |
| 13 | .1760 | 273 | -2136 | 192. | | | 759- | | 24 |
| 14 | -181.2 | 360 | -2383 | | | | 507- | | |
| 15 | -185.3 | | | | | | 757. | | |
| = | .100.0 | 678 | | 707 | .1163 | | | 8 | |
| 17 | .1863 | 750 | | 907- | 09-6- | | -962 | | 959 |
| • | 1997 | 751 | -2837 | 789- | | | 028- | | 9 |
| -10 | 2161. | 1007 | | 1096 | | | 096 | | 746 |
| 8 | 1924 | 1244 | 3000 | -1195 | | | 286- | | 92. |
| 21 | 1924 | 3121 | | 5771- | | | 218- | | 992. |
| 22 | | 5014 | 10200 | 19061 | 543 | | 680 | | 797. |
| 23 | | 27802 | -14414 | .2630 | 1670 | 1466 | -1045 | | 633 |
| 22 | | 28606 | .14328 | .2690 | 1725 | 1495 | -1086 | 1236 | 943 |
| 32 | | 31131 | 14017 | -2762 | 1830 | 1447 | -1023 | 1021 | 916- |
| 8 | 1106 | 32486 | 13863 | 2002 | 1913 | 1449 | -1022 | 1611 | -912 |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| AXIAL | AXIAL FORCE (KN) | -75.4 | 5.4 | 19 - | -65.1 | 13.5 | 5. | 12.5 | 6. |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN PG-A

| | TEST PANEL D (REAR DIAGONAL NOT | KEAK DIAGGRAL | | | | | | | |
|----------|---------------------------------|---------------|-------------|--------|----------|------------|--------|--------|--------|
| į | Load (MIN) | | at a second | Strate | - Strain | Otraile | Strade | Strata | 96rata |
| | | • | | 11 | 12 | 13 | 7 | = | • |
| - | 33.6 | 8. | 281- | 001- | 128 | \$ | 27. | | 35 |
| 2 | -51.5 | .76 | | | | | • | | |
| 3 | .70.3 | -07 | -431 | -211 | | | | | |
| • | 900 | 108 | | | | | | | |
| S | .112.0 | .100 | | | | | | | |
| • | -124.8 | | -803 | 350 | -615 | | | | |
| , | -140.6 | 27. | • | | | | | | |
| 9 | 152.0 | -42 | | | | | | | |
| • | -158.4 | -25 | -1285 | -430 | | 503 | | 320 | |
| Ō, | .163.3 | | 2381. | -430 | | | | | |
| : | -108.6 | 18 | 2291. | -440 | -915 | | -562 | | |
| 12 | 1.571- | | 1496 | 450 | -954 | | | | |
| 13 | 176.0 | | | -465 | | | | | |
| = | | 8 | | 187 | • | | | | |
| <u>=</u> | .185.3 | 114 | -1659 | -463 | | | | | |
| = | -106.9 | 144 | -1616 | - | -1042 | | | | |
| 17 | .186.3 | 196 | 1654 | 925- | | | 96.4- | | 594- |
| 2 | 7.001- | 223 | 1881 | 545 | | 209 | | | 27 |
| 9 | | 300 | 1713 | 989 | 1045 | 803 | | 956 | |
| 2 | | | 1742 | 9895 | 1046 | 215 | | | |
| 21 | 192.4 | | | -710 | 198- | 1014 | | | |
| 22 | .192.2 | | -2490 | -785 | 928- | 1043 | | | |
| 23 | 221. | | | 2211. | 11. | 1222 | • | | |
| 2 | .121.3 | | | .1167 | 21 | 1261 | .1275 | | |
| 22 | 1132 | | .2256 | .1216 | 141 | 1310 | -1343 | 107 | |
| 8 | 1106 | 1041 | .2248 | .1276 | 214 | 1365 | .1405 | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| AXIAL | AXIAL FORCE (KN) | -57.1 | 7.1 | 9 | -60.2 | N | 2.3 | 1.4 | * |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN PS-A

| i | Î | opene. | | 96.46 | Déreite |
|-------|------------------|--------|--------|--------|---------|
| | | | | 0.5 | |
| | 1 | | :01: | | 161- |
| | | | 276 | | |
| | 207. | 440 | 300 | | |
| | 98 | | | 987 | |
| | 9211. | | | | |
| | 9821- | | | | |
| | 7 | | | | |
| | 9 251. | 10001 | | 9121- | |
| | • 1884 | | | | |
| | £ £41. | | | | |
| | 1100 | | | | |
| | 1771. | | 627 | | |
| | 1780 | | | | |
| | 101. | | | 9971 | |
| | 18 | | | | |
| | -100.0 | ett). | | | |
| | 1003 | | | | |
| = | 1881 | | | | |
| | 2101. | 0861- | | | |
| 2 | A 591. | | | | |
| 21 | 1824 | ORZ1: | | | |
| 22 | 5231. | | | 1981 | |
| 7 | | 187. | | 2001- | |
| 2 | | | | 1015 | |
| ٤ | | 100 | | 058- | |
| - | 100 | 986 | 200 | -012 | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| | | | | | |
| AXIAL | AXIAL FORCE (KN) | -24 | -248.1 | -246.6 | 6.6 |
| | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN P8-B

| TES | ST PANEL D (F) | TEST PANEL D (FRONT DIAGONAL TOP H | 7 | BUCKLED INSIDE) | | | | Test Re- | Test Serial No. 18 |
|-------|------------------|------------------------------------|--------|-----------------|--------|--------|---------|----------|--------------------|
| į | Leed (RIV) | Strein | Strain | Strain | Strate | Strain | Strain. | Strate | Dêrnên |
| | | | - | 7 | 7 | | , | | • |
| | .34.6 | -286 | 85 | -273 | .61 | 69- | 151 | 85- | 145 |
| 14 | .540 | 247 | 7. | 927 | 8 | -80 | | | |
| | .74.9 | 197 | | -567 | .103 | | | | |
| | 986 | 887. | 001. | 757. | .113 | | | | |
| - | 5 -1153 | 998- | | .837 | -112 | | | | |
| | 1361. | 9811. | | -1127 | | | | | |
| | 7 | 1514 | | -1323 | | 746. | | | |
| | 169.6 | 5201- | | .1409 | | | | | |
| • | 175.4 | -2084 | | | | | | | |
| 9 | 181.2 | .2180 | | 1434 | | | 998 | | |
| = | | 2282 | | .1417 | | | | | |
| 12 | 1981 | -2374 | 211 | -1407 | -208 | | | | |
| 13 | .188.2 | -2506 | | 1368 | | | | | |
| 7 | -190.2 | 3865 | 344 | -1273 | | | | 2 | |
| 15 | 1920 | .2780 | | -1106 | | | | | |
| 16 | 7 281. | .2878 | 603 | <i>811</i> . | | | | | |
| 17 | 9.191. | 1926- | | -351 | • | | | | |
| = | 191.6 | -3474 | | -206 | | | | | |
| 10 | 1920 | 3002 | 1349 | 43 | -1444 | | | | |
| 8 | .192.3 | -4483 | 1702 | 277 | .1630 | | | | |
| 21 | .193 0 | .5253 | | 431 | | | | | |
| 77 | 6.281. | 7414 | 3305 | 612 | | 585- | | | |
| 23 | | 7570- | 7957 | 726 | 1961- | 267 | | | |
| 24 | | .12086 | 7505 | 828 | -2076 | -560 | | | |
| æ | | | 1199 | 970 | | -543 | | | |
| 8 | | 15001 | 1.08 | 1066 | .2200 | -534 | | | |
| 2 | | | | 1165 | -2461 | 975 | | | |
| 2 | | -21199 | 11946 | 1220 | -2510 | -520 | 1455 | | 1841 |
| 8 | | .22086 | 12558 | 1279 | -2565 | -521 | | | 1944 |
| 8 | | | 11826 | 1536 | 9222- | .775 | | | |
| 31 | 1138 | 20056 | 11904 | 1517 | -2205 | .775 | | | |
| AXIAL | AXIAL FORCE (HN) | -82.0 | 2.0 | Ÿ | -62.9 | 121 | 21.0 | | 9: |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN PS-B

| 1 | | | Shoule | 1 | | | | | | |
|--------|------------------|--------|--------|----------|-------|------|-------|----------|----------|--------|
| | | | | | | | 1 | | | Otrada |
| 1 | 346 | 18 | | | | | | * | = | |
| 2 | 0.75 | | 8 | | | | 2 | \$5 | ş | - |
| 6 | | | | | 8 | | 8 | <i>"</i> | 10 | 12 |
| | 4 | | | | | | | -114 | -92 | 35 |
| | | | | 427 | | | | .150 | 151- | 3 |
| , | | | | | | 151 | | -214 | 971. | 911 |
| | | | | | | 216 | | -281 | .240 | 176 |
| | 1366 | 211: | . 186 | 2361- | | | | :863 | 716 | |
| | | .1233 | 190 | 1491 | 83 | | | ş | 3 | 70 |
| • | | | 081- | 1556 | 29 | | | 105 | , 5 | 3 |
| 9 | 101.2 | 1344 | 281. | .1687 | 29 | | | 3 | 1 | R |
| = | 1834 | 1367 | .100 | 1745 | | | | 5 | | Ì |
| 12 | 1981 | 1362 | | | | | | | 3 1 | * |
| 2 | -1862 | -1415 | | | 32 | | | 5 3 | S) C | Š |
| = | 2.081- | -1462 | -166 | | 2 | 7 | | | \$ | |
| 2 | -102.0 | .1465 | 146 | 9901- | Į. | | | | | |
| 2 | 192.7 | 1486 | .133 | | 103 | | | 200 | | |
| F | 9101 | . 1480 | | | 901 | | | 200 | R | //2 |
| 2 | .191.6 | -1482 | | | 801 | | | | 3 1 | 8 |
| 2 | .182.0 | .1513 | | 5281. | 5 | | | 20 1 | <u>.</u> | 35 |
| 2 | .192.3 | 1544 | 2 | 5081- | 2 | | | 9/9 | 00 | 782 |
| 21 | -193.0 | 7951- | 19 | 0981 | 3 6 | 8 | | 805 | 75 | ž |
| 22 | 192.9 | 5085- | | 9250 | 10 | A S | | 988 | -677 | 9 |
| 23 | .192.3 | 0181- | | 2700 | 9 | 1023 | | -1016 | 98 | 978 |
| 24 | .162.6 | CA81. | | 773 | 77 | 1076 | | -1060 | -985 | 1032 |
| 22 | 9 191. | 3141 | | | S. | 1143 | | -1113 | -1006 | 1100 |
| 8 | \$ 191. | | | 13/4 | 728: | 1222 | | 8 | 1001 | 1180 |
| 2 | 1 69 | 900 | | 1121- | -448 | 1201 | .1203 | S | .1070 | 1237 |
| 1 | | A/AL- | 1 | 296 | -614 | 1322 | 9021- | 90 | -1088 | 1282 |
| 1 | | | 28 | 4 | -692 | 1335 | -1194 | 3 | .1050 | 1319 |
| 1 | 1 BB . | 2130 | 8 | -712 | 087. | 1332 | 21172 | 22 | -1045 | 1329 |
| 7 | 900 | 7887 | 1524 | 6 | .1037 | 1263 | .1237 | 37 | -1048 | 1326 |
| | | NO. | 1487 | Si | 1005 | 1277 | | 23 | -1036 | 1308 |
| AXIALF | AXIAL FORCE (KN) | -62 | 2 | -68.5 | .5 | • | -1.9 | | -1.5 | |
| 1 | | | | | | | | | \mid | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN PS-B

| į | | | | | |
|----------------|------------------|---------------|--------|-----------|-------|
| | Lond (max) | | 1 | - Section | 49040 |
| | 1 | 5 | | | |
| | 2 +40 | | | | |
| | 3 -74.1 | | | | |
| | 94 | | | | |
| | 6 111. | | | | |
| | 181. | | | 48 | |
| | A 481. | | | | |
| | 9 | | | 9111- | |
| | 141: | | 22. | | cm. |
| | 101. | | | (82) | |
| | | | | | |
| | | | 282 | (21) | |
| | | | | 940:- | 445 |
| | | | | 0001: | |
| | | | | -1877 | |
| | | | | 98.1. | 4 |
| | | 701. | | ¥. | ** |
| | | | | 1301 | |
| | | | | 181. | 4 |
| | | | | 0091- | |
|] | | | | 1991 | |
| | | 2001- | | 1191- | |
| Ţ' | | | | 1191- | |
|] | | | | 991. | |
|] ' | | 0081: | | 0191. | £. |
|] ' | | | | (34) | 26 |
|] | | | | 891 | |
|] ' | , a . | 0891 : | 2 | 9861- | ¥ \$ |
|] | | | | 2261- | * |
|] [*] | 7 | | 8 | 9761- | 140 |
| Ī | | | | 3 | 3 |
| | 1 | | 989 | 207- | * |
| AMA | AXIAL FORCE (KN) | -28 | -263.8 | -252.4 | |
| | | | | | |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN S1-A

| 2 | WEL C (F | PANEL C (FRONT DIAGONAL) | JONAL) | | | | | | | | Test Serial No. 6 | 6 0. 6 | |
|--|-------------------|--------------------------|--------|--------|--------|-----------|------------|--------|--------|-------------|-------------------|----------------------|--------|
| į | Load kN Strain | Strain | Strain | Strain | Strain | Strain | Strain | Strain | Strain | Strain | Strain | Strain | Strain |
| | | • | 2 | 9 | • | 6 | • | 7 | , | • | 10 | + | 12 |
| | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | Ö | 0 | 0 | 0 |
| | 10 | 30 | -230 | -152 | -130 | -216 | 46 | -208 | 44 | 70 | -318 | 89- | -144 |
| | 3 | 52 | -552 | | -262 | -492 | -10 | -466 | -28 | 224 | | -104 | -286 |
| 1 | 25 | 132 | -730 | 400 | -326 | -648 | 29 | -800 | 24 | | | -104 | -348 |
| | 30 | 230 | -924 | 470 | -382 | -626 | 144 | -738 | 25 | | • | -100 | 410 |
| | 35 | 364 | -1142 | .546 | -440 | -1028 | 256 | -884 | 124 | 76 9 | -1362 | \$ | 470 |
| | 7 37.5 | 434 | -1242 | -578 | 468 | -1132 | | | 148 | | | 97- | 87 |
| | 40 | 532 | -1394 | -624 | 504 | -1268 | 420 | -1012 | 182 | | | 8 | -528 |
| | 42.5 | 909 | -1500 | 959 | -530 | -1376 | 492 | -1070 | 200 | 009 | | 99- | 999- |
| 9 | 0 45 | 702 | -1640 | 989 | -560 | -1520 | 594 | -1130 | 222 | 798 | | 97 | -580 |
| Ξ | 1 47.5 | 612 | -1788 | -736 | -590 | -1684 | 724 | -1176 | 230 | 878 | 0691- | 85 | -614 |
| 12 | 8 | 1030 | -2162 | -830 | -66 | -1920 | 926 | -1210 | | | | | |
| 13 | 33.3 | 2926 | 4874 | -1540 | .1244 | -2036 | 1278 | -1762 | 796 | 2380 | -3756 | 100 | -700 |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| AXIAL. | AXIAL. FORCE (kN) | -14.1 | 1.1 | -19 | 6 | 1. | -12.6 | | | | | | |
| SE CONTRACTOR DE | MOMENT(N.m) | 62.7 | .7 | -3.3 | 3 | 57.1 | 1 : | | | | | | |
| | | | | | | | | | | | | | |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN S1-A

| PANEL | PANEL C (REAR BIAGONAL NOT | DIAGONA | - 1 | DOCKLED) | | | | | | | Test Serial No. 6 | ¥ o. 6 | |
|------------------|----------------------------|-------------|--------|---------------|------|--------------|-----------|-----------|-----------|--------|-------------------|----------------------|--------|
| į | Less KN | Strain 1 | Strate | Strain rie | | Strain 24 | Strain 22 | Strain 25 | Strain 21 | Strain | Strain | Strain | Scrats |
| | | | | | 3 | | 1 | | 5 | 87 | 8 | 72 | 2 |
| | 0 | 9 | œ. | -18 | Ġ. | -0 | -61 | 0 | 8 | 22 | 0 | 0 | -13 |
| 2 | 10 | .78 | 184 | -152 | -97 | -189 | -130 | -158 | 99- | • | 176 | -130 | 411- |
| | 20 | -70 | -467 | -326 | -182 | -436 | 191- | -384 | 8 | | | -302 | .218 |
| 1 | 25 | -12 | 4 | 412 | -207 | -581 | -138 | -536 | 78 | | | .388 | -243 |
| 9 | 30 | 103 | • | -493 | -211 | 757. | -73 | -702 | ę | | -679 | 8 | 250 |
| 9 | 35 | 256 | -11 | -570 | -200 | 096- | 36 | 106- | 8 | | | 280 | -240 |
| 7 | 37.5 | 340 | | -600 | .187 | -1057 | 3 | 1000 | 201 | | | 930 | -226 |
| 9 | 40 | 447 | -1453 | -644 | -172 | -1190 | 172 | -1129 | 253 | | -1459 | 288 | .213 |
| 3 | 42.5 | 528 | | -672 | -157 | -1281 | 230 | -1219 | 324 | | .1570 | 127. | -180 |
| 10 | 45 | 619 | -1703 | -710 | -140 | -1390 | 305 | -1334 | \$ | 695 | -1708 | 76.8 | 184 |
| 11 | 47.5 | 707 | -1639 | -743 | -118 | -1495 | 378 | -1432 | 8 | 802 | -1859 | -813 | -167 |
| 12 | 50 | 803 | -1976 | em. | -90 | | | | | | | | |
| 13 | 33.3 | 936 | -1436 | -578 | 0110 | 086- | -108 | -1138 | 393 | 550 | .1363 | 755- | 1.0 |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| AXIAL FORCE (KN) | CE (KN) | -14.8 | .8 | -11 | _ | | | | | | | | |
| MOMENT(N.m) | (u | 9'99 | 6. | 13.6 | 9 | | | | | | | | |
| | | | | | | | | | | | | | |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN S1-A

| <u> </u> | | State of the state | | | | | | Test Serial No. 6 | |
|------------|-------------------|--|-----|------|--------|--------|--------|-------------------|--------|
| į | 3 | | | | Otrain | Strain | Strain | Strain | Berein |
| Ľ | | | - | = | 10 | 230 | 96 | 7 | 5 |
| | | | 0 | 0 | 0 | 0 | 0 | | |
| | | -70 | 8 | 8 | 3 | 75. | | | |
| 1 | | -175 | 234 | 09- | 234 | | | OS. | \$ |
| | \$2 | .234 | 312 | | 318 | | 140 | -102 | 143 |
| 9 | 30 | -283 | 400 | 471. | | | 208 | 8 <u>5</u> - | 211 |
| 9 | 35 | | | | 9 | | 288 | -230 | 306 |
| 7 | 37.5 | | | | 0.00 | | 412 | -310 | 426 |
| 8 | 9 | | | ē. | 200 | 330 | 466 | .343 | 463 |
| • | • | | | 82 | 630 | -372 | 544 | 086- | 727 |
| 5 | | | | 85 | 674 | -306 | 785 | 4.7 | |
| | | 455 | | 985 | 25 | 428 | 1 | | 010 |
| | | 478 | 754 | -370 | 92 | 694 | | OST I | 682 |
| 12 | 2 | 470 | | 774 | | | | 712 | 742 |
| 13 | 33.3 | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| 10124 | 1000 | | | | | | | | |
| | MANUEL FUNCE (RM) | 0.8 | | 2.6 | - | | · | | |
| MOMENTAN.m | | | | | | | | | |
| | | -36.3 | 5 | -38 | | | | | |
| | | | - | | | - | + | - | |
| | | | | | | | | _ | |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN 52.A

| | 7 1 1 1 | THE A (FROMT DIAGONAL BUCKLED | | - | H BOTTO | | | ! | | | | | |
|-------------------|-----------|-------------------------------|------|------------|---------|--------|--------------------------|--------|----------|--------|----------------|--------|--------|
| - | | Sinis | | 1 | | | TO INSIDE AND TOP INSIDE | | | | Tonk Day | | |
| | | | | - | 4 | Strate | Strain | Strade | Strain | Strain | est serial No. | Ž0.4 | |
| | 10 | 100 | | | | | 8 | | _ | | | Strain | Strain |
| | 200 | | | | 25. | -37 | -102 | | 9 | | 2 | = | 12 |
| | | | | 18 -187 | -114 | -62 | | | | 124 | -58 | 95- | ٤ |
| | 3 | 418 | 22 | 2 -276 | 176 | | | | -12 | -251 | | | 77 |
| | | -582 | 35 | | | | | | -18 -392 | -388 | | | 67. |
| | 8 | -754 | 55 | | | | | | 36 -565 | 565 | | | 386 |
| 9 | 8 | -690 | 98 | | | | 584 | 8 | -765 | | | | 467 |
| 7 | 70 | -1040 | 7. | | ZGC. | -148 | -668 | 190 | 986 | | | -142 | -571 |
| • | 75 | 97.07 | | | Ş | -190 | -790 | 432 | | | 10 | -174 | 456 |
| L | 1 | 9/01- | 97 | 969 | -421 | -222 | | 197 | | 1280 | 242 | -210 | 730 |
| = | | 0801 | \$ | | 431 | -240 | | 8 | | 1417 | 320 | -232 | 762 |
| | | 1107 | 22 | | 927 | | | 202 | -1486 | -1480 | 386 | 243 | 701 |
| = | 82.5 | .1110 | 10 | | | 797- | -814 | 586 | -1614 | 1506 | 1 | 783 | -750 |
| 12 | 65 | 1007 | 1 | | 8 | 900 | 909 | 646 | | | 794 | -258 | -770 |
| 13 | 87.5 | 900 | | | 476 | -370 | -782 | 77.6 | | | 493 | -274 | -772 |
| 71 | 8 | 8 | -82 | 756 | 160 | € | CAT. | 8 | | | 602 | -292 | 111. |
| | 2 | -1048 | -146 | -758 | 492 | ACS. | 1 | | 1980 | 1950 | 706 | -310 | 17.7 |
| | 82.5 | 930 | -290 | -726 | cos | 1 | 200 | 1064 | -2164 | -2106 | 820 | 2 | |
| 9 | 95 | -512 | -657 | ş | | 78/ | \$ \$ | 1490 | -2798 | .2562 | | By. | 7/62 |
| 17 | 63.3 | 72. | 1 | | 8 | -1316 | 122 | 2250 | 7357 | 2002 | 720 | .358 | -735 |
| - - | | | | R | ž | -3326 | 2260 | 3832 | | nor: | 1824 | -432 | -712 |
| | + | | 1 | | | | | | 7 | 4342 | 3120 | -632 | -220 |
| AXIAL FORCE (ILN) | ACE (ILN) | -14.8 | | -12.3 | | -15.1 | |] | | | | | |
| MONENT(N.m. | .E. | 6 | | | 1 | | | 7.71- | , | -15.9 | | -14.5 | |
| | | 8.7 | | 8 . | | 28.9 | - | 93.8 | œ | 000 | | | |
| | 1 | | | | | | 1 | | | 90.9 | | 9.6 | |
| | | | | | | | | | | L | | | |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN \$2-A

| | Strate | | | | Strain Name | _ | _ | Strain | | | _ | Strain. |
|------------------|---|--|---|---|--|--|--|--|---|---|--|--|
| | 47 | • | • | 22 | 21 | 22 | 23 | 24 | 25 | | 27 | 22 |
| 5 | | -22 | 95. | 111- | 96- | -82 | 46 | . | -148 | 60 | 2 | -90 |
| 8 | | 47 | -140 | -166 | £9- | .188 | 8 | -200 | .340 | 16 | -117 | -202 |
| క | | -87 | -192 | -242 | .72 | -297 | -140 | -300 | -504 | 22 | -175 | -305 |
| 9 | | 8 | 172- | 338 | -62 | 434 | -164 | -404 | -678 | 8 | -230 | 400 |
| S | | 8 | -333 | 436 | -12 | -588 | -238 | 496 | -854 | 46 | -292 | 909 |
| 8 | | 28 | 980 | -536 | 76 | -774 | -310 | -568 | | 2 | 350 | -587 |
| 22 | | 208 | 8 | -676 | 308 | -1054 | 484 | -558 | | -20 | 400 | ğ |
| 75 | | 336 | 402 | -738 | 470 | -1207 | -582 | -486 | | 96 | 414 | .740 |
| 77.5 | | | 386 | -770 | 924 | -1280 | -646 | -444 | | -124 | 410 | 157- |
| 8 | | | | -628 | 726 | -1428 | -778 | -340 | | -208 | 408 | 267. |
| 82.5 | | | | 96 | 954 | -1528 | -870 | -259 | | -274 | 704 | -610 |
| 95 | | | -328 | 066- | 7255 | -1756 | -1062 | -30 | | -428 | -380 | -852 |
| 87.5 | | | -296 | -1008 | 1568 | -2062 | -1236 | 250 | | -596 | .337 | 988- |
| 8 | 767- | | | -1122 | 2060 | -2478 | -1360 | 576 | | 794 | -265 | .920 |
| 92.5 | | | | -1316 | 2872 | -3150 | -1492 | 1000 | | -1042 | .150 | -955 |
| 2 | | | 336 | 9971- | 2690 | -3622 | -1606 | 1386 | 8 | -1210 | -54 | -972 |
| 53.3 | | | 2967- | -2496 | 0980 | -3202 | -2326 | 3228 | | | 416 | 446 |
| | | | | | | | | | | | | |
| AXIAL FORCE (KN) | 23 | 3.8 | -27 | 2.7 | Ö | 9 | -5 | 80 | 7 | 4.3 | 7 | -13 |
| MOMENT(N.m) | ě | 5.4 | 22 | 3 | -14 | 1.6 | 9 | 7 | ž | 5.9 | 18 | 18.5 |
| | | | | | | | | | | | | |
| | 10 10 20 30 30 30 40 60 60 60 60 60 60 60 60 60 60 60 60 60 | 10 -50 170 | Strates Strates 10 12 12 12 12 12 12 12 | Merain Strain Strain 148 149 140 <t< td=""><td>N Strain Strain Strain Strain Strain 20 17 20 17 20 17 20 17 20 17 20 17 20 17 20 17 140 140 170 140 170 140 170 140 170 140 170</td><td>Name Strain Strain</td></t<> <td>Month Strain Strain<!--</td--><td>Month Strain Strain<!--</td--><td>Modernia Strain Strai</td><td>Montage Serration Serration</td><td>Montalization Securine Sec</td><td> Secretary Secr</td></td></td> | N Strain Strain Strain Strain Strain 20 17 20 17 20 17 20 17 20 17 20 17 20 17 20 17 140 140 170 140 170 140 170 140 170 140 170 | Name Strain Strain | Month Strain Strain </td <td>Month Strain Strain<!--</td--><td>Modernia Strain Strai</td><td>Montage Serration Serration</td><td>Montalization Securine Sec</td><td> Secretary Secr</td></td> | Month Strain Strain </td <td>Modernia Strain Strai</td> <td>Montage Serration Serration</td> <td>Montalization Securine Sec</td> <td> Secretary Secr</td> | Modernia Strain Strai | Montage Serration Serration | Montalization Securine Sec | Secretary Secr |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN \$2.A

| | Strate | | Strain | | | Strain | _ | |
|------------------|--|---|--|--|---|---|---|---|
| | \$ | 7 | | 16 | 82 | 8 | 31 | R |
| 2 | 7.4 | 16 | 98 | 2 | 9 2 | 16 | 9 | 8 |
| | | 92 | | 7 | 166 | 8 | 140 | 30 |
| | | 8 | | 9 | 244 | 52 | 212 | 3 |
| \$ | | * | | 8 | 344 | 8 | 782 | 120 |
| 50 | | 23 | | 12 | 418 | 88 | 376 | 144 |
| | | | | 20 | | 106 | | 162 |
| 2 | | | | 16 | | 134 | | 196 |
| | | | | | | | | 21 |
| 1 | | | | | | 156 | 909 | 22 |
| 96 | | | | | | | 634 | 23 |
| 8 | | | | | | 180 | 878 | 252 |
| 12 85 | | | 959 | 70 | | 204 | 674 | 27 |
| 13 87.5 | | | 000 | | | 226 | 769 | 306 |
| | | | 914 | | | 268 | | 36 |
| 9 | | | | | | 330 | | 416 |
| | | 282 | | 178 | | 396 | 792 | 757 |
| 53.3 | | | 832 | | 91.2 | 116 | 610 | 19 / |
| | | | | | | | | |
| AXIAL FORCE (IN) | 15 | * 3 | 11 | 5.0 | 16 | 3.0 | 16.2 | 7.3 |
| MOMENT(N.m) | -12 | 6 | 1- | 6.7 | 6. | 6. | 1.0 | - |
| | | | | | | | | |
| | 10 20 20 30 40 40 60 60 60 60 60 60 60 60 60 60 60 60 60 | 96rates 13 20 20 20 20 20 40 50 60 60 60 60 60 60 60 60 60 6 | 96 bit of the second of the se | 20 13 14 20 156 28 1 20 156 28 1 30 226 36 2 40 332 46 3 50 436 74 5 60 528 74 5 7 666 112 7 7 70 132 7 86 76 134 9 86 826 154 9 86 826 216 9 86 826 216 9 85 826 216 9 86 826 226 10 85 750 206 9 86 826 206 9 86 826 206 9 86 86 9 9 86 86 9 9 86 86 9 | Strate Strate< | Secretion Secretion <t< td=""><td>Specialist Specialist Specialist 14 15 15 20 74 16 20 17 16 20 17 16 20 17 16 20 17 16 20 17 16 16 20 16 20 16 20 16 20 16 20 <th< td=""><td>100 110</td></th<></td></t<> | Specialist Specialist Specialist 14 15 15 20 74 16 20 17 16 20 17 16 20 17 16 20 17 16 20 17 16 16 20 16 20 16 20 16 20 16 20 <th< td=""><td>100 110</td></th<> | 100 110 |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN 52-B

| PANE | IL A (FRO | PANEL A (FRONT DIAGONAL) | HAL) | | | | | | | | Test Serial No. 8 | 1 0.8 | |
|-------------|------------------|--------------------------|--------|--------|--------|--------|---------|--------|--------|--------|-------------------|-------------------|--------|
| á | Land kN | Strain | Strain | Strain | Strain | Strain | Strain. | Strain | Strain | Strain | Strain | Strain | Strate |
| | | 1 | | 2 3 | • | 5 | • | 7 | | 9 | 10 | 11 | 12 |
| | 9 | -202 | 90 | -82 | 9 | 10 | -140 | 12 | -147 | -175 | 38 | 01 | -80 |
| 2 | 8 | 410 | 128 | į. | .126 | 10 | -284 | 28 | -304 | -350 | 28 | 63 | -145 |
| 3 | 8 | -616 | 190 | -244 | .166 | 25 | -426 | 60 | -470 | -528 | 132 | -123 | -236 |
| 7 | 40 | -900 | 254 | | -254 | 35 | -560 | 105 | -844 | -705 | 186 | -162 | -310 |
| \$ | 8 | 066- | 316 | 380 | -326 | 54 | -700 | 166 | -638 | -896 | 254 | -205 | -372 |
| 9 | 90 | -1150 | 360 | | -396 | 99 | -820 | 252 | -1040 | -1086 | 330 | | 432 |
| 1 | 70 | -1293 | 368 | 14 | 474 | \$ | -925 | 370 | -1276 | | 433 | | 472 |
| Ą | 80 | -1390 | 378 | 30- | -566 | -18 | 096- | 555 | -1578 | | 578 | | -500 |
| î | 88 | -1414 | 338 | 1 -496 | 420 | -82 | -870 | 698 | -1780 | -1718 | 999 | 00 1 - | -800 |
| 10 | 67.5 | -1390 | 308 | 37 | -652 | -144 | 076- | 826 | -1880 | -1625 | 772 | 420 | 404 |
| 1 | 8 | -1360 | 250 | 9 | -684 | -244 | -966 | 1038 | -2075 | -1980 | 885 | -445 | -468 |
| 12 | 91.25 | -1258 | 154 | ¥ | .700 | .370 | -745 | 1220 | -2305 | -2065 | | -462 | -448 |
| 13 | 92.5 | -1127 | 28 | | -706 | .580 | -510 | 1600 | -2745 | -2203 | 1220 | 0 91- | -380 |
| 7 | 93.75 | -610 | -155 | | -670 | -854 | -174 | 2030 | -3180 | -2368 | 1476 | 909- | -340 |
| 15 | 95 | -450 | -445 | 5 -268 | -595 | -1278 | 444 | 3000 | -4190 | -2880 | 2125 | 919 | 08- |
| 16 | 96.25 | -157 | -796 | | -575 | -1733 | 680 | 4025 | -5236 | -3290 | 2500 | -520 | -20 |
| 17 | 97.5 | | | | | | | | | | | | |
| 18 | 25.25 | 640 | -1166 | -514 | 195 | -5650 | 3660 | 6920 | .7070 | -4540 | 4350 | -650 | 490 |
| AXIAL F | AXIAL FORCE (HN) | -13.6 | 3.6 | -14 | 4.2 | -1; | -13.3 | -13.7 | 1.7 | -4: | -13.0 | 7 | -11.4 |
| MOMENT(N.m) | IT(N.m) | 35.2 | 3.2 | 2. | 2.5 | 47 | 17.9 | 48 | 49.8 | 48 | 48.8 | | 2 |
| | | | | | | | | | | | | | |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN 52-B

| PANEL A | PANEL A (REAR DIAGONAL) | AGONAL) | | | | | | | | | | | |
|------------------|-------------------------|---------|--------|--------|---------------|--------|-------|-------|--------|--------|--------------------|-------------|--------|
| 2 | Load kiv | _ | Strain | Strain | Strain | Strain | 4 | | | | Test Serial No. 10 | 6. 10 | |
| • | | | = | = | 20 | _ | 22 | | Strain | Strain | Strain | Strain | 1 |
| | 01 | 101- | -35 | -52 | -82 | 4 | 1 | | \$ | 2 | 200 | 27 | |
| 2 | 2 | -232 | -60 | -105 | 180 | | * | 95 | -74 | -130 | 9 | | |
| - | 30 | -372 | c7. | | 3 | 77. | -206 | -109 | -165 | 176- | | | -110 |
| 7 | 0* | 400 | | | -281 | 28 | -326 | -170 | 236. | | | \$ | -226 |
| in | 2 | 900 | 2 | 160 | ş | 8 | 455 | 21.6 | 5 | 410 | -25 | -130 | -336 |
| | 3 8 | R | \$ | -222 | -501 | 3 | 818 | | 255 | -545 | .30 | -178 | 436 |
| | 3 | -883 | 9 | -236 | -622 | 130 | 30 | | 426 | -874 | S. | -234 | . K3.c |
| + | 20 | -1138 | 102 | -224 | 787. | 1 | 3 | 412 | 997 | -779 | 8 | 200 | |
| • | 8 | -1517 | 334 | 160 | 9 | OC S | -1068 | 575 | 420 | -841 | 271- | | 929 |
| 0 | 32 | -1791 | 3 | ā | | 200 | -1496 | -902 | -218 | 977- | 376 | 0/5 | 989 |
| ē | 87.5 | -1989 | 718 | 1 | 2 | 1002 | -1890 | -1204 | 9 | A2A. | | 77. | -716 |
| = | 8 | | | | 1211- | 1317 | -2377 | -1445 | 33. | | 9/6 | 929 | -702 |
| 5 | | | 2 | 7 | -1181 | 1840 | 2260 | | | | 744 | -558 | -682 |
| | 67 | -2302 | 1020 | * | -1216 | 1826 | 100 | | | 282 | -032 | -682 | 777 |
| 2 | 92.5 | -2410 | 1150 | 140 | -1248 | 3066 | | -1846 | 728 | 021- | -1067 | 9 | |
| 2 | 93.75 | -2495 | 1233 | 167 | 1280 | 3 6 | -3323 | -1966 | 923 | -14 | 191 | 9.4 | 710 |
| 15 | 88 | -2662 | 1397 | 223 | 98.9 | 3 | 3430 | -2100 | 1086 | 100 | -1295 | 1 | 9/6- |
| 92 | 86.25 | -2060 | 1570 | 252 | | e : | 3809 | -2349 | 1393 | 319 | -1403 | 3 | 920 |
| 17 | 97.6 | -2986 | 1672 | 284 | | à i | -3700 | -2506 | 1865 | 525 | -1852 | \$. | 8 |
| 2 | 25.25 | -2361 | 1593 | -162 | 45 | 3187 | 3849 | -3073 | 1970 | 727 | | 700- | 7 |
| AXIAL FORCE (KN) | = (KN) | -16.0 | _ | 111. | | 10101 | 010 | 3413 | 2676 | 2241 | -3076 | 986 1986 | \$ 5 |
| MOMENT(N.m) | - | | + | | + | -13.7 | | -14.7 | | -15.5 | <u> </u> | -15.5 | |
| | | 60.9 | | 24.7 | | | | | | | 1 | | |
| | | - | - | | + | 4.10 | | 44.8 | | 12.9 | | • | |
| | | | | 1 | $\frac{1}{1}$ | | _ | _ | | } | + | 7.7 | |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN 52-B

| | A (FRONT AND | PAMEL A (PRONT AND REAR TENSION DIAGONAL) | ABONAL) | | | | | Test Seriel No. e | |
|--------------|------------------|---|---------|--------|----------|--------|----------|---|-----|
| ź | Leadth | Strain | Strain | Strain | Strate | Serate | Series - | OF STATE OF | |
| | | 13 | 1 | | | _ | | | |
| | 1 10 | 101 | 4 | | | | 8 | 20 | 22 |
| .4 | 20 | | | | | | 28 | 98 | 28 |
| | 30 | | | | 9 | 134 | 88 | 136 | 3 |
| | 1 | | | | 0 | 208 | 100 | 212 | |
| | | | 24 | 440 | 16 | 276 | 171 | | |
| 1 | 200 | 929 | 98 | 554 | 42 | 472 | | | 132 |
| | 90 | 634 | 98 | 959 | | | 8 | | 20 |
| | 70 | 732 | | 758 | | 200 | 228 | | 196 |
| | 90 | | | 296 | | 3 | 270 | 512 | 234 |
| _ | 2 | | | 700 | | 574 | 326 | 596 | 280 |
| ٩ | | | | | | 614 | 390 | 040 | 316 |
| - | | 986 | 218 | 822 | 206 | 636 | 70. | *** | |
| = | 8 | 922 | 234 | 976 | | | | B | 32 |
| 12 | 91.25 | 87.8 | | 98 | | | 5 | 8 | 366 |
| 13 | | 963 | | | 244 | 676 | 452 | 718 | 368 |
| 71 | ľ | 2 | | D/8 | 38 | 888 | 476 | 724 | 90* |
| | | | | 976 | 284 | 200 | \$ | 730 | 254 |
| 2 | | 286 | 380 | 805 | 38 | 718 | CEA | | 100 |
| 2 | 86.25 | 1006 | 416 | 200 | C77 | 728 | | 2 | 407 |
| 17 | 97.5 | | | | | 8 | 9/0 | 98/ | 900 |
| 16 | 54.54 | 920 | \$ | 748 | 150 | 000 | | | |
| | | | | | 3 | 90% | 622 | 462 | 200 |
| WINT I | AXIAL FORCE (KN) | 13 | 13.6 | 13.8 | 9 | 13.8 | • | 13.4 | * |
| MONIENT(N.m) | (M.m) | -13.5 | 90 | 244.2 | | | | | |
| | | | | | | 7. | | 6.5 | - |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN 52-C

| | | | | 1 | Strain | Strate Strate | | Test Se | Test Serial No. 23 |
|---------|------------------|-------|-------|-------|--------|---------------|------|-------------------|--------------------|
| | 23.9 | | | ~ | | | | Marale alerate | at a second |
| 2 | | | | | 6. | 176 | | - | |
| 3 | | | | | 950 | | | 257 | |
| 4 | 430 | | | 518 | .73 | | | 120 | |
| \$ | | | | 616 | | | | 395 | |
| 8 | | | .778 | | | | | 663 | |
| ^ | | | | | | | , | | |
| 1 | 97.4 | 150 | | | 922 | 9 | | | 35 |
| 1 | 907. | 9 | | | 424 | | | | 637 |
| • | .742 | | | 2 | 969 | | | 198 | |
| 2 | .77.6 | 234 | | | | | | 215 | |
| = | 9.06 | 2 | 221 | 33 | | | 7 | | |
| 22 | 200 | 2 | 727 | -26 | | | | 783 250 | |
| 5 | 242 | 2 2 | .1233 | | 8 | | 9 | | |
| = | -872 | 1 | 1207 | | | | • | | - |
| 5 | -804 | 5 | 1371 | | | | 3 | 200 | |
| = | -027 | | :1453 | | | | 83 | | |
| 17 | 1.09. | | -1622 | 22 | 16.5° | | 8 | | |
| 92 | 8.0 | 8 3 | 1480 | -18 | | | 2 | | |
| 9 | c 18. | * | 1410 | 2 | 6000 | | 28 | | |
| 8 | A CS | 8 | 92/1- | 1085 | 1076 | | 888 | | |
| 21 | 100 | /6/ | -1622 | | | | 25 | 986 | 100 |
| 2 | 200 | 789 | .1970 | | SON? | | 780 | | 873 |
| 2 | c i | 756 | 0281- | | 1627- | | 100 | | 8 |
| 3 3 | 487 | -2080 | met | | 3444 | | 194 | | 7887 |
| | 47.1 | -2160 | | //901 | -20270 | | 3 3 | | 1010 |
| + | | | SKE | 16247 | .22627 | | /91 | 261. | 406 |
| + | | | | | | | 6603 | 841. | 603 |
| + | | | | | | | | | |
| + | | | | | | | | | |
| + | | | | | | | | | |
| + | | | | | | | | | |
| - | | | | | | | | | |
| XIAL FO | AXIAL FORCE (KN) | -13.9 | | | | | | | |
| H | | | | -14.5 | n | | | 9 94 | |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN S2-C

| | | | | Otrate Strate | Strate | 1 | | TOPE CONTINUES ASS | |
|---------|------------------|-------|--------|---------------|--------|------|-----|--------------------|---------|
| | | | 10 | | | | | į | Strate. |
| | -236 | \$2. | | | | | | = | |
| | -30.6 | | | | | | | 200 | |
| | 37.3 | | | | | | 8 | | |
| | 43.0 | 2 | | | | | 91 | | |
| | 542 | | | | | | | | |
| • | | | | | | | | | |
| | 974 | | | | | 563 | | | |
| • | | | | | | | | | |
| 9 | | | | | -622 | 679 | | 100 | |
| 2 | | | | | | | | | |
| = | | | | | | | | | |
| 2 | | | | | | | 272 | | 248 |
| 1 | | 300 | | | | | | | |
| | | 8 | | | | | | 3 | |
| | | | | | | | | | |
| | | * | | | 12 | | | | |
| | | 2353 | | 1638 | 93 | 910 | | 2 | |
| 7 | 28 | 2437 | | 7281. | 3 | | | | |
| 9 | 989. | 3334 | -5665· | | | | | | |
| 2 | -83.2 | 31300 | 7707 | WORK. | | | 35 | | |
| 2 | -53.8 | 31506 | ACAUP | OBOC. | | 633 | 43 | | |
| 7 | -53.6 | 31644 | 40647 | DBC? | 3113 | 22 | 88 | | |
| 22 | 53.5 | 32061 | 27207 | | 9502 | 917 | 2 | | |
| 23 | | 32262 | 200 | 2423 | 3008 | 906 | 100 | | |
| 24 | | 04000 | 2100 | 1985 | 2874 | 785 | 120 | | |
| | | | CE//DF | 9126 | 2862 | 778 | 131 | 477 | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| AXIAL F | AXIAL FORCE (KN) | -14.8 | | 44.8 | | ; | | | |
| | | | | | | 15.1 | | 14.0 | • |
| | | | | | | | | | |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN 53-A

| NA | EL C (FRO | PANEL C (FRONT DIAGONAL) | WAL) | | | | | | | | Test Codel No. 2 | • | | |
|-------------|------------------|--------------------------|-------------------------------|-----------|--------|--------|--------|--------|--------|--------|------------------|---|--------|----|
| į | Load Ich | Strain | Strain | Strain | Strain | Strain | Strain | Strain | Strain | Strain | Strade | Strain | Strain | |
| | | | | | 1 | 9 | | 7 | | • | \$ | 11 | 12 | _ |
| | | -172 | -28 | | -92 | -108 | 77- | -84 | -138 | -130 | 72. | | | |
| | 20 | .365 | 9 | | -186 | -246 | -145 | 011- | | - | 2 | | 00- | |
| | 30 | -604 | -25 | | -290 | 917 | | +22 | | 8 | 63- | 230 | -180 | =- |
| 1 | 40, | -872 | 30 | | | A19. | | 77. | | 900- | -130 | -355 | -270 | - |
| | 5 50 | -1207 | | 160 | | 979 | 145 | 2/- | | -774 | 95 | 470 | -345 | _ |
| _ | 6 55 | | | 505 | | 3 | | \$ | -106/ | -1142 | 128 | -574 | 404 | - |
| | 7 57.5 | | | | | S. | 9)- | 190 | -1276 | -1386 | 286 | -626 | 430 | - |
| | 9 | | | | | 1060 | 96 | 284 | -1388 | .1515 | 376 | -650 | -440 | |
| | | | | 10. | | -1126 | 2 | 336 | -1492 | -1536 | 467 | -668 | -447 | _ |
| | | | | -784 | | -1200 | 8 | 420 | -1608 | -1770 | 920 | 069- | -452 | _ |
| 2] : | | | | -814 | | -1272 | 110 | 200 | -1718 | -1895 | 999 | -708 | 166 | _ |
| | | | | 750 | -630 | -1320 | 180 | 594 | -1843 | -2040 | 784 | .728 | 470 | _ |
| | | | 632 | 006- | -664 | -1116 | 230 | 644 | -1936 | -2127 | 852 | 750 | 787 | |
| 21 | 72.6 | -2460 | 766 | -963 | 81.Z- | -1043 | 350 | 745 | 2002. | 2250 | | | | _ |
| | 63.1 | | | | | | | | | | 3 | | 210- | _ |
| | 45.0 | | | | | | | | | | 1 | | | |
| | | 72.5kN Fr | 72.5kN Front Diagonal Failure | I Failure | | | - | | | | 1 | | | |
| | | | | | | | - | | | | | | | |
| | | | | | | | | | | | | | | |
| AXIAL P | AXIAL FORCE (LN) | -26.4 | * | -27.3 | .3 | -11.1 | - | -21.3 | 6. | -19.8 | æ | -21.0 | 0. | |
| MOMENT(N.m) | IT(N.m) | 87.7 | 7 | 7.6 | | 39.9 | o, | 80.6 | 9 | 91.8 | | « | | _ |
| | | | | | | | † | | † | | | ֓֡֟֝֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֓֡֓֓֡֓ | | |
| | | | | | | | 1 | _ | | | | | | |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN 53-A

| PANEL C | PANEL C (REAR DIAGONAL | GONAL) | | | | | | | | | Test Serial No. 7 | No. 7 | |
|-----------------|------------------------|--------------|-------------------------|-----------|--------------|--------------|--------------|--------------|-----------|--------------|-------------------|--------|--------|
| No. | Load kN | Strain 47 | Strain 48 | Strain 40 | Strain 20 | Strain 24 | Strain 22 | Strain 20 | Strain 24 | Strain 24 | Strain 24 | Strain | Strain |
| | ١ | | 2 2 | | | | | | | | | | 3 |
| 7 | | | | | | 166 | -242 | 771 | \$ 70 | 246 | 8 6 | -100 | 0/- |
| | | | | | 336 | | 35. | | 787 | .376 | 184 | 382 | 210 |
| 7 | 40 | -222 | -552 | | -464 | | -478 | | -388 | S. | -234 | -516 | -270 |
| Ş | 5 50 | .272 | -712 | -348 | -626 | | 859- | | 787 | -656 | -270 | 8 | 320 |
| 8 | 55 | -300 | -600 | -334 | -748 | -310 | 187 - | -510 | 969- | -754 | -276 | -746 | 356 |
| 7 | 67.5 | .312 | -838 | 306 | -624 | -282 | 878- | -534 | 095- | -808 | -272 | 062- | 98. |
| • | 60 | -328 | -872 | -272 | -912 | -244 | -970 | 959- | 9899- | -964 | -264 | -834 | .376 |
| ٥ | 62.5 | -346 | -912 | -212 | -1026 | .176 | -1090 | -584 | -610 | -926 | -246 | 979- | -390 |
| 10 | 65 | -364 | -942 | -124 | -1160 | 88- | -1230 | 719- | -632 | 168 | -218 | 028- | -402 |
| 11 | 67.5 | .386 | 996- | 20 | -1354 | 99 | -1430 | 0+9- | -650 | -1090 | -176 | 0.60 | 416 |
| 12 | 70 | -424 | -1000 | 160 | -1530 | 202 | -1616 | 929- | 999- | -1168 | -144 | -1004 | 434 |
| 13 | 72.5 | 472 | -1032 | 410 | -1776 | 466 | -1932 | -756 | -624 | -1248 | -110 | -1034 | -450 |
| 14 | 63.1 | -640 | -1048 | 1134 | -2350 | 2314 | -4016 | -2892 | 1236 | -144 | -1068 | 432 | -360 |
| 15 | 45.6 | -520 | -756 | 2190 | -2824 | 3064 | 4376 | -2820 | 1694 | -536 | -212 | 346 | -402 |
| | | | | | | | | | | | | | |
| | | 63.1KN R | 63.1kN Rear Diagonal Fa | I Failure | | | | | | | | | |
| | | | | | | | | | | | | | |
| AXIAL FORCE (KN | RCE (KN) | Ą | -25.5 | 4 | -19.1 | 1- | -19.4 | -2 | -20.7 | -18 | -19.8 | -19.1 | 1.1 |
| MOMENT(N.m) | m) | 14 | 14.6 | 97 | 97.3 | 1 | 139 | 5 | 103.4 | 27 | 27.0 | 13 | 13.5 |
| | | | | | - | | | | | | | | |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN 53-A

| PANEL | C (FRONT AND | PAMEL C (FRONT AND REAR TENSION DIAGONAL) | GOHAL) | | | | | Test Serial No. 7 | |
|--------------|------------------|---|--------|------------|--------|--------|---------|-------------------|--------|
| 2 | Na bead | Strain | Strain | Strain | Strain | Strain | Strain. | Strain | Strade |
| | | 13 | 14 | 18 | 16 | 23 | 8 | 31 | 32 |
| | 10 | -22 | 97 | 8 6 | 0 | 28 | 10 | 62 | 9 |
| .`` | 2 20 | -54 | 104 | 78 | -14 | 09 | 10 | | 7 |
| ~" | 30 | -110 | 164 | 140 | -50 | 76 | 0 | 101 | -10 |
| | 40 | .188 | 268 | 220 | 011- | 110 | -10 | | -26 |
| 47 | 5 50 | -294 | | | -202 | 150 | -30 | | 95- |
| و ا | 55 | -370 | 755 | 977 | | 182 | -46 | | -82 |
| | 7 57.5 | 410 | | 900 | | 202 | -60 | 240 | 001- |
| | 8 | 440 | 672 | 920 | -324 | 222 | -70 | | -122 |
| • | 62.5 | -482 | 730 | 606 | -362 | 250 | -92 | 310 | -152 |
| 5 | 989 | -520 | | 659 | 384 | 282 | -112 | 348 | 081- |
| Ξ | 67.5 | -562 | 664 | 720 | | 330 | -152 | | -236 |
| 12 | 2] 70 | -600 | 910 | 756 | -450 | 366 | 194 | | 982- |
| 13 | 72.6 | -652 | 972 | 810 | -624 | 412 | -244 | 538 | -370 |
| | 63.1 | | | | | | | | |
| | 45.6 | -1282 | 1184 | 1120 | 7901- | 618 | 959- | 10701 | -1058 |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| AXIAL | AXIAL FORCE (KN) | 5.1 | .1 | • | 4.6 | | | | |
| MONNENT(N.m) | (N.m) | -46.5 | 3.6 | 9; | 63.5 | | | | |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN 53-B

| 1940 1944 1944 1945 1951 1951 1951 1951 1951 | 497 - 1540 487 - 1609 511 - 1644 434 - 1586 434 - 1574 410 - 1567 - 1574 - 601 | |
|--|--|-------|
| | 181- | -18.4 |
| | | |
| | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN 53-B

| 1 | | 1 | l | | | | | | |
|-----------|------------------|------|--------------|--------|--------|------|------|--------|--------------------|
| Ė | | | 1 | Strata | 9 tage | 1 | | | Test Serial No. 25 |
| | | | • | | = | | | Strate | Brats |
| " | 2 | | 414 | 902 | | | | 10 | |
| | | | -842 | | | | | -74 | |
| | | 100 | 789- | | | 3/6 | 120 | | |
| | | 320 | | | | 300 | | | |
| " | | 533 | | | | | | | |
| | 48.4 | 900 | | | | | | | |
| 7 | 1.00 | | | | | -709 | | | Ş |
| | 000 | | | | | | | 3 | |
| • | | | | -563 | | | | | |
| 10 | | | 7147 | | | 100 | | | |
| = | | | | | | | | | |
| 2 | | | 2925 | 38 | | 200 | 463 | | |
| 2 | | | .3033 | | | | 187 | | |
| 1 | | | 7200 | | | | -482 | | |
| 1 | | 4663 | 4477- | 100 | | 618 | | | |
| | 976 | 4016 | 7000 | DCS . | | 971 | | | 7 |
| | | | | 1963 | 1160 | | | | 8 |
| | | | - | | | | | | -238 |
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| \dagger | | | | 1 | | | | | |
| 1 | | | | | | | | | |
| AXIAL F. | AXIAL FORCE (KN) | 100. | _ | | | | | | |
| H | | - | | -20.0 | 0 | 4.6 | | * | |
| | | | | | | | _ | | |

AXIAL FORCES AND BENGING MOMENTS IN MEMBERS FOR SPECIMEN S4A

PAREL A(FRONT DIAGONAL TOP HALF BUCKLED INSIDE AND BOTTOM OUTSIDE)

TEST SERIAL NO. 1

| _ | | | | | | | | | _ | | | | | | | | | | | _ | |
|--|-----------|------|------|------|------|------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--------------|---|---|---|----------|
| Strate | = | 8 | 42 | 7 | 8 | -12 | 2 | 351 | 242 | 386 | 610 | 1306 | 4906 | 5034 | 5044 | | 3 | | | | |
| 100 | 17 | 132 | 702 | -262 | 432 | -630 | 90 | -1024 | -1146 | -1414 | -1830 | -3844 | | | | -20.1 | 105.4 | | | | Ī |
| a de la constante de la consta | _ | 20 | 727 | 8 | 328 | 300 | 3 | 530 | 264 | 624 | 900 | 786 | 618 | 999 | 700 | Ø. | 7 | | | | |
| Strate | | 122 | 8 | 114 | 136 | 156 | 2 | 191 | 200 | 228 | 268 | 207 | 234 | 360 | 296 | 16.9 | -13.2 | | | | |
| Strate | 7 | 90- | -102 | -110 | -178 | -166 | -244 | -290 | -332 | -334 | -368 | 857 | -260 | -514 | -532 | | | | | | |
| Strade | 5 | 178 | 132 | 180 | 226 | 200 | 574 | 780 | 386 | 434 | 909 | *** | 909 | 778 | 268 | | | | | | |
| Strate | 12 | -424 | -166 | -278 | 992. | -366 | -320 | -114 | -314 | -280 | -286 | -120 | -236 | 206 | -122 | | | | | | |
| a de la companya de l | 1 | -17 | 100 | 0+ | -22 | 29 | 99 | 14 | 8 | 46 | 32 | 20 | 906 | -210 | -160 | | : | - | | | |
| Strain 6 | 10 | 92 | 53 | 90 | 112 | 142 | 158 | 182 | 200 | 230 | 256 | 284 | 22 | 112 | 110 | | | | | | |
| Otroin a | 9 | -2 | φ | -10 | -12 | .10 | -20 | -24 | 32 | -36 | 7 | 9 | -204 | -266 | -214 | | | | | | |
| Strote | • | -28 | -56 | -82 | -122 | -234 | -194 | -234 | -276 | -318 | 364 | 907 | 432 | -602 | -534 | | | | | | |
| Ofrada 0 | 7 | 32 | 72 | 106 | 144 | 178 | 222 | 264 | 310 | 356 | 402 | 450 | 484 | 652 | 564 | | | | | | |
| Strate (| • | 9 | 12 | 16 | 22 | 30 | 40 | 8 | 62 | 76 | 3 | 110 | 3 | 0 | -134 | ~ | _ | | | | |
| Strate | | 98 | 124 | 186 | 250 | 314 | 300 | 468 | 544 | 622 | 702 | 778 | 830 | 882 | 796 | 14.2 | -19.1 | _ | | | |
| 45 | • | -01 | -174 | -270 | -362 | 456 | -578 | -686 | 796 | -916 | -1034 | -1164 | -1090 | 100. | 1534 | 7 | ~ | | | | |
| et et e | 8 | -30 | 30 | -20 | 35 | 8 | -56 | 95: | Ş | 9 | -32 | -22 | -140 | -2505 | -2202 | -18.7 | 32.2 | | | | |
| at est | 2 | 0 | S | 10 | 10 | 22 | 28 | ਨ | ş | \$ | 3 | 62 | 116 | 230 | 88 | | | | | | <u> </u> |
| et et e | • | 11. | -24 | -36 | 9 | 9 | .76 | 8 | Ş | 5 | -136 | -160 | 191 | -324 | 128 | | | | | | |
| ľ | Lead(NIN) | 10 | æ | 8 | 4 | 8 | 8 | 22 | 8 | 8 | 100 | 110 | 87 | 81.25 | 63.6 | KN | T (N.m) | | | | |
| | 9 | - | 7 | 9 | 4 | 6 | • | 7 | • | 9 | 10 | -11 | 12 | 5 | 7 | FORCE | MOMENT (N.m. | _ | - | | _ |

AXIAL FORCES AND BENGING MOMENTS IN MEMBERS FOR SPECIMEN S4A

| 3 | PANEL B(FRONT DIAGONAL BOTTON | RONT D | IAGON | IAL BO | _ | HALF BI | UCKLE | TOO 0: | BUCKLED OUTSIDE AND TOP INSIDE) | MD TC | SKI 40 | | | | TEST | TEST SERIAL NO. 1 | NO. 1 | | |
|------|-------------------------------|----------|--------|---------------|-------|-----------------------------|--------|--------|---------------------------------|------------|----------------------|-----|--------|--------|--------|-------------------|--------|---|--------|
| | | Strain | Strain | Strain Strain | l _ | Strain Strain Strain Strain | Strain | Strain | | Strain | Strain Strain Strain | | Strain | Strain | Strain | Strain | Strafe | Strain Strain Strain Strain Strain Strain | Strate |
| 身 | Lond kn | • | 2 | 3 | • | 10 | • | 7 | • | • | 9 | Ŧ | 42 | 1 | 7 | 18 | * | 11 | 7 |
| | 01 | 9 | 8 | 99 | 14 | 14 | 2 | 9 | 92 | 12 | 22 | 8 | 12 | 22 | 8 | 140 | 8 | ş | |
| 2 | 8 | -28 | .34 | -162 | -16 | 70 | 172 | 0 | 46 | 18 | 00 | 10 | 6 | • | | | | 9 | |
| c | 8 | 8. | 86 | -245 | | 114 | 246 | 0 | 8 | 3 | 0+ | 12 | 20 | • | 8 | 316 | L | 2 | |
| 7 | \$ | -52 | .76 | -320 | | 156 | 324 | 8- | 62 | 6 E | 48 | | | • | 22 | 9 | | 9 | |
| 8 | 8 | ş | 8. | 410 | • | 2 | 396 | 0 | 100 | 98 | 25 | 2 | | 9 | | 492 | | ÷ | İ |
| | 8 | -74 | .110 | -510 | 9 | 242 | 464 | -12 | 120 | 96 | 40 | 36 | 22 | 9 | 110 | | | 3 | |
| | 70 | 8 | -126 | -014 | .70 | 200 | 570 | -10 | 134 | 20 | 38 | 3 | | 0 | | | 274 | 230 | |
| | 8 | 6 | -146 | -724 | 20 | 330 | 848 | -16 | 150 | 98 | 30 | 26 | | * | 146 | 22. | 306 | 7,00 | |
| | 8 | -116 | .156 | -636 | 8 | 382 | 736 | -16 | 172 | 102 | 20 | 67 | 82 | 01 | | ğ | 25 | 376 | |
| 2 | 100 | -134 | -176 | -944 | -124 | 422 | 816 | -16 | 188 | 110 | 2 | 7.8 | 28 | 6 | 901 | 970 | 374 | -510 | |
| = | 110 | -130 | -190 | -1026 | -170 | 464 | 908 | -10 | 902 | 126 | -12 | 100 | 92 | 40 | | 3 | | ž | |
| 12 | 87 | 184 | -86 | 516 | 797 | 436 | 008 | -32 | 188 | 124 | -320 | 652 | | | | 25 | | 1980 | l |
| 13 | 81.25 | -314 | 26 | 2120 | 1 | 222 | 914 | 9 | 142 | 152 | -100 | 382 | \$ | 8 | 116 | 8 | 8 | .2962 | |
| 14 | 63.6 | -340 | 150 | 1998 | .2838 | 98 | 772 | 214 | 8 | 140 | -18E | ह | ę. | - | Ş | 8 | Ş | -2762 | |
| 1 | | | | | | | | | | | | | | | | | | | |
| FORC | FORCE KN | | | -19.2 | 3.2 | 22 | ٠. | | | | | | | | | 21.6 | 9. | | |
| | MOMENT (N.m) | | | 75 | 24.5 | -12.7 | .7 | | | | | | | | | -15.7 | 7: | | |
| | | | | | | | | | | | - | | | | | | | | |

AXIAL FORCES AND BENGING MOMENTS IN MEMBERS FOR SPECIMEN S4.A

PANEL C(FRONT DIAGONAL TOP HALF BUCKLED INSIDE AND REAR DIAGONAL TOP HALF

| 2 | KLED | UCKLED OUTSIDE | | | | ;)] | | | | | | | | | | A CALIAISE | 9 | | |
|-------|-------|----------------|------|---------------|-------|-------------|---------------|------|--------|--------|--------|--------|--------|--------|--------|------------|------|--------|-----|
| | | Strain | 1 | Strain Strain | | Strain | Strain Strain | | Strafe | Strain | Strain | Strate | Strate | Strate | Strain | 4 | . I. | Strate | |
| Š | Deol | • | 2 | n | • | 0 | 9 | | - | | 8 | 1 | N | 2 | • | - | 16 | 17 | 18 |
| | 10 | -42 | -32 | 19- | 81- | 120 | 32 | 12 | OC | 18 | 5 | ۴ | 91 | 22 | | 2 | ľ | 7.8 | 8 |
| | 20 | 8 | ŝ | .130 | -202 | 200 | 62 | 28 | 98 | 30 | 96- | .20 | -52 | 3 | | 8 | 282 | 302 | 72. |
| ` ' | 30 | .70 | 06- | -196 | -452 | 400 | 06 | 44 | 106 | 95 | | æ- | \$ | 22 | | 5 | 442 | 628 | 104 |
| 1 | \$ | -206 | .120 | -244 | -602 | 929 | 114 | 62 | 152 | | | 85. | -116 | 3 | | 3 | 8 | -852 | Ą |
| | 50 | -236 | 151 | -284 | -762 | 699 | 148 | 82 | 161 | 112 | SQ. | \$ | ŝ | 22 | | 252 | 762 | -1000 | 108 |
| _ | 9 | -206 | -164 | -300 | 096 | 842 | 168 | 26 | 912 | 106 | 8 | ŝ | 3 | 28 | | Ř | 98 | 4361 | 77. |
| | 70 | -240 | -212 | -320 | -1170 | 1000 | 218 | 100 | 292 | 120 | -120 | \$ | 991- | 28 | | 88 | 1036 | 1588 | 25 |
| | 90 | -410 | -240 | -316 | -1364 | 1170 | 200 | 106 | 294 | | | ş | 176 | 2 | | Ş | 1174 | -1840 | \$ |
| | 8 | -412 | -272 | -306 | .1626 | 1340 | 302 | 120 | 340 | 148 | -162 | \$ | ŝ | 2 | | 9 | 1314 | -2126 | 128 |
| 2 | 100 | -491 | -305 | -270 | -1862 | 1510 | 344 | 120 | 384 | 191 | -200 | 7 | -212 | 118 | | 988 | 1460 | -2458 | 246 |
| - | 110 | -864 | -324 | -210 | -2136 | 1606 | 380 | 132 | 428 | 961 | 961- | 7 | -242 | Ī | | 7.6 | Ī | .2822 | 3 |
| 12 | 1 07 | -324 | -286 | 276 | -1602 | 1766 | 816 | 3 | 330 | 971 | 091- | 3 | 278 | * | | 9 | 2 | .1842 | 212 |
| 13 | 81.25 | -294 | -254 | 386 | -3218 | 1582 | 504 | -284 | 706 | 238 | \$ | 146 | 136 | -182 | | • | 1014 | -3124 | 704 |
| 7 | 63.6 | -57 | ę | | | 1410 | -370 | -554 | 830 | 220 | 011 | 2 | 2 | .376 | | 071- | 25 | | |
| | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |
| FORCE | E K | | | -37.5 | .5 | 33.3 | - | | | | | | | | | 36.4 | • | -35.3 | 6 |
| | į | | | 7 64 | • | 27.6 | | | | | | | | | | | | | |
| | | | - | | | | | | • | | - | | - | | | | | | |

| | PAREL B(MOT BUCKLED) | T BUCK | | | | | | | | | | | | | TEST & | TEST SERIAL NO. 1 | 6 . 4 | | |
|-------|----------------------|--------|------|------|--------|--------|--------|----------------------|-------------|---------|---------------|--------|--------|--------|--------|-------------------|--------------|--------|--------|
| | | Strate | i i | į | Strate | Strain | Strain | Strain Strain Strain | Strain | Strain. | Strain Strain | Strain | Strain | Strain | Strafe | Strafe | Strate | Strate | Strain |
| 2 | 5 70 | • | 2 | 2 | • | • | • | 7 | • | • | 10 | 11 | 12 | 13 | 14 | 18 | 10 | 11 | = |
| | - 0 | 8 | -120 | ŞŞ | Ś | Ş | -62 | -70 | 08- | • | 44 | 100 | 200 | 136 | 059- | -1035 | 8 | -120 | 88, |
| | 2 | 7 | 8 | 2 | 8 | 22 | -200 | -42 | 82 | 8 | 43 | 090 | 320 | 340 | | -100 | -10 | 8 | \$ |
| | 8 | 9 | 8. | 320 | 8 | 99 | -242 | 107 | 108 | 28 | 38 | 099 | 312 | 340 | | .223 | 8 | 753 | 95 |
| | \$ | -146 | 33 | 425 | 22 | φ | 411 | 70 | 63 | 1 | 33 | 634 | 280 | 368 | | -222 | 901 | 3 | 673 |
| | 55 S | -146 | 2 | 512 | 74 | 15 | -516 | 130 | 115 | 72 | 12 | 299 | 205 | 412 | | 335 | ē | 870 | 2 |
| | 8 | 198 | Ş | 98 | ē | 22 | 940 | 107 | 128 | 28 | 12 | 989 | 321 | 386 | 151 | -371 | -222 | 815 | 929 |
| | 20 | -152 | 11- | 747 | 101 | ã | -713 | 176 | 228 | 115 | 8 | 516 | 312 | 436 | 180 | 475 | -214 | 838 | 101 |
| | 2 | -260 | 76- | 751 | 116 | 5 | 508 | 128 | 174 | 50 | -23 | 460 | -465 | -224 | 996- | -1300 | -012 | ş | 8 |
| | 8 | -250 | 20 | 910 | 207 | 951 | ģ | ş | SS 2 | 145 | 20 | -189 | -688 | 490 | -574 | -1305 | 8, | 153 | 670 |
| - | 100 | -275 | -28 | 1032 | 233 | 178 | -1092 | 233 | 200 | 148 | 12 | -282 | -422 | -356 | -487 | -1353 | .728 | \$ | 35 |
| | 110 | -302 | 84- | 1103 | 247 | 190 | -1284 | 236 | 310 | 101 | 97 | 200 | 300 | -354 | 256 | - - | 2 | 258 | Ž |
| | 12 87 | 246 | 187 | 677 | 137 | 762 | -720 | 232 | 300 | 173 | -193 | -668 | -540 | -120 | 99 | -700 | 90 | 8 | 1297 |
| | 13 81.25 | -219 | 308 | 912 | 171 | 200 | -793 | 210 | 252 | 170 | -48 | -1000 | -200 | 280 | 13 | 743 | -1415 | 8 | -322 |
| - | 14 63.6 | \$ | 630 | 711 | 197 | 160 | 400 | 47 | 440 | 161 | 41 | 006- | -1060 | 900 | 413 | 981 | 3 | 421 | 1063 |
| | | | | | | | | | | | | | | | | | | | |
| FORCE | CE KN | | | | | | | İ | | | | | | | | | | | |
| | OMENT (N.m. | | | | | | | | | | | | | | _ | | | | |
| | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |

AXIAL FORCES AND BENGING MOMENTS IN MEMBERS FOR SPECIMEN 84.A

| | 1 | PARKE E(NOT BUCKLED) | | | | | | | | | | | ĺ | | 16.51 | TEST SERIAL NO. | 9 | | |
|-------|--------------|----------------------|--------|-----------------|--------|----------|---------------|----|---------|---------|--------|-----------|--------|------------------------------------|-------|-----------------------------|----------|--------|--------|
| | | Strate | Strafe | Strate et al | Strain | Strain | Strain Strain | | Strain. | Strain. | Strain | Strain | Strain | Strain Strain Strain Strain Strain | | Strain Strain Strain Strain | - Strain | Strain | Strain |
| ž | 5 2 3 | | 2 | 3 | • | • | • | 7 | • | • | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 11 | # |
| | 2 | 7 | -17 | \$ | 97 | 8 | 0 | 9 | 23 | 3 | -13 | 3 | 02 | 02 | C7 43 | 9 8 | 01- | 143 | 8 |
| 7 | 8 | -18 | S, | 8 | | -202 | 9 | -1 | 41 | 0 | 8 | 6- | 24 | 77 | 00 | 13 | .163 | 241 | 8 |
| | 8 | .29 | 95 | 137 | 284 | -318 | -14 | 0 | 95 | Ŝ | 25 | .20 | 27 | 22 | 02 | 47 | L | 335 | 82 |
| * | \$ | 7 | .78 | 182 | | -440 | -17 | 9 | 75 | 9 | 4 | .37 | 02 | 21 | 11 | 13 | | | 8 |
| S | 8 | 25. | -97 | 231 | 467 | -572 | -18 | 2 | 98 | 9 | 65 | -51 | 28 | 28 | 88 | | | | 128 |
| 9 | 28 | 88 | .122 | 38 | 531 | 789- | -19 | 2 | 102 | 22- | 69 | 95. | 29 | 28 | 1 | | | | Š |
| _ | 2 | -78 | 136 | Š | 612 | -817 | -15 | 9 | 116 | 4 | 75 | -55 | 31 | 22 | 125 | | | 119 | ğ |
| 9 | 8 | 25 | -156 | 348 | 793 | -942 | 8. | 9 | 130 | 4 | 97 | -67 | 35 | 20 | 120 | 112 | 628· | 740 | 207 |
| 9 | 8 | -107 | -174 | 387 | 762 | -1074 | -7 | 0 | 141 | -57 | 111 | -69 | 41 | 28 | | | • | 639 | 240 |
| 2 | | .119 | -197 | 431 | 647 | -1203 | -19 | 14 | 155 | -645 | 129 | -81 | 48 | 88 | 163 | 275 | -1324 | 927 | 270 |
| Ξ | 110 | .133 | -214 | 471 | 828 | -1256 | -63 | 10 | 170 | | 150 | 34 | 878 | 36 | 162 | 413 | -1880 | 088 | 280 |
| 12 | 64 | ġ | .177 | 982 | 200 | 999 | 28: | 10 | 122 | -171 | 112- | 107 | 120 | 0 | 129 | 700 | 0191- | 1037 | 274 |
| 2 | 61.25 | 8. | -156 | 920 | 3 | -874 | ŝ | | 110 | -92 | 76 | -16 | 25 | 24 | 131 | 268 | -1239 | 619 | 210 |
| = | 63.6 | 8 | -120 | 307 | 523 | -649 | -47 | | \$ | -102 | 45 | 9 | 98 | 95 | 98 | | 118 | 999 | 8 |
| | | | | | | | | | | | | | | | | | | | |
| FORCE | E EN | | | | | | | | - | | | | | | | | | | |
| MOME | MOMENT (N.m. | | | | | ' | | | | | | | | | | | | | |
| | | | | | | | | | | _ | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | |

AXIAL FORCES AND BENGING MOMENTS IN MEMBERS FOR SPECIMEN S4A

| PAN | PANEL F(NOT BUCKLED) | BUCKLE | ê | | | | | | | | | | | | | | | | |
|----------|----------------------|----------|--------|-----------------------------|-----|--------|----------|---|----------|--------|--------|-------|---------|-----|------|-------------------|-----------------------------|--------|--------|
| | | Strain | Strain | Strain Strain Strain Strain | | Strain | Strain | Strain Strain Strain Strain Strain Strain | Hrain | Strain | Strain | Stone | Service | - 1 | | TEST SERIAL NO. 1 | 9 | | |
| 운 | Lond kn | • | 2 | • | • | 8 | • | 7 | • | • | 10 | + | 12 | 13 | 14 | | Strain Strain Strain Strain | Strain | Strafa |
| | 10 | ٥ | 0 | 42 | 0 | 0 | ° | 3 | ٦ | ľ | 1 | 9 | 1 | | | | | | 2 |
| 7 | 20 | 8 | .12 | 8 | 91- | 3 | | 1 | | ľ | 3 3 | | 2 | | ş | 25 | 7 | .78 | 8 |
| 6 | 30 | | ٦ | Ş | | | | 1 | 2 | | 3 | • | 8 | 3 | -110 | 992 | -146 | -62 | 176 |
| | 4 | | | 3 3 | | - | Ş | 2 | 2 | 9 | 8 | ŝ | \$ | 2 | 131 | -367 | -177 | -68 | 263 |
| _ | | | 1 | | | • | ğ | 2 | ā | ٥ | 503 | • | 2 | 201 | -142 | 448 | -200 | ġ | 75 |
| | | | 7 | 202 | 2 | 2 | ş | 137 | -132 | 9 | 127 | 7 | ಜ | 125 | .157 | 940 | -224 | 8 | 428 |
| 1 | | | 8 | ž | 8 | \$ | \$ | 57 | -155 | ٩ | 142 | 2 | 8 | 155 | -182 | -652 | 246 | ş | 537 |
| | | | | 8 | 5 | 62 | ş | 2 | -187 | 7 | 161 | 2 | 113 | 177 | -202 | -750 | 2.70 | r. | 5 |
| | | 8 | 1 | \$ | 2 | 55 | 288 | 222 | Ę | -10 | 178 | 4 | 136 | 202 | -222 | 543 | Ŕ | 2 | 200 |
| | | 22 | | 525 | 212 | 2 | 8 | 32 | -236 | 90 | 2 | 7 | 162 | 231 | 777 | 9 | 32 | ٤ | |
| | | = | 9 | 8 | 258 | 207 | 828 | 280 | -202 | -37 | 218 | 10 | - - | 257 | ž | 100 | 2 | \$ 5 | 3 8 |
| | | ş | 2 | 3 | 202 | 428 | -1002 | 317 | -280 | 7 | 236 | _ | 212 | Ž | į | | | 1 | |
| 2 | 87 | 2. | ٥ | 366 | 167 | 130 | -516 | 192 | 071- | 900 | 137 | | ş | ě | 1 | | | 7 | 1020 |
| ត | 81.25 | -108 | Ş. | \$ | 180 | 771 | 422 | 1 | ã | - | • | † | 3 3 | 787 | ? | -1034 | 2 | 2 | 1013 |
| 7 | 63.6 | 70- | 0 | ş | 8 | 8 | 8 | | | ! | 20 1 | 72 | 22 | 2 | 72. | 2 | SS. | ş | 827 |
| | | | | | | | | * | <u>8</u> | ? | 2 | 2 | 182 | 2 | 92 | -707 | -208 | -102 | 960 |
| | | | 1 | | 1 | | † | | + | 1 | | | | | | | | | |
| FORCE KN | 3 | | | | | | | | _ | | | | | | | | | | |
| | | | - | | | | <u> </u> | | | | | | | | 1 | | | | |
| MOME | MOMENT (N.m.) | <u> </u> | | | | | | | | | | | | | | | | | |
| | | | | | | | | _ | | | | | T | | + | ľ | 1 | | |
| | | | | | | | | | | | | | T | | 1 | + | 1 | 1 | |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN S4-B

| PANI | IL A (FRO | PANEL A (FRONT DIAGONAL BUCKLED WI | HAL BUC | | BOTTOR | HALF OU | TH BOTTOM HALF OUTSIDE AND TOP INSIDE |) TOP INS | | | Test Serial No. 3 | £0.3 | |
|------------|-----------|------------------------------------|---------|--------------|--------------|---------|---------------------------------------|-----------|--------|--------|-------------------|--------|----------|
| į | Lead kill | | Strain | Strain | Strain | Strain | Strain | Strain | Strain | Strain | Strain | Strain | Strain |
| | | • | 7 | 9 | • | 9 | • | 7 | • | • | 10 | Ţ | 4 |
| | 10 | 8 | -21 | | \$ | -58 | -72 | 32 | -160 | 181- | 07 | ġ | ş |
| 2 | 20 | -190 | 43 | | -114 | -110 | -142 | 11 | -322 | -357 | | | A. |
| 9 | 8 | -272 | -64 | | 191 - | -164 | -201 | 131 | | -532 | | | S S |
| 1 | 35 | -313 | .78 | | -191 | -194 | -230 | 164 | 929- | -626 | | | 101 |
| 2 | \$ | -350 | -01 | | -216 | -224 | -256 | 200 | | -723 | | 178- | 115 |
| 0 | 45 | -383 | -104 | | -236 | -254 | -279 | 238 | | -812 | | 417 | 120 |
| | 47.5 | -402 | -114 | | -250 | -272 | -282 | 259 | | -962 | | 740 | .123 |
| • | S | 416 | -122 | | -262 | -297 | -303 | 280 | | 906- | | 465 | 721. |
| • | 52.5 | 431 | -132 | -328 | -274 | -303 | -312 | 301 | | .953 | | 488 | 021- |
| 10 | 55 | 445 | -140 | | -262 | -320 | -319 | 322 | 976 | 966 | 306 | 016- | 183 |
| = | \$ | -472 | .159 | ļ | -306 | -354 | -338 | 370 | -1048 | -1090 | | 999 | 25. |
| 12 | 92 | 207 | 179 | | -324 | -389 | -344 | 420 | -1141 | -1182 | | -603 | 140 |
| 13 | 2 | -513 | -202 | | -344 | -430 | -362 | 475 | -1244 | -1278 | | 648 | C41- |
| 3 | 75 | -530 | .228 | | .363 | -472 | -366 | 533 | -1350 | -1374 | 462 | 989 | -142 |
| 15 | 8 | -542 | -258 | | -363 | -520 | -371 | 585 | -1460 | -1471 | | 744 | .142 |
| £ | 92 | -551 | -289 | -482 | 400 | -569 | .370 | 662 | 1577 | -1572 | | .703 | 140 |
| 17 | 8 | -554 | -324 | -501 | | -624 | -362 | 734 | 1691- | -1672 | 989 | -842 | -135 |
| ₽ | 92.5 | -553 | 25. | -512 | 426 | -652 | -358 | 772 | 1758 | -1722 | 624 | 996 | 135 |
| = | 98 | -552 | .361 | -510 | 757 | -679 | -352 | 808 | -1814 | -1768 | 8 | 069- | 130 |
| R | 97.6 | -547 | -382 | -528 | 442 | -712 | -342 | 852 | -1883 | -1821 | 676 | 916- | -124 |
| 2 | <u>ਤ</u> | -542 | 80 | -536 | 950 | -750 | -330 | 888 | -1958 | -1882 | 708 | 78 | .120 |
| ล | 102.5 | -536 | 430 | -544 | 456 | -760 | -320 | 942 | -2022 | -1928 | 734 | 996 | -114 |
| Ñ | 105 | .530 | 455 | -552 | 984 | -614 | -308 | 988 | -2121 | 1961- | 766 | 986 | 108 |
| 20 | 107.5 | -518 | 8 | -558 | -472 | 759- | -289 | 1075 | -2163 | -2040 | 962 | -1024 | -102 |
| 3 2 | 5 | -507 | -507 | 78 9. | 478 | 5005 | -270 | 1150 | -2264 | -2097 | 832 | -1052 | -92 |
| 8 | 112.6 | 94 | -538 | -570 | \$ | -942 | -244 | 1240 | -2450 | -2156 | 970 | -1062 | 0 |
| 27 | 116 | -468 | -574 | -573 | 8 | 866- | -210 | 1347 | -2676 | -2222 | 910 | -1114 | 88 |
| 28 | 117.5 | 77 | -610 | -578 | ğ | -1054 | .173 | 1484 | -3008 | -2284 | 954 | -1145 | -35 |
| 8 | 120 | 414 | 848 | -578 | 496 | -1118 | 128 | 1616 | -3284 | -2350 | 866 | -1178 | -38 |

| 0. | 38.0 | 6.0 | 100.9 | 8. | 130.8 | 8 | 40.8 | 2 | 2. | 14.2 | 7 | AOMEINT(N.m) | |
|-----|-------|------|-------|--------|-------|------|-------|------|------|-------|-------|-----------------|-------|
| 1.0 | -20.1 | 2. | -21.2 | 6. | -24.9 | 7.0 | -20.7 | 7.1 | -11 | 5 | -17.1 | KIAL FORCE (KN) | AXIAL |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| 400 | APAC. | 3600 | -5193 | | 20850 | 2960 | -9450 | 190 | -570 | -1598 | 1144 | 145 | 8 |
| 468 | -1668 | 2220 | -3728 | -17404 | 12244 | 1164 | -2283 | -302 | 473 | -1160 | 344 | 142.5 | 8 |
| 435 | 1808 | 2120 | -3608 | -16438 | 11317 | 1035 | -2171 | .330 | 478 | -1132 | 274 | 140 | 37 |
| 305 | 0221. | 2006 | -3475 | .15380 | 10378 | 913 | -2068 | -350 | -490 | -1068 | 212 | 137.5 | 8 |
| 2 | 15.00 | 1786 | -3170 | -13144 | 8350 | 22.1 | -1906 | -364 | -500 | -1022 | 106 | 135 | S |
| | 1424 | 1492 | -2848 | 0069- | 4600 | 901 | -1658 | 450 | -636 | -923 | 90 | 132.5 | 3 |
| 9 | A321. | 1309 | -2002 | -5618 | 2805 | 200 | -1480 | -482 | -562 | -640 | -209 | 130 | 8 |
| 8 | -1290 | 1182 | -2676 | -4660 | 2244 | 23 | -1357 | -496 | -672 | -782 | -287 | 127.6 | 2 |
| | -1240 | 1112 | -2494 | -4009 | 1960 | -10 | -1266 | 486 | -576 | .733 | -338 | 125 | 5 |
| 9 | 6161. | 1050 | -2416 | -3590 | 1764 | -75 | -1188 | 496 | -578 | -688 | -380 | 122.6 | S |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN S4-B

| PANELA | PANEL A (REAR DIAGONAL BUCK | AGONAL | _ | 2 | P HALF O | UTSIDE A | ND BOTT | GISNI MO | | | Test Serial No. 3 | No. 3 | |
|-----------|-----------------------------|-----------|----------|--------------|--------------|-----------|---------|----------|--------|--------|-------------------|--------|--------|
| į | Leed EX | Strain 47 | era e | Strain 40 | Strain 20 | Strain 2. | | Strain | Strain | Strain | Strain | Strafe | Strain |
| | | | | | | | | 3 | 2 | 220 | R | 22 | 2 |
| | | 3 | 9 | S | 7 | -10 | 8 | -22 | -74 | -90 | 10 | -40 | \$ |
| 2 | 8 | -214 | 7 | -124 | \$ | -18 | -196 | 44 | -166 | -224 | 28 | | |
| 3 | 8 | -336 | 2 | -192 | .126 | -16 | -312 | 98- | -254 | 96. | | | |
| 4 | 35 | 396 | • | -226 | -146 | -10 | -370 | -76 | | 424 | | | |
| 9 | \$ | 9 | 14 | -260 | -166 | 7 | 0€₱ | \$ | 346 | 4 | | | |
| 0 | 45 | -526 | 24 | -286 | .186 | 0 | 4 | 8 | 380 | 582 | | | |
| 7 | 47.5 | -564 | 75 | -315 | -196 | • | 83 | -100 | 414 | 508 | | | 764 |
| 8 | 8 | 85 | 8 | -334 | -206 | 10 | -562 | ş | 8 | -630 | 8 | | 400 |
| 8 | 52.5 | -630 | 45 | -352 | -216 | 16 | 985 | -10 | 8 | 487 | 505 | | 616 |
| 01 | 55 | 999 | \$ | -372 | -226 | 30 | -632 | 116 | 8 | ş | 107 | AAC. | 640 |
| 1 | 8 | -742 | 62 | 410 | -244 | 48 | -704 | -128 | .526 | 786 | 118 | 200 | 303 |
| 12 | 92 | -818 | 62 | 794- | -262 | 70 | -780 | .140 | -570 | -836 | 130 | -288 | -650 |
| 13 | 2 | -892 | 20 | 767 | -276 | 8 | -855 | -152 | -612 | 8 | 140 | 306 | 200 |
| 7 | 75 | -972 | 138 | -522 | -294 | 126 | -936 | -166 | -652 | 998- | 55 | .326 | 751 |
| 15 | 8 | 1054 | \$ | -562 | 906- | 162 | -1022 | -180 | 889 | -1028 | \$ | 350 | POP. |
| 16 | 92 | -1138 | 8 | 900 | -310 | 204 | -1116 | -200 | -722 | 9601- | ₹ | 368 | 854 |
| 17 | 8 | .1226 | 214 | 638 | -332 | 226 | -1210 | -224 | .750 | -1148 | 170 | 386 | 98 |
| 10 | 87.5 | -1270 | 22 | 958 | .336 | 250 | -1258 | -235 | -784 | -1172 | 170 | 390 | 926 |
| 9 | 8 | -1316 | 254 | 980 | 344 | 278 | -1312 | -248 | 977- | 1200 | 170 | 400 | 059 |
| 2 | 97.5 | 1366 | 274 | -700 | -348 | 312 | -1364 | -264 | -785 | -1225 | 89 | 90 | 476. |
| 21 | <u>\$</u> | -1426 | SS. | .720 | -353 | 340 | -1426 | -283 | -792 | -1251 | 3 | 7 | 986 |
| 22 | 102.5 | -1462 | 321 | -739 | .356 | 374 | -1477 | -289 | 787. | -1271 | 162 | 428 | 1019 |
| 23 | 105 | -1512 | 돐 | .750 | -358 | 410 | -1534 | -320 | 8 | 1290 | 85 | 432 | 1041 |
| 24 | 107.5 | 1566 | 372 | -778 | -361 | 451 | -1597 | -343 | 008- | 1309 | 151 | 433 | -1062 |
| 25 | = | -1616 | 401 | 796 | 300 | 497 | -1662 | -368 | -795 | .1325 | 143 | 77 | -1082 |
| 58 | 112.5 | -1675 | \$ | -821 | .366 | 548 | -1732 | -398 | .790 | -1340 | 132 | 440 | -1102 |
| 22 | 115 | -1741 | 488 | -844 | .368 | 602 | -1812 | 434 | 677- | -1352 | 11 | 757 | .1123 |
| 28 | 117.5 | -1802 | 906 | 28 | -368 | 663 | -1688 | -472 | -762 | -1358 | 90 | 455 | CA11. |

| 29 | 120 | -1968 | 552 | -886 | -369 | 733 | -1973 | 919- | 147- | -1363 | 70 | 787 | 1159 |
|------------------|----------|-------|------|-------|------|------|-------|-------|------|-------|-------|-------|-------|
| 8 | 122.5 | -1940 | ñ | -911 | -370 | 620 | -2068 | -570 | -711 | -1362 | 53 | 462 | -1175 |
| 31 | 125 | -2021 | 649 | -934 | -369 | 979 | -2163 | -636 | 999- | -1351 | 16 | 8 | 1101 |
| 32 | 127.5 | -2118 | 725 | -956 | .361 | 1280 | -2370 | .740 | -576 | -1312 | 7 | 3 | -1195 |
| 33 | 130 | -2262 | 652 | -966 | -344 | 2040 | -2810 | -922 | -396 | -1220 | -143 | 867 | -1162 |
| 8 | 132.5 | -2640 | 1194 | -1046 | -296 | | | -135 | 62 | -955 | -378 | -372 | -1105 |
| 35 | 135 | -3202 | 1842 | -1174 | -204 | | | -1988 | 872 | -462 | -705 | -217 | -905 |
| 8 | 137.5 | | 2166 | -1250 | .157 | | | -2203 | 1284 | -232 | -648 | -138 | -812 |
| 37 | 140 | | 2300 | -1288 | -138 | | | -2449 | 1503 | -122 | -920 | 8 | -773 |
| 2 | 142.5 | | 2396 | -1305 | -116 | | | -2619 | 1684 | 30 | 196. | 99- | -740 |
| 38 | 145 | | 2911 | -1357 | 303 | | | | | 1714 | -2220 | 909 | -200 |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| AXIAL FORCE (KN) | ICE (KN) | : | | -22.8 | 2.8 | | | -13.9 | 6. | -16.2 | | -12.9 | 69 |
| MOMENT(N.m) | (a | | | 40.7 | 7. | | | 116.8 | 80, | 27.3 | 6 | 19.3 | 8 |
| | | | | | | | | | | | | | |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN S4-C

| | L A (FRO) | PANEL A (FRONT DIAGONAL) | WAL) | | | | | | | | Test Serial No. 5 | o. 5 | |
|----|-----------|--------------------------|------------------|--------|-------|--------|--------|--------|--------|---------|-------------------|-----------------|---------|
| | | etrate | - State | Strate | et et | Strate | Strata | Strate | Strain | Strain. | Strate (| Merata | Strain. |
| į | | _ | 7 | • | 4 | | • | 7 | | • | 10 | ÷ | 12 |
| [| 10.01 | 85- | -128 | 27- | 77- | -120 | -28 | -126 | 36- | 48 | .163 | -14 | -132 |
| 2 | 80 | | | | -120 | -207 | -34 | -190 | -52 | 78 | 300 | -22 | -210 |
| 6 | 30.0 | 8, | | | -172 | -314 | -42 | -286 | -70 | 120 | 450 | 35 | -312 |
| • | 40.0 | | | | -236 | -440 | -38 | -304 | -87 | 172 | -624 | -42 | 430 |
| 9 | 88 | | | | -294 | -570 | -32 | -500 | -105 | 224 | -788 | \$ | -536 |
| • | 90.08 | | | | -354 | -708 | 9- | -605 | -116 | 280 | -952 | Ş | -652 |
| 7 | 70.07 | | | -364 | -406 | 098- | 34 | -706 | -132 | 332 | -1126 | Ş | .758 |
| • | 75.0 | | | 418 | -438 | -946 | 56 | -760 | -138 | 364 | -1208 | -62 | -812 |
| 9 | 80.0 | | ľ | -442 | 997 | | | -810 | -146 | 393 | -1288 | -62 | 999 |
| 10 | | | | | -492 | 2111- | | -960 | -154 | 420 | .1370 | \$ | -922 |
| 11 | | | | | -520 | -1203 | 156 | -902 | -170 | 440 | 1444 | -70 | 996 |
| 12 | | | | -513 | 999- | -1310 | 202 | -944 | -184 | 466 | -1524 | 27. | -1024 |
| 13 | | | | -528 | 199- | -1378 | | -966 | -196 | 476 | .1572 | -74 | -1055 |
| 1 | Ĺ | | | -532 | -570 | -1410 | 255 | -972 | -203 | 463 | .1590 | .75 | -1070 |
| 15 | | | | L | 989- | -1474 | 290 | -960 | -220 | 492 | -1628 | 8 | -1100 |
| 10 | | | | | 969- | .1532 | 322 | -1002 | -232 | 500 | .1660 | \$ | -1120 |
| 17 | | | | | -612 | -1500 | | -1008 | | 505 | .1690 | -88 | -1142 |
| 18 | | | | -576 | -622 | -1648 | | -1018 | -266 | 504 | -1716 | .90 | -1164 |
| 92 | | | | | -632 | -1706 | 438 | -1024 | .286 | 906 | -1740 | \$ | -1182 |
| 8 | | | | | 059- | -1805 | 506 | -1020 | -324 | 906 | 2771- | -103 | -1210 |
| 21 | | | | | 959- | -1852 | 547 | -1018 | -346 | 900 | -1784 | -105 | -1220 |
| 22 | | | | | 899- | -1944 | 612 | -1004 | -384 | 490 | .1800 | -105 | -1240 |
| 23 | | | | -620 | 089- | -2036 | 969 | -962 | 437 | 476 | -1812 | -124 | .1256 |
| 24 | | | -200 | 929 | | -2008 | 796 | 976 | 492 | 454 | -1612 | -137 | -1270 |
| 8 | | | -206 | | 760 | -2180 | 826 | | -574 | 410 | -1785 | -152 | -1272 |
| × | | | | 1 -622 | 969 | -2856 | 1312 | 989- | .780 | 306 | -1706 | \$ 1 | -1200 |
| 27 | | | 1 87- | | -714 | -4500 | 2786 | | -1410 | -105 | -1206 | -280 | 1074 |
| 28 | | | | -652 | | | 6236 | 796 | -1942 | 403 | -728 | 306 | -674 |
| 8 | 137.5 | | 996- | -652 | -656 | .10360 | 6716 | | -2000 | 470 | -500 | -300 | -903 |

| - | | - | - | - | _ | | | | | | | | |
|------|-------------|------|----------|-------|-------|------|--------|------|-------------|-------|-------|-------------------|-------------|
| T | - | 1 | | - | - | | _ | | | | | | |
| T | 31.2 | | 57.7 | | 2.9 | | 163.4 | 2 | 2.2 | * | 89.4 | T(N.m) | MOMENT(N.m) |
| | -23.2 | _ | -22.4 | | 1.63- | | | | | | | | |
| | - ; | | .224 | | -23.7 | | -19.9 | .2 | -21.2 | - | -23.1 | AXIAL FORCE (ILN) | AXIAL F |
| | | | | | | | | | | |] | | |
| | | | | | | | | | | | | | |
| | 4 | | 1 | + | | | | | | | | | |
| 3 | | | _ | | | | | | | | | | |
| ٤ | ž | 425 | 905 | -2310 | 1326 | | 1 | 3 | 770 | | | | |
| -746 | -205 | -480 | 85 85 | 9027 | 200 | 3 | | | | 9000 | 2470 | 145.0 | 32 |
| 2 | 8 | 200 | | 1 | 1369 | AG74 | -10640 | 98 | -635 | -3620 | 2440 | 142.5 | <u></u> |
| | | | 313 | 2480 | 1140 | 0000 | -10500 | -626 | 6 75 | | 2378 | | 3 |
| | | | | | | | | | | | | | 5 |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN S4-C

| PANEL | Panel a (rear diagon) | DIAGONA | AL) | | | | | | | | I GEN GETTEL FRO. 0 | 9.0 | |
|-------|-----------------------|-------------|--------|--------|--------|--------|--------|-------|--------|----------|---------------------|----------|------|
| | 44,500 | Strain | Strain | Strain | Strate | Strain | Strain | | Strain | aferale. | al and a second | Servet . | |
| į | | 17 | 10 | = | 2 | ž | Z | 2 | 2 | 2 | 2 | 12 | R |
| 1 | 10.0 | 18 | -124 | 99- | -30 | 8 | -10 | -106 | -16 | 28 | ă | 8 | \$ |
| 7 | 20.02 | 88 | -228 | -150 | -42 | .177 | -23 | 178 | .20 | 8. | -166 | -57 | -115 |
| 9 | | ļ ! ! | 98. | -248 | c7. | .281 | -23 | -263 | -18 | 45 | -265 | \$ | .178 |
| - | 40.0 | | 984 | 330 | 8 | 976- | -33 | 368 | -11 | S. | 366 | -106 | -232 |
| 9 | | | 98 | 907 | -106 | -471 | -30 | -450 | 3 | S | 977 | -129 | -288 |
| 9 | 90.0 | | | 967 | 121. | -573 | -27 | -610 | 27 | 95 | -552 | -150 | -342 |
| - | | | | :993 | .140 | -672 | | -732 | S | 7 | -647 | .163 | -36F |
| • | 75.0 | | 026- | -610 | .150 | -726 | -15 | .779 | 2 | 35 | -706 | -172 | 415 |
| 0 | | | -962 | -646 | -155 | -772 | .7 | -870 | 2 | -28 | -754 | 178 | 445 |
| 2 | | | _ | 989 | 151- | -825 | 0 | 169- | 111 | % | -819 | -166 | 466 |
| = | 0.08 | | | .723 | 191- | -878 | 4 | -1000 | 140 | .10 | -873 | 187 | -491 |
| 12 | | | 2111- | .765 | -172 | -931 | 12 | 1071 | 165 | S | -930 | -198 | -514 |
| 13 | 97.5 | | 1205 | .785 | C91- | -962 | 13 | -1106 | 177 | 14 | .972 | 202 | -528 |
| 2 | | | 1224 | -794 | | | 17 | -1130 | 9 | 82 | -985 | -202 | 538 |
| 15 | 102.5 | | .1256 | -819 | .185 | -1005 | 23 | -1172 | 202 | 28 | -1118 | .203 | -550 |
| 9 | 105.0 | 308 | 1288 | -632 | -195 | -1031 | 27 | .1205 | 218 | 35 | 1047 | -206 | .560 |
| 17 | | | L | | -200 | -1055 | 25 | -1255 | 235 | \$ | .1170 | -211 | 995 |
| 9 | | | | | .200 | -1074 | 30 | .1285 | 250 | 8 | -1104 | -214 | -561 |
| 9 | 112.5 | | 961 | -892 | -192 | -1006 | 27 | | 274 | 9 | .1130 | -216 | -592 |
| 8 | | | -1406 | 910- | .183 | -1134 | 30 | -1389 | 308 | | -1185 | -220 | -607 |
| 12 | | | -1424 | 628- | -217 | -1149 | 35 | -1432 | 322 | | .1217 | .220 | -614 |
| 22 | | | .1455 | 940 | -204 | -1175 | 35 | .1475 | 746 | æ | -1257 | -218 | -624 |
| 23 | | | 1488 | | -211 | -1202 | 40 | .1540 | 371 | ŝ | .1296 | -223 | 909 |
| 24 | | | -1512 | | -226 | -1226 | 40 | .1550 | 401 | 125 | .1330 | -220 | \$ |
| 25 | | | .1533 | | -238 | -1246 | 98 | .1640 | 430 | 55 | .1355 | -224 | -855 |
| 2 | | | -1565 | -1024 | -254 | -1275 | 8 | .1686 | 469 | 292 | | 222 | 98 |
| 27 | | | -1602 | | -255 | -1310 | \$ | -1767 | 523 | 197 | 1471 | 122: | -675 |
| 28 | | ğ | 1991- | | -250 | .1346 | 98 | -1688 | 618 | 98 | .1583 | -212 | -880 |

| 82 | 137.5 | 88 | -1688 | -1112 | 992 | -1363 | 22 | -2031 | 705 | 317 | -1657 | -206 | -085 |
|------------------|----------|-----|-------|-------|-------|-------|------|-------|-------------|-----|-------|-------|------|
| 8 | 140.0 | | 7171- | -1130 | -276 | -1360 | -19 | -2190 | 828 | 370 | 1771- | -195 | 089 |
| 31 | 142.5 | 341 | .1600 | .1133 | -311 | -1304 | 101- | -2457 | 1046 | 470 | -1896 | -100 | 789 |
| 28 | 145.0 | 922 | 1500 | -1080 | 950 | -1148 | -280 | -3136 | 1467 | 615 | -2044 | -139 | 482 |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| AXIAL FORCE (KN) | RCE (KN) | ·2- | 91.9 | -23 | -23.2 | -22.9 | 6. | -22.8 | 8 9. | -2, | -22.8 | -12.7 | 7. |
| MOMENT(N.m) | (L | 6 | 52 | 21.1 | ₹. | 24.8 | 85 | 110.1 | 1.1 | 75 | 75.5 | 14.4 | ₩, |
| | | | | | | | | | | | | | |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN S4-C

| | L A (PROPE AN | PAWEL A (PROMT AND REAR TENESON BIASON | DIABONAL) | | | | | Test Serial No. | 2 |
|----------|---------------|--|-----------|---------|----------------|---------|--------|-----------------|--------|
| ź | Londith | | Strate | Strain. | S train | Strain. | Strain | Strain | 9train |
| | | 2 | | 4 | 16 | 20 | 8 | 34 | 27 |
| | | | | 18 | 7.8 | * | 82 | 2 | |
| 7 | | 9 | | 30 | 128 | 8 | | | 961 |
| <u>"</u> | | • | 240 | 42 | | 14 | | 5 | |
| 1 | 40.0 | 12 | | | | | | 4 | |
| 9 | 20.0 | 20 | | | | | | 76 | |
| 9 | 90.09 | | 209 | | | | | | 800 |
| 7 | 70.07 | | | | | | 773 | 5 | |
| | 75.0 | | | 122 | 528 | 2 | | 2 3 | |
| • | 0.08 | | | 3 | | | | B | |
| 10 | | | | 146 | | | | 8 ; | |
| Ξ | 0.08 | | | 3 | | | | V | 610 |
| 12 | | 8 | | 3 6 | | 3 | 9 | 2 | |
| 5 | | | | | | | | 8 | |
| ! : | | | | 2 | | | | 201 | |
| - | | | | 162 | 714 | | | 8 | 716 |
| 2 | | 3 | | 190 | 734 | | 905 | 21 | |
| 2 | 105.0 | 100 | 2 | 196 | 754 | 52 | 622 | 122 | 757 |
| 2 | 107.5 | 106 | | 202 | 772 | | 949 | 36 | |
| 9 | 110.0 | 110 | 976 | 210 | 280 | C#1 | 3 | 22 | 7// |
| 2 | 112.5 | 114 | | 216 | 908 | 871 | 878 | 2 | OR/ |
| ଥ | 115.0 | 122 | | 228 | 830 | 25 | 8 | 3 | |
| 21 | 117.5 | 130 | | 232 | 842 | 9 | 810 | 3 | |
| 22 | 120.0 | 136 | 1036 | 244 | 962 | 2, | 8 | 69 | 800 |
| EZ | 122.5 | 146 | | 254 | 982 | 871 | 8 | 72. | 900 |
| 72 | 125.0 | 156 | 1084 | 264 | 88 | 5 | 8 | 9 | 999 |
| 25 | 127.5 | 162 | | 274 | 910 | 3 | 2 | 3 | 000 |
| * | 130.0 | 176 | 1132 | 792 | 912 | 202 | 8008 | 40 | 970 |
| 27 | 133.1 | 230 | 1172 | 384 | 922 | 212 | 1054 | 200 | 990 |
| 92 | 135.0 | 350 | 1240 | 906 | 920 | 222 | 10801 | 210 | 98 |
| | | | | | | | | | |

| 8 | | | | | | | | | |
|-------------|------------------|-------|------|----------|-------|-------|------|-------|------|
| | 13/.5 | 424 | 1288 | 252 | | | | | |
| ۶ | 0077 | | | | 800 | 234 | 1110 | 200 | |
| 3 | 2 | 472 | 1324 | 212 | | | | | 1024 |
| 6 | 3 671 | 713 | | | 202 | 250 | 1140 | 228 | 4907 |
| | | | 1356 | 656 | 1014 | 096 | G P | | 7001 |
| 3 | 145.0 | 3 | 1380 | | | | 0/11 | 254 | 1080 |
| | | | | 000 | 1030 | 206 | 1180 | 272 | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | - | | | | |
| AXIAL FI | AXIAL FORCE (KN) | 2 | | * | 19.3 | 22.7 | 4 | | |
| | | | | | | 3 | • | 22.0 | |
| MOMENT(N.m) | Z.m.) | | | | | | | | |
| | | -27.4 | • | 7 | -17.7 | • | _ | | _ |
| | | | | | | 8.67- | | -23.7 | _ |
| | | | | | | | | | |
| | | | | | | | | • | • |

AXIAL FORCES AND BENGING MOMENTS IN MEMBERS FOR SPECIMEN S5-A PANEL A (NOT BUCKLED)

| ś | Lond kill | | Strain Strain Strain Strain | Strain | | Strain | Strain | Strain Strain | | Strain | Strain | Strain | Strain | Strain | Strain |
|-----|-----------|------|-----------------------------|--------|-----|--------|--------|---------------|------|--------|--------|--------|--------|--------|--------|
| t l | - | • | 2 | 3 | 7 | 8 | • | 7 | • | 9 | 10 | 11 | 12 | 13 | 14 |
| - | 10 | -11 | 10 | 6- | -30 | 6 | 29 | 29 | -30 | 20 | -19 | 72 | 26 | 8 | -100 |
| 2 | 20 | -28 | 18 | -206 | -54 | 15 | 123 | 95 | -52 | 56 | -43 | 126 | 95 | 8 | -202 |
| 3 | 30 | -43 | 27 | -299 | 11. | 20 | 176 | 82 | -73 | 70 | .63 | 240 | 87 | 10 | -330 |
| 4 | 40 | -55 | 34 | -400 | -91 | 26 | 239 | 106 | 96- | 92 | -83 | 317 | 122 | 22 | -436 |
| 5 | 50 | -72 | 43 | -516 | 96- | 34 | 310 | 136 | -120 | 114 | -100 | 398 | 167 | 38 | -538 |
| 9 | 9 | -89 | 52 | -648 | -81 | 58 | 402 | 164 | -146 | 134 | -118 | 484 | 228 | 65 | -626 |
| 7 | 65 | -95 | 52 | -705 | -60 | 60 | 450 | 176 | -158 | 138 | -122 | 530 | 273 | 82 | -660 |
| 8 | 20 | -100 | 25 | -745 | -32 | 87 | 506 | 181 | -163 | 140 | -126 | 282 | 338 | 86 | -670 |
| • | 71.6 | 96- | 87 | -740 | -14 | 112 | 528 | 179 | -161 | 136 | -124 | 604 | 378 | 105 | -656 |
| 10 | 69.3 | 98- | 96 | -586 | 14 | 168 | 518 | 140 | -124 | 138 | | 601 | 400 | 66 | -615 |
| 11 | 61.4 | 26 | -134 | -266 | 176 | 288 | 268 | 09 | -56 | 172 | -150 | 670 | 190 | 296 | -1176 |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| 1 | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |

| 3 | PANEL B(NOT BUCKLED) | 71 EC | KLED) | | | | | | | | | | | Test Serial No.2 | I No.2 |
|----|----------------------|-------|--------|--------|--------|--------|--------|---------------|-----|--------|------------|--------|--------|------------------|--------|
| 4 | Lond to Strain | | Strain | Strain | Strain | Strain | Strain | Strain Strain | | Strain | Strain | Strain | Strain | Strain | Strain |
| | | • | 2 | 3 | 4 | 8 | • | 7 | • | 6 | 10 | 11 | 12 | 13 | 14 |
| | 10 | 15 | -18 | -19 | -74 | 23 | 17 | 4 | 24 | 26 | p - | 28 | 103 | 9/- | 8- |
| 2 | 8 | 20 | -50 | -32 | -144 | 230 | 80 | -4 | 40 | 48 | -13 | 57 | 234 | -186 | -15 |
| က | 30 | 29 | -83 | -49 | -201 | 316 | 120 | -4 | 99 | 64 | -17 | 88 | 340 | -282 | -23 |
| 4 | 40 | 36 | -113 | -76 | -270 | 412 | 165 | 9- | 72 | 80 | -28 | 106 | 440 | -375 | -28 |
| C) | 50 | 53 | -148 | -113 | -339 | 504 | 213 | -8 | 89 | 101 | -35 | 140 | 532 | -476 | -50 |
| 9 | 9 | 78 | -198 | 171- | -430 | 598 | 265 | -7 | 112 | 122 | -48 | 176 | 628 | -580 | -86 |
| | , 65 | 100 | -232 | -214 | -480 | 638 | 286 | 6- | 124 | 133 | -58 | 179 | 661 | -646 | -125 |
| 80 | 70 | 140 | -284 | -280 | -556 | 668 | 292 | -11 | 145 | 158 | -72 | 174 | 700 | -742 | -184 |
| • | 71.6 | 170 | -312 | -314 | -596 | 999 | 275 | -11 | 149 | 162 | -72 | 158 | 714 | -801 | -218 |
| 10 | 69.3 | 222 | -362 | -367 | -708 | 633 | 181 | -10 | 126 | 168 | -74 | 140 | 712 | -814 | -238 |
| Ξ | 61.4 | 492 | -610 | -684 | -894 | 762 | -60 | 8- | 114 | 80 | -10 | -656 | 1056 | 2210 | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
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AXIAL FORCES AND BENGING MOMENTS IN MEMBERS FOR SPECIMEN S5-A

PANEL C(FRONT COMPRESSION DIAGONAL BUCKLED OUTSIDE TOTALLY AND REAR DIAGONAL

| نا | 44 600 | | Strain Strain Strain Strain | Strain | | Strain Strain Strain | Strain | Strain | Strain Strain | | Strain | Strain | Strain | Strain | Strain |
|--------|--------------|------|-----------------------------|----------|-------|----------------------|--------|--------|---------------|------|--------|-----------|--------|--------|--------|
| ė E | | • | 2 | 3 | 4 | 8 | • | 7 | • | 9 | 10 | 11 | 12 | 13 | * |
| | 10 | -27 | 0 | -178 | -24 | 017- | 98 | 3 | 12 | 4 | 14 | 09 | -101 | -230 | -52 |
| ~ | 20 | | 0 | -378 | -42 | 96 - | 168 | 10 | 25 | 10 | 32 | 156 | -154 | -462 | 04 |
| | | -108 | 0 | -568 | -38 | -154 | 254 | 15 | 38 | 14 | 56 | 252 | -220 | -686 | S |
| | 40 | -140 | 9 | -802 | 0 | -228 | 370 | 22 | 52 | 20 | 58 | 368 | -308 | -954 | 130 |
| 2 | 9 | -176 | 12 | -1110 | 90 | -328 | 522 | 32 | 64 | 28 | 77 | 514 | 440 | -1278 | 278 |
| 9 | 9 | -228 | 30 | -1542 | 287 | -470 | 730 | 42 | 9/ | 40 | 88 | 720 | 989- | -1700 | 736 |
| | 9 | -264 | 48 | -1786 | 420 | -568 | 870 | 90 | 78 | 48 | 92 | 860 | -770 | -2018 | 1156 |
| | | | 82 | -2748 | 884 | -732 | 1080 | 62 | 92 | 58 | 92 | 1050 | -946 | -2608 | 1548 |
| 6 | 7 | -346 | 104 | -4690 | 1780 | 008- | 1160 | 0.2 | 99 | 09 | 92 | 1130 | -1032 | -3202 | 1906 |
| 9 | 69.3 | -386 | 150 | | | -760 | 1055 | 88 | 42 | 28 | 92 | 1140 | -1036 | 998- | |
| = | 61.4 | -718 | 514 | | | -1054 | 1088 | 112 | 9 | -718 | | | | | |
| 12 | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| FO | FORCE KN | | | ਲ਼ | -38.9 | 7.1 | - | | | | | T- | 1.9 | | -21.6 |
| 04 | MOMENT (N.m) | | | <u>1</u> | 136.7 | 1.77. | 7. | | | | | 7 | -85 | 17 | 175.4 |
| | | | | | | | | | | | | | | | |

AXIAL FORCES AND BENGING MOMENTS IN MEMBERS FOR SPECIMEN 55-A

PANEL D(FRONT COMPRESSION DIAGONAL BUCKLED OUTSIDE TOTALLY AND REAR DIAGONAL

Test Serial No.2

| | 1 | | | | | | | | | | | | | | |
|-----|--------------|--------|---------------|--------------|--------|--------|--|-----------------------------|----|----------|--------|--------|--------|--------|--------|
| | | | | | | Г | | | | | Charle | Strain | Strain | Strain | Strain |
| Š | NA PEOT | Strain | Strain Strain | Strate | Strain | Strain | e de la companya de l | Strain Strain Strain attain | | 0 | 10 | + | 12 | 13 | 14 |
| _ | | | N | | 1 | 1 | 2 | • | 5, | 20 | 10. | 390 | 20 | 62 | 118 |
| - | 10 | -150 | -19 | -90 | 59 | ş | 8 | 5 | ? | /9. | | | | 62. | 22 |
| G | | | ٩ | .170 | 153 | 95 | -44 | 99 | æ | -5 | -85 | 320 | | | 3 1 |
| 7 | | | | | | -47 | -50 | 70 | 19 | -22 | -70 | 320 | -440 | 266 | 3/1- |
| ၈ | 30 | | | | | | · | 6.7 | 23 | -12 | 69- | 440 | -664 | 390 | -180 |
| 4 | 40 | -290 | 5 | -352 | 3 | Ş | ? | 3 | 1 | ; | | 610 | -1232 | 286 | -292 |
| 5 | 20 | -318 | 21 | -464 | 516 | -42 | 83 | 8 | 9 | 2 | | | | | |
| ď | | -415 | 3 | -685 | 730 | -49 | 245 | 95 | 9 | 37 | 94 | | | | |
| | | | | | 883 | -52 | 367 | 112 | 47 | 49 | -20 | | | | |
| | | | | | ľ | | 658 | 116 | 49 | 99 | -37 | , 2278 | -3340 | 1160 | -C/- |
| 8 | 70 | -492 | 2 | 201- | | | | | | | 70. | 3172 | -5022 | 1218 | -810 |
| ٥ | 71.6 | -578 | 108 | 3 -1174 | 1245 | -62 | 960 | 135 | 42 | W | | | | | |
| | | l | | | 1207 | 77. | 1891 | 114 | 57 | 74 | -76 | 3 4720 | -7730 | 200 | ? |
| 일 | 69.3 | c0c- | 140 | 0021- | ١ | | L | | | 1, | 100- | | | 1152 | -1194 |
| 11 | 61.4 | -970 | 535 | 5 -1414 | 1450 | 85 | | | 3 | | | | | | |
| | | _ | | | | | | | | | | | | | |
| | | | | | • | ; | 9 | | | | | | -20.9 | | 8.1 |
| FOR | FORCE(KN) | | | | 4. | | 0. | | | | | | | | |
| | | | | | 95.1 | 4 | -40.2 | | | | | 3 | 212.5 | '- | -79.7 |
| 0 | MOMENT (N.m) | | | <u>'</u> | | | | | | | | | | | |
| | | | | \downarrow | | | | | | | | | | | |
| _ | | | _ | _ | | | | | | | | | | | |

AXIAL FORCES AND BENGING MOMENTS IN MEMBERS FOR SPECIMEN S5-A

| | Г | 7 | 143 | 263 | 99 | 1,4 | 578 | 88 | 721 | 746 | 18 | 20 | 735 | 2 | Т | Т | Т | Т | T | |
|------------------|-----------------------------|----|------|-----------|-----------|------|------|------|------|-------|-------|-------|-------|---|---|---|---|---|---|---|
| al No.2 | Strain | | | | | | | | | | | | | | | | | | | |
| Test Serial No.2 | Strain | 13 | 8 | 114 | 129 | 173 | 218 | 172 | 309 | 315 | 216 | 134 | .170 | | | | | | | • |
| | Strain | 12 | -22 | 98 | -51 | -72 | 85 | -134 | 151- | -170 | -218 | -276 | | | | | | i | | • |
| | Strain | 11 | -125 | -225 | -318 | -426 | -560 | -736 | 448 | -1069 | -1137 | -1186 | | | | | | | | • |
| | Strain | 10 | 26 | 46 | 85 | 88 | 100 | 123 | 139 | 161 | 122 | જ | 05- | | | | | | | • |
| | Strain | | 9- | -20 | -29 | -39 | -47 | 09- | 89- | 08- | -106 | -148 | 84 | | | | | | | • |
| | Strain | • | 24 | 0# | 67 | 29 | 18 | 104 | 117 | 132 | 109 | 99 | 61 | | | | | İ | | • |
| | Strain Strain | 7 | 6- | -17 | -21 | -28 | -35 | -47 | -52 | -65 | -92 | -155 | -164 | | | | | | | |
| | Strain | • | -58 | -148 | -224 | -305 | -386 | -475 | -537 | -635 | -720 | -858 | -2026 | | | | | | | |
| | Strain Strain | 2 | -8 | ģ | -29 | -35 | 89- | -64 | 96- | -115 | -141 | -191 | 520 | | | | | | | |
| | Strain | • | 9 | 117 | 172 | 228 | 285 | 347 | 375 | 389 | 367 | 264 | 109 | | | | | | | |
| | Strain Strain Strain Strain | | 98 | 187 | 280 | 360 | 454 | 509 | 545 | 564 | 539 | 456 | 460 | | | | | | | |
| | Strain | 7 | -29 | 19 | -92 | -126 | -161 | -211 | -245 | -292 | -345 | -448 | -680 | | | | | | | |
| | | | 14 | 12 | 36 | 38 | 49 | 7 | 100 | 130 | 134 | 132 | 380 | | | | | | | |
| | Load kN | | 10 | 20 | 30 | \$ | 92 | 99 | 65 | 70 | 71.6 | 69.3 | 61.4 | | | | | | | |
| | ğ | | 7 | 2 | က | 4 | 2 | 9 | 7 | 8 | 6 | 10 | Ξ | | | | | | | |

PANEL F(NOT BUCKLED)

| | Water of Mos Bookers | | | | | | | | | | | | | Test Serial No.2 | M No.2 |
|---|----------------------|---------------|------|-----|-----|------------------------------------|--------------|--------|--------|-----|--------|--------|---------|-------------------------|--------|
| ş | Load KN | Strain Strain | | | | Strain Strain Strain Strain Strain | Strain | Strain | Strain | | Strain | Strain | Strain. | Strain | Strain |
| | | | ~ | 7 | • | 8 | • | 7 | • | 9 | 10 | + | 12 | 13 | 7 |
| | 9 | -16 | 10 | -10 | 70 | -92 | -25 | 22 | 61- | 37 | -32 | 98 | .125 | 100 | ľ |
| 2 | 20 | -20 | 20 | 5 | 148 | -210 | 0 5 - | 44 | 96- | 71 | 75- | | | | 36 |
| 3 | 30 | -40 | 27 | 15 | 217 | 906- | 29- | 8 | -51 | 97 | -78 | | | | S |
| * | 40 | -60 | 36 | 27 | | -411 | -73 | 8 | 65 | 124 | -103 | | | 707 | 200 |
| 5 | 50 | -71 | 77 | 33 | 370 | -522 | 62- | 103 | 1 | 155 | -127 | | | | 60 |
| 9 | 99 | 9- | 51 | 35 | 451 | -626 | 89 | 110 | ę | 180 | 151 | 6. | | | 8 8 |
| 7 | 65 | -91 | 25 | 38 | 511 | -670 | \$ | 117 | -92 | 189 | 164 | | | | 5 |
| 8 | 70 | -96 | 50 | 60 | 561 | -700 | -44 | 110 | -92 | 189 | -166 | | | | 170 |
| 0 | 71.6 | -95 | 45 | 8 | 986 | -680 | 9 | 110 | -87 | ž | 157 | | | 252 | 386 |
| 5 | 69.3 | 08- | 44 | 128 | 296 | 909- | -37 | 102 | 92- | 164 | .140 | | | 20Z | e e |
| Ξ | 61.4 | 112 | -152 | 276 | 701 | -217 | ₽ | - | ^ | 212 | -176 | | | 780 | 140 |
| | | | | | | | | | | | | | 1000 | 3 | |
| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |
| | | | | - | | | | | | | | | | | |
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| | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN SS-B

| | EL C (FRO | PANEL C (FRONT DIAGONAL BUDKLED) | MAL BUD! | (GED) | | | | | | | Teet Sected Mo. 10 | Ş | |
|-------------|------------------|----------------------------------|----------|--------|--------|--------------|--------|--------|--------|--------|--------------------|---------|--------|
| ş | Load kill | Strain | Strain | Strain | Strain | Strade. | Strade | Strain | Strate | Strain | Strain. | Strain. | Strain |
| | | • | 2 | • | | 9 | • | 7 | • | • | 9 | | 12 |
| | 11.8 | S. | .130 | -108 | -86 | .152 | 23 | 951- | 02. | 01- | , | | 100 |
| | 202 | -83 | -272 | | -168 | -273 | | | | | | | 120 |
| | 30 | 92 | -512 | -323 | -240 | | | 115. | | | | | CGL. |
| | \$ | -37 | -588 | | -326 | | | .623 | | | | | 612- |
| | 50 | 0 | -637 | -454 | .389 | | | 287. | | | | | 248 |
| 9 | 98 | 8 | -1024 | -533 | -477 | 296 - | | 946 | | | | | 905 |
| 7 | 2 | 2 | .1208 | * | -512 | 7 | | 1092 | | | | 9/6- | Sec. |
| 8 | 75 | 9 | .1296 | Ÿ | -566 | -1188 | 0 | 1140 | | 406 | | 099 | 450 |
| 8 | 8 | 144 | 1371 | 029 | 995 | -1294 | 4 | .1238 | | 697 | | 200 | 700 |
| 9 | 88 | 206 | -1525 | 675 | -623 | -1382 | 24 | 1340 | | 570 | | 32. | 307 |
| = | | 277 | -1675 | 069 | -675 | .1592 | 128 | -1461 | 51 | 674 | | .83 | 460 |
| 22 | | 352 | 1796 | .764 | 711. | -1694 | 176 | 1521 | 98 | 722 | | .850 | 446 |
| ត | 87.5 | 164 | -1667 | .700 | -729 | -1734 | 188 | .1440 | 0 | 512 | | 787 | - |
| = | 100 | 432 | -1937 | -m- | -754 | -2225 | 783 | -1430 | 8 | 8 | | | |
| 15 | 9.96 | | | | | | | | | | | | 3 |
| 16 | | | | | | | | | | | | | |
| AXIAL ! | AXIAL FORCE (KN) | -29.8 | 80 | -30.3 | e, | -33.2 | 8 | -27.9 | 6. | -25.0 | 5.0 | -33.0 | 0. |
| MOMENT(N.m) | П(м.m) | 93.1 | - | 6.0 | | -106.6 | 5.6 | 57 | | 121 | 121.5 | + | - |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN 85-B

| | AHEL C (NEAR BIAGORAL HOT BU | TWECHE | | CKLED) | | | | | | i | Test Serial No. 10 | No. 10 | |
|------------------|------------------------------|--------|--------|--------------|-------|--------|--------|--------|--------|--------|--------------------|---------------|--------|
| į | Lead RN | | Strain | Strain. | Strat | Strate | Strain | Strain | Strain | Strain | Strain | Strain | Strain |
| | | | 7 | 8. | 2 | 21 | 22 | 23 | 24 | 26 | * | 27 | 8 |
| • | 11.8 | 33 | .123 | .72 | -18 | 96- | 9 | 26- | 4 | 108 | 24 | 7.7 | 30 |
| 2 | 20 | 55 | 2. | -117 | 06- | .163 | 12 | 191 | 12 | | | | 3 |
| 3 | 30 | 164 | | 272- | 59- | .383 | | | 2 | | _ | | 3 |
| * | 40 | 217 | 9. | | 174 | | | | 8 | | | | 910. |
| \$ | 09 | | | | 8 | | | | 3 8 | | | | 141 |
| 9 | | | ' | | 8 | | | | 136 | | | | -173 |
| | | | | | Ŗ | | 167 | \$08· | 190 | -880 | 332 | 300 | -200 |
| , | | 533 | .1234 | 950 | 201 | 906 | 219 | .944 | 246 | .1028 | 408 | -340 | -222 |
| 8 | 75 | 583 | .1325 | 999 | 106 | -1003 | 245 | -1014 | 276 | 1096 | 448 | 096- | -230 |
| 6 | 8 | 9 | .1422 | .700 | .105 | -1076 | 277 | -1089 | 312 | | | | .240 |
| 10 | 98 | 715 | 1548 | .755 | -106 | 1711 | 317 | .1183 | 358 | | | | 250 |
| 11 | 86 | 816 | .1712 | -825 | -102 | .1297 | 375 | -1314 | 424 | | | | 26. |
| 12 | 95 | 932 | -1888 | 769 - | 8. | -1430 | 445 | -1453 | 503 | | | | 07.6 |
| 13 | 87.5 | 1322 | -2274 | -1048 | 33 | | 006 | 1706 | 750 | | | 72.7 | 606 |
| 14 | 100 | 5921 | -2866 | -1290 | 120 | | ē | 201- | 8 | | | | 203 |
| 15 | 9 98 | | 56.50 | 6600 | 100 | | | | 1 | | | /00. | -Z- |
| 19 | | | 2315. | 201 | 2 | G. | 2002 | -2371 | 100 | -2390 | 1900 | -642 | -238 |
| AXIAL FORCE (KN) | TCE (KN) | -16.9 | 0,1 | .22. | C | 107 | | 1 8 | | | | | |
| | | | | | | | | 3 | | - | *·71- | + ./1- | • |
| MOMENT(N.m) | М.т) | 164.4 | * | 55.4 | 4 | 109.1 | 7. | 112.1 | 7. | 1,4 | 145.3 | 15.9 | o, |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN SS-B

| | C (FRONT AND | PAMEL C (FRONT AND REAR TENENON DIAGONAL) | MONTH) | | | | | Test Serial No. 10 | • |
|-------------|------------------|---|----------|-------------|-------------|--------------|--------|--------------------|---|
| ğ | Leed IV | Strain. | - Strain | Strafe | Strain | Strain | Strain | Strado | Strain |
| | | 13 | 20 | 15 | 16 | 20 | 200 | 31 | *************************************** |
| | 11.8 | -10 | 29 | -10 | 199 | -34 | 9 | 9 | |
| 2 | 2 | 0 | 104 | .20 | 100 | 3 5. | 20 | 99 | 78 |
| 3 | 30 | 95. | 228 | 3 6- | 218 | 118 | 168 | 291. | |
| | 40 | 77. | 284 | -66 | 0.2 | .142 | 214 | 1981 | 67.6 |
| 9 | 92 | 401. | 374 | -92 | +5 C | 881. | 282 | -268 | 37.6 |
| 9 | 99 | .138 | 458 | -124 | 430 | ≯ 22· | 370 | 332 | 476 |
| 7 | 20 | .168 | 534 | -146 | 408 | -256 | 434 | 388 | 284 |
| 9 | 75 | 182 | 572 | .158 | 532 | -268 | 897 | 414 | Rin |
| 6 | 90 | 1981 | 612 | -172 | 999 | .286 | 504 | -442 | 859 |
| 5 | 88 | .220 | 999 | 186 | 919 | 70 E | 920 | 4.78 | 718 |
| = | 96 | .246 | 738 | -214 | 829 | -334 | 612 | 925 | 962 |
| 12 | 2 8 | .276 | 908 | -236 | 742 | -374 | 678 | | 878 |
| 5 | 87.5 | .278 | 788 | .270 | 752 | 068- | 910 | 026. | 979 |
| 1 | 180 | -324 | * | 8C1:- | 798 | 1112 | 1166 | 1200 | |
| 15 | 96.6 | -714 | 0001 | 878- | 1020 | 1308 | USC. | 3061 | 900 |
| 18 | | | | | | | | 0001 | 1900 |
| AXIAL F | AXIAL FORCE (KN) | 11.1 | .1 | 10 | 10.4 | 1.1 | | 0 | |
| MOMENT(N.m) | T(N.m) | -47.6 | 7.6 | 7 | -46.5 | -89.6 | 97 | -94.9 | 6. |
| | | | | | | | | | |
| | | | | | | | | | |

AXIAL FORCES AND BENDING MOMENTS IN MEMBERS FOR SPECIMEN SS-B

| PAN | EL C (THI | PANEL C (THREE LEGS) | ĺ | | | | | | | | Test Serial Mo 40 | Ş | |
|-------------|-----------------|----------------------|--------|----------|------------|--------------------|----------------|--------|--------|----------------|-------------------|---------|---------|
| į | Na beel | Strain 22 | Strain | Strain . | Strate | a de la composição | Otrain near | Strain | Strain | Bitrain | | - Break | 9 trade |
| | | | | | | | | R | \$ | \$ | \$ | \$ | 3 |
| | | | | 9 | .9 | 13 | 0 | 0 | 24 | 24 | 14 | • | 8 |
| " | 20 | 86 | 35 | 10 | 94. | 24 | 0 | 0 | 32 | 32 | 14 | | |
| " | 30 | .200 | 110 | 82 | .94 | 42 | 0 | 0 | 9 | | | | |
| 1 | \$ | -242 | 134 | | • | | | | | | | | |
| 2 | 50 | 322 | 180 | | | | | | | | | | |
| 9 | 9 | 390 | 220 | 28 | 0/1- | 96 | | | | | | | e ; |
| 7 | 8 | -450 | | | | | | | | | | | 3 |
| 8 | 75 | 478 | | | | | | | | | | | 901 |
| G | 86 | -512 | 284 | | | | | | | | | | 801 |
| 10 | 885 | .552 | 318 | | | | | | 021 | 671 | | | 122 |
| = | 86 | 909- | 350 | | -256 | | | | 921 | 2 | | | 8 |
| 12 | | 999- | 390 | 95 | -278 | | | | 136 | 168 | | | 20 25 |
| ± | 87.5 | .758 | 496 | 88 | -306 | | | | 162 | 176 | | | P. C. |
| = | 100 | 806 - | 620 | 120 | 196- | 22 | | | 72. | 1 | | ٩ | 80 |
| 15 | 98.6 | .1280 | 964 | 248 | -466 | 8 | | | 8 | | | ? ! | 2 |
| 16 | | | | | | | | | 3 | | 8 | 48 | 10 |
| AXIAL | AXIAL FORCE(IN) | -5.7 | 7. | 7 | 9.1 | 2.6 | 9 | 3.2 | 2 | | 1.6 | 3.1 | |
| MONENT(N.m) | T(N.m) | 60.0 | 0: | 18.6 | 6 | -0.5 | rč. | -7.A | 4 | + | -11.6 | -6.7 | 7 |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |

AXIAL FORCES AND BENDING MOMENT IN TEST MEMBERS FOR SPECIMEN SS-C

| | T PANEL C (FI | TEST PANEL C (FRONT DIAGONAL BUCK | BUCKLED FIRST | (1) | | | | S Test OF | Test Serial No. 12 |
|-----------------------------|-----------------------------|--|----------------|--------------|--------|-------------|--------|-----------|--------------------|
| į | Leadith | a de la composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della composition della comp | strate | ŧ | otrate | strain | otrain | strate | otrain |
| | | - | 2 | 2 | • | | | | • |
| | 14.6 | 128 | | S1. | -49 | 8 2. | | 35 | 15. |
| 2 | 28.3 | 133 | | 88 7. | | | • | | 64 |
| 0 | 43.9 | 437 | | | .119 | | | | 28: |
| • | 56.5 | 593 | | - P44 | .123 | • | | | |
| £ | 7.07 | 287. | 981. | | | | | | |
| 9 | 84.8 | 1336 | .37 | | | | | | 2 |
| 7 | 91.8 | 90+1 | | | 197 | | | | |
| • | 7.86 | 2991 | | .1665 | | | | | |
| 6 | 6.08 | 9741. | 12 | | | | 757 | | |
| QI. | 100.5 | 9051 | 27 | .1762 | | | | | 787 |
| = | 102.2 | 1521 | 24 | 1824 | ESE . | | | | |
| 12 | 104.0 | 1524 | 12 | | | | | | |
| : | 186.0 | 9631- | 2 | -1948 | 499 | | | | |
| 2 | 108.0 | 1487 | S | -2025 | 819 | | | | 968 |
| 15 | 111.1 | 1337 | .211 | -2165 | | | 98 | | |
| 2 | 114.3 | | CO+- | .2318 | 1283 | ₩ZS: | | | |
| 22 | 116.3 | 38 | 016. | 3665 | 2305 | 681 | | | |
| = | 110.6 | -01 | 1451 | -6636 | | Z*- | | 523 | |
| 2 | | 788 | 1966 | -14938 | 12376 | ZEC: | | | |
| R | | | .2001 | -15446 | | | 88 | | |
| Ž. | 123.0 | 798 | -2386 | -16273 | | 216- | | | |
| 8 | 107.4 | | 2031 | .15823 | 06161 | | 988 | | |
| 23 | 109.4 | 763 | -2062 | 15897 | 13250 | 976. | | | |
| 72 | 10.8 | | -20 8 4 | 15958 | 13297 | 78 0 | | | |
| \$ | | | 1112. | .16033 | 13358 | | | | |
| 8 | 114.5 | 282 | -2136 | .16116 | 13423 | .396 | | | |
| 27 | 115.4 | 919 | 7715. | 16274 | 13550 | -406 | | | |
| 8 | 105.0 | | -20 6 4 | 16674 | 13915 | -451 | 1153 | | |
| 8 | 106.7 | 803 | 1966 | .24797 | 22269 | -963 | 1120 | • | |
| ARIAL FORCE (| ATIAL FORCE (MI) FOR VIBLAM | 30.2 | 2 | 29.0 | 0.0 | 4 | - | | |
| DENOMIC INCIDENT(N.m.) | ENT(N.m) | 1.8 | | 5 | 1 | ę. | -53.7 | - | -53.1 |
| ANSAL FORCE (187)for 123.9M | Myler 123.966 | -28.4 | * | 4.7 | 7. | ** | 13.7 | | 12.4 |
| DENDING MONENTINE, | ENT(N.m.) | 125.4 | | 251.7 | 7.1 | ç. | -51.9 | T | -60.0 |

AXIAL FORCES AND BENDING MOMENT IN TEST MEMBERS FOR SPECIMEN 85-C

| TES | IT PANEL C (R | TEST PANEL C (REAR DIAGONAL BUCKL | BUCKLED SECOND | (OH(| | | | Test Ser | Test Serial No. 12 |
|-----------------------------|--------------------------------|-----------------------------------|----------------|--------|--------|----------|--------|----------|--------------------|
| ź | Leadhin | ateria | strate | strain | straie | otrate | otrate | strain | otrate |
| | | | * | 11 | 12 | 13 | * | * | * |
| • | 14.8 | 151. | 15: | 521. | P2. | 65. | 97 | | 5 |
| 2 | 28.3 | .276 | | -268 | | | | | |
| 3 | 43.9 | -487 | | | | • | 190 | | |
| • | 56.5 | -662 | 28 | | | | | | |
| 9 | 7.07 | | | | | | | | 200 |
| 9 | 9.79 | .1429 | | | | 968: | | | |
| 7 | 91.0 | -1495 | | | | | | | |
| • | 7.38 | 1564 | | | | | | | |
| • | 88 | 1586 | 279 | | 378 | -444 | 728 | | |
| ů. | 100.5 | 1618 | | | | | | | |
| = | 102.2 | .1652 | | | | | | | |
| 12 | 104.0 | -1685 | | .1783 | | | | 79- | |
| ţ | 106.0 | 170 | | | | | | | |
| * | 108.0 | -1752 | | | | | | | 2 |
| 15 | 111.1 | 1796 | | | | | | | |
| 16 | 114.3 | .1622 | | | | | | | |
| 17 | 116.3 | 1836 | | | | | | | |
| 92 | 118.8 | 1631 | | | | | | | |
| 9 | 120.4 | 1741 | | | | | | | |
| ଛ | 122.6 | .1719 | | | | | | | 1115 |
| Z | 123.0 | .1662 | | | | | 1038 | | 181 |
| 22 | 107.4 | .1828 | 667 | | | | | | |
| 23 | 109.4 | 6691 | | | | | | | |
| 2 | 110.8 | 1776 | | 4796 | 1875 | 1074 | 1155 | 9+11- | 1355 |
| XI | 113.2 | .1680 | 36 | 920S· | | | | | |
| 8 | 114.5 | 1516 | | 5895 | 2281 | 1089 | | | 1416 |
| 27 | 115.4 | 1212 | 6 | 9999- | | 2601 | 1176 | | |
| 2 | 105.0 | 548 | 100 | 7874 | 3386 | . 1222 | | | |
| 8 | 106.7 | 951 | 583 | .8766 | 3882 | 1140 | 0001 | | |
| ANDAL FORCE (| AKIAL FONCE (140) FOR 106.06.H | 57.3 | 7.3 | ĸ. | | 6.4 | Į. | 2 | 7.8 |
| DENDAND INCHENTINA | ENT(N.m) | 8 | 13 | 67.9 | | S | 91 | 3. | 2.1 |
| AXIAL FORCE (IM)Aer 123.9km | Milher 123.9600 | 8 | 30.2 | -40.4 | 7.4 | 8.6 | œ | - | 11.5 |
| DEHORIGI INCHERIT(N.m) | EMT(N.m) | 72.1 | 2.1 | 145.3 | 13 | -42 | 2.1 | Ť | -67.6 |

AXIAL FORCES AND BENDING MOMENT IN TEST MEMBERS FOR SPECIMEN SS-C

TEST PANEL C (LEGS)

| i | | etrete | 1 | alerate . | - | 1 | 1 | | | | | Ę | Serial No. 12 |
|-----------------|------------------------|--------|-----|-----------|----------|------|-----|------|-----|----------|----|-----------|---------------|
| | | 44 | _ | * | <u> </u> | _ | | | | Į | 4 | Strate | Derete |
| - | 101 | 39 | | | | | | | | | * | - | 2 |
| ~ | 28 | | 8 | | | | | | = | = | 2 | 2 | 4. |
| | | | | | 8 | | | | 8 | 8 | | 6 | 3 |
| • | 7 | | | أ أ | | 3 | | ~ | 25 | 95 | 5 | 3 | 3 |
| | | | | | | | 7 | 6 | 74 | | _ | | 1 |
| 1 | 2 | | | | | | ç | • | 68 | | ٥ | | |
| | 1 | | | | | | 91. | 13 | | | | | 8 |
| 7 | = | | | | | | 11. | | | | | | 22 |
| 1 | 3 | 3 | | | | | | | | | 12 | | 130 |
| • | 8 | | | | | | | | | | | | 137 |
| 2 | | | | | | | | | | | | | 138 |
| = | 100.2 | | | | | | | | | | | 24 | 98. |
| 12 | | | | | | | | | | | - | | 130 |
| 1.0 | | | | | | | | | | | | | 140 |
| 2 | 1000 | | | | | | | | | The Back | | | |
| 2 | | | | | | | | | | | 9 | | |
| 1 | | | | | | | | | | | | | 2 |
| 1 | | | | | | | | | | | | | |
| 1 | | | | | | | | | | | | | |
| | | | | | | | | | | | | | 8 |
| 1 | | | | | | | | | | | | | |
| 1 | | | | | 2 | | 8 | | | 149 | 92 | E | 1 |
| 1 | | | | | | | | | | 1.7 | | 1000 1000 | |
| ST S | | 3 | 701 | " | | 116 | 1.0 | 6 | 153 | 651 | 8 | 400 | X |
| 3 2 | | | 716 | | | 916 | | 11 | | | 8 | | |
| र्ग र | | | 73 | | .374 | 116 | | 13 | | | | ٤ | 8 3 |
| Q 2 | | | 260 | • | .377 | 11 | | 16 | | | | 3 8 | à |
| | | | 280 | | Š | = | | 8 | | | | 9 | 9 |
| 1 | | | 8 | | ā | 101 | 98 | 27 | | 16.0 | - | | 25 |
| | non! | | 978 | | OŞ. | 0 | 2 | 28 | | 3 | - | | 8 |
| | 100 | | | | -203 | Ş | 180 | 24 | | 2 | 25 | 2 8 | 3 ' |
| | | 6.191 | | . 281- | - | 25 | | 53 | 1 | 3 | | 3 | |
| | | 7 | | 1627.2 | * | \$ | | | - | 4 | - | 1 | |
| 1 | AL FORCE (MINE 122 MAI | 127.2 | Ŋ | 124.2 | 5 | 71.7 | 2 | 70.9 | 9 | 68.2 | 2 | 69 | |
| CHEST SOCIALISM | Train) | 4703.6 | | 1231 3 | 3 | 7863 | 3 | 3246 | 9 | 4 | | 3 | |

AXIAL FORCES AND BENDING MOMENT IN TEST MEMBERS FOR SPECIMEN SG-A

| 98 | | | | | | | | | | Test Serial No. | 1 No. 11 |
|--|-----------|------------|-------|--------|----------|--------------|--------|--------|--------|-----------------|----------|
| 10 10 10 10 10 10 10 10 | į | _ | | strate | 4 | | otrate | etrate | ptrain | • | iet |
| 1.00 | | | | | | | | | • | 1 | |
| 200 -140 -140 -40 -140 - | | 001 | | | | | | ~ | 2 | ٩ | 3 |
| 900 348 440 250 461 10 61 10 <t< td=""><td>2</td><td>20.2</td><td></td><td></td><td></td><td></td><td></td><td></td><td>117</td><td>2</td><td>305</td></t<> | 2 | 20.2 | | | | | | | 117 | 2 | 305 |
| 4.40 3.37 5.50 -5 | 3 | 30.0 | | | | | | | 175 | 4 | 795 |
| 0.00 442 440 410 110 120 200 <td>7</td> <td>40.0</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>239</td> <td>27</td> <td>100</td> | 7 | 40.0 | | | | | | | 239 | 27 | 100 |
| 0.00 4.50 4.50 1.70 2.50 4.50 <th< td=""><td>5</td><td>20.0</td><td></td><td></td><td></td><td></td><td></td><td></td><td>305</td><td>8</td><td>28</td></th<> | 5 | 20.0 | | | | | | | 305 | 8 | 28 |
| 7.70 .61 .62 .63 .145 .62 .63 .61 .65 .61 .61 .62 .61 .62 .61 .62 .61 .62 .63 .64 </td <td>•</td> <td>0.09</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td>362</td> <td>2</td> <td>345</td> | • | 0.09 | | | | | | | 362 | 2 | 345 |
| 110 | 7 | 70.5 | | | | | | | \$24 | 5 | 707 |
| 1.10 + | 7 | 90.2 | | | | | | | 087 | 98 | 9 |
| 110 | 6 | 0.18 | | | | | | | 585 | 8 | 163 |
| 110 1100 1 | 9 | 100.9 | | | | | | | 009 | 52 | 878 |
| 115.6 115.0 115.0 120 250 250 650 650 670 6 | = | 110.5 | | | | | | | 959 | • | 2 |
| 122 b 123 b 472 b 226 b 472 b 226 b 774 b 26 b 122 b 122 | 12 | 115.9 | | | | | | | 969 | 6 | 673 |
| 1226 1230 1230 1102 <th< td=""><td>5</td><td>121.9</td><td></td><td></td><td></td><td></td><td></td><td></td><td>734</td><td>8</td><td>210</td></th<> | 5 | 121.9 | | | | | | | 734 | 8 | 210 |
| 1326 1369 1360 <th< td=""><td>2</td><td>127.6</td><td></td><td></td><td></td><td></td><td></td><td></td><td>77.4</td><td>88</td><td>748</td></th<> | 2 | 127.6 | | | | | | | 77.4 | 88 | 748 |
| 138 b 1427 110 100 600 600 600 100 100 144 1 145 1 145 2 1143 225 256 176 114 144 1 145 2 112 2 230 73 60 172 175 152 6 175 6 249 1220 261 60 176 176 160 7 162 7 229 261 60 100 116 116 160 2 162 7 230 112 7 266 60 101 116 160 2 161 2 250 266 266 100 116 116 144 2 141 2 116 3 117 266 266 100 116 142 3 211 3 118 4 118 4 118 4 118 4 118 142 4 4 3 114 4 4 4 4 114 4 4 4 4 114 4 4 4 4 114 4 4 4 4 4 114 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | 15 | 132.6 | | | | .22: | | | 608 | 104 | 1 |
| 144 152 144 226 726 726 114 600 114 600 114 600 114 600 114 600 114 62 114 62 112 62 112 62 115 62 116 | 92 | 136.9 | | | | | | | 98 | 100 | 910 |
| 152 156 156 248 152 | 17 | 144.1 | 1531 | | | | | | 296 | 411 | 1.58 |
| 152.0 113.0 124.0 125.0 126. | 9 | 149.5 | | | | | | | 935 | 122 | 506 |
| 157.6 152.6 152.0 23.1 6.9 99.1 116 <th< td=""><td>9</td><td>152.0</td><td></td><td></td><td></td><td></td><td></td><td></td><td>862</td><td>126</td><td>100</td></th<> | 9 | 152.0 | | | | | | | 862 | 126 | 100 |
| 1602 11603 366 1223 366 1009 111 144.5 -1784 384 -1167 -285 36 961 67 140.2 -1842 -1842 -285 42 968 93 97 141.6 -1813 -1166 -313 48 1019 113 114 142.7 -2136 -781 -117 -418 58 1164 121 114 | 2 | 157.6 | 2081 | | | | | | 166 | 116 | 296 |
| 1445 .1784 .384 .1167 .286 .286 .881 .87 .87 1402 .1862 .41 .1176 .296 .42 .966 .83 | 2 | 160.2 | | | | | | | 6001 | = | 86 |
| 1416 1962 42 980 42 980 623 62 | 2 | 144.5 | | 8 | | 282 | | | 196 | 48 | 8 |
| 1416 1911 453 1189 313 49 1019 103 103 103 103 103 103 103 113 114< | R | 140.2 | .1842 | | | 282 : | | | 986 | 8 | 588 |
| 142.0 .201.3 .201.3 .50.1 .110.4 .50.1 .110.4 .114.2 .201.3 .201.3 .114.2 .114.2 .114.2 .114.2 .114.3 .112.3 .114.2 .112.3 <td>2</td> <td>141.6</td> <td>1161-</td> <td></td> <td></td> <td>.313</td> <td></td> <td></td> <td>6101</td> <td>103</td> <td>885</td> | 2 | 141.6 | 1161- | | | .313 | | | 6101 | 103 | 885 |
| 1127 2196 729 1114 419 549 1124 121 | 8 | 142.0 | 2113 | | | 196. | | | 1097 | 7.1 | 9901 |
| 14.2 -220 | R | 142.7 | 2196 | | | -419 | | | 1124 | 121 | 9601 |
| -27.3 66131 1074 -460 70 1142 157 108.0 -9809 6131 1624 -2554 -182 1236 36 -27.3 -31.2 23.9 24.6 120.8 26.1 -36.1 -36.5 -36.5 | 2 | 143 | *22. | 3 | | 157 | | | 1144 | 121 | 1110 |
| 120.6 1824 1854 1826 1826 356 | 8 | | 2233 | 96 | | 087 | | | 1142 | 137 | 1113 |
| -27.3 -31.2 23.9 | 88 | 106.0 | 6086 | 6131 | | 1555 | | | 1236 | 8 | 1134 |
| -27.3 -31.2 23.9 120.8 24.5 | | | | | | | | | | | |
| -27.3 -31.2 23.9 120.8 28.1 42.5 | | | | | | | | | | | |
| 120.8 26.1 42.5 | IXIAL FOI | ICE (KN) | -27 | .3 | <u> </u> | 7:7 | ห | 3.9 | | 24.6 | |
| | ENDING IN | OMENT(N.m) | 120 | 91 | 75 | 13 | 7 | 2.5 | | 1 | |

AXIAL FORCES AND BENDING MOMENT IN TEST MEMBERS FOR SPECIMEN S6-A

| | | | | | | | | 1, | | |
|---------|---------------------|---------------|--------|----------|--------|--------|--------|--------|----------|-------|
| ź | (conf(th)) | otrate | aterde | etrain | strain | otrain | strate | otente | etrate | |
| | | • | • | 44 | 12 | 13 | 8 | 2 | ? | = |
| | 10.0 | π. | 21. | . 90 | 11. | | 0 | 28 | 9 | 5 |
| | 20.2 | 591. | .27 | | | | 9 | 136 | = | 25 |
| | 30.0 | , 234 | .37 | . 256 | | | 6 | 961 | 17 | 151 |
| | 40.0 | 315 | -47 | | | | 21 | -Se | 183 | 243 |
| | 50.0 | 986. | 95 | | | | 7 | 326 | 88 | 302 |
| | 60.0 | 474. | 29: | | | | 25 | 98 | 1 | 36. |
| | 7 70.5 | .558 | .68 | .636 | | | - | 453 | 3 | 423 |
| | 8 60.2 | - PEG2 | ο. | | | | 0 | 512 | 3 | 478 |
| | 91.0 | .720 | .72 | | | 98 | 0 | 005 | 92 | 275 |
| | 1009 | .792 | 11. | -908· | | | 6 | 629 | 8 | 5.95 |
| - | 110.5 | 6949 | 69: | | | | 0 | 969 | -6 | 650 |
| _ | 115.9 | 128: | .66 | | | | | 730 | 90 | 88 |
| | 13 121.9 | 69 8 : | -62 | | | | - | 778 | 116 | 722 |
| | 14 127.6 | 2201- | | .1282 | | | 0 | 817 | 123 | 759 |
| - | 132.6 | 9901 | 35 | | | | 2 | 653 | 181 | 780 |
| | 138.9 | 2011 . | 05. | | | | - | 883 | 8 | 916 |
| - | 17 144.1 | 6511. | 6.3 | .1478 | | | 9 | \$28 | 971 | 759 |
| - | 16 149.5 | 1224 | æ | | | | 2 | 21.6 | 163 | 8 |
| - | 19 152.0 | .1262 | 82: | | | | 2 | 1001 | 170 | 28 |
| 24 | 20 157.6 | 1348 | 6. | | | | 9 | 1071 | 178 | 8 |
| C4 | 21 160.2 | .1372 | 3 | | | | 3 | 1093 | 96 | 10101 |
| ~ | 22 144.5 | 9611 | æ | 0521 | | 186 | 6 | 986 | 223 | 8 |
| 2 | 23 140.2 | 1307 | 211 | | | | 2 | 856 | 3 | 963 |
| 2 | 24 | 1469 | 208 | .2067 | | | 6 | 972 | ģ | 568 |
| 2 | 25 142.0 | 1786 | 141 | .2473 | | | | 1060 | .267 | 970 |
| S | 142.7 | -2001 | 565 | | | | 2 | 660) | 306 | 1003 |
| " | 27 144.3 | -2104 | 123 | -2860 | C963 | 109- | | 1134 | ŝ | 1033 |
| ο, | 28 | 2022 | 715 | 3128 | | | 1 | 1167 | 98, | 1062 |
| Ö | 106.0 | -8457 | 7298 | 248 | | | | 1298 | 13 | 1042 |
| | | | | | | | | | | |
| | | | | | | | | | | |
| AXIAL | AXIAL FORCE (KN) | -29.2 | ci. | ਲ | -38.5 | * | 14.5 | | 13.8 | |
| BENCHIG | BENDANG MOMENT(N.m) | 9901 | • | 127.1 | 7.1 | • | -60.3 | | • 13. | |

AXIAL FORCES AND BENDING MOMENT IN TEST MEMBERS FOR SPECIMEN SO.A

| | TEST PANEL A (LEGS) | . A (LEGS) | | | | | | | | | | Test Se | ried Min. 11 |
|-----------|---------------------|------------|-------|-------|-------|----|-------|--------|--------|--------|--------|---------|--------------|
| į | (Penditte) | dende | dende | 40.40 | 4 | į | 1 | otrate | otrate | Berein | Derein | Octobe | Obrata 1 |
| | | = | • | | 2 | | 21 | 22 | 23 | 72 | | | 2 |
| | 100 | 9 | | | e, | Ņ | 5 | ē | | μ, | - | 8 | |
| | 8 | 51. | | | ŝ. | | 10 | 1. | | - | 1 | | |
| | 300 | 5 | | | Ţ. | 9 | 1.1 | - 6. | | | = | - | |
| | 40.0 | œ. | 30 | | | ., | | 25 | | | 91 | 2. | |
| | 9 | .4. | - | | 12 | 7 | | | | | 9 | 2 | |
| | 9 | 9 | 9 | | 15 | | | | | | 8 | 21 | |
| | 7 70. | | 23 | | 81 | | | | | | | 3 | |
| | 802 | | | | 12. | | | | | | | | |
| | 166 | | 16 31 | | | | | | | | | | |
| _ | 100 100 9 | | | | | | | | | | | | |
| _ | 1105 | | | | | | | | | | | | |
| _ | 1159 | | | | | | | | | | | | |
| _ | 121.9 | -105 | | | | | | | | | | | |
| | 127 6 | -112 | | | | | | | | | | | |
| _ | 15 1326 | -118 | | | | | | | | | | | |
| | 15 138 9 | .122 | | | | | | | | | | | |
| | 17 1661 | 128 | | | | | | | | | | | |
| | 18 1495 | -138 | | | | | | | | | | | |
| - | 19 1520 | .164 | | | | | | | | | | | |
| ** | 20 157.6 | .163 | | | | | | | | | | | |
| ~ | 21 1602 | .166 | 2 | | 01- | | 118 | | 330 | | | Z, | |
| ~ | 22 | 221. | | | | | | | | | | | |
| 6 | 2001 | £. | ē. | | | | | | | | | | |
| 2 | | -6- | Ş | | | | | | | | | | |
| 2 | | 9 | | | Ş | | | | | | | | |
| ٦ | | | | | 15. | | | | | | | | |
| " | 77 | | - 167 | | 4 | | | | | | | | |
| 6 | 8 | 37 | | - | 13 E | 8 | | | | | | | |
| Ci | 1080 | 8 | 89 | - | .75 | | | | | | 300 | 233 | 282 |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| AXIAL | AXIAL FORCE (KN) | -33.9 | 1.9 | 7 | -20.6 | | 16.9 | _ | 17.6 | | 13.9 | | 22.1 |
| | ENDING MOMENT(N. | 6417 | 6, | 8 | 6122 | | .1124 | | 203 | | | | |

AXIAL FORCES AND BENDING MOMENT IN TEST MEMBERS FOR SPECIMEN 86-B

| ź | | | Bersin | 1 | - Serate | Otrafa | Strate | Strate | Strate | |
|----------|--|-------|------------|------|----------|---------|--------|------------|--------|------|
| | | | 1 | 2 | 3 | • | - | • | • | |
| | 723.7 | 13 | 721. | | 11. | 144 | | - | Ž | |
| 2 | 9.09 | 22 | -313 | | | | 9 | 8 | 06 | |
| 3 | 9.96 | 9 | | | | | - | 63 | 157 | |
| * | A.TT. | 3 | | | | | 4 | 8 | 2867 | N N |
| 8 | 1.88 | 16 | | | | | • | 252 | 98 | 1 |
| 8 | 106.5 | 106 | 2039 | | | | 4 | 143 | 759 | 36 |
| 7 | .114.5 | 123 | | | | | 0 | 159 | 623 | |
| 9 | 124.1 | 140 | | | 9801 | | | 179 | 2 | 8 8 |
| • | 1334 | 159 | .1059 | | • | | 9 | 961 | 28 | 8 |
| Ş | .142.4 | 179 | | | | | 7 | 219 | 1016 | 201 |
| = | 7.151. | 202 | | | | | | 239 | 1078 | |
| 12 | 156.4 | 220 | | | | | | 242 | 1120 | |
| 2 | .153.8 | 237 | | | | | 0 | 823 | 91. | = |
| 7 | .154.9 | 245 | | | | | 9 | 243 | 1165 | - |
| 15 | 122.1 | 179 | | | | | 0 | 313 | 296 | 182 |
| 10 | 121.0 | 181 | | | | | 3 | 020 | 8 | 25 |
| 12 | | 184 | | | | | 8 | 323 | 786 | × |
| 9 | .1220 | 196 | | | | | 3 | 328 | 0001 | 20, |
| 9 | .121.2 | 061 | | | | | 6 | 333 | 1005 | 214 |
| 2 | .121.3 | 196 | 198 | | | | 2 | 331 | 1001 | 213 |
| 21 | 120.4 | 211 | | | | |] | 305 | 1000 | 181 |
| 22 | .115.1 | 329 | | | .1232 | | 0 | 63 | 972 | } ÷ |
| R | 114.9 | 349 | .1216 | | | | 5 | 09 | 976 | 8 |
| 22 | .114.4 | 367 | 1284 | | | | D | 22 | 796 | 8 |
| 2 | | 416 | | | | | | S. | 766 | 26 |
| 3 | .112.9 | 918 | 1501 | | | | • | 3 6 | 1031 | .165 |
| 27 | 111.4 | 689 | 1756 | 6449 | | | | 981 | 1097 | .253 |
| 8 | -111.7 | 182 | .1969 | | | | 0 | .218 | 1132 | .278 |
| R | .106.0 | 1287 | -2462 | | | | , | -283 | 1220 | × |
| 8 | 103.5 | 800* | .5630 | - | 354 | | | .132 | 1234 | 9- |
| 7 | | | | | | | | | | |
| AXIAL | AXIAL FORCE (KN) | -25.4 | * * | ~ | -26.9 | <u></u> | 17.3 | | 17.9 | |
| M DING | DESIGNATION SECTIONS AND AND AND AND AND AND AND AND AND AND | | | | | | | | | |

AXIAL FORCES AND BENDING MOMENT IN TEST MEMBERS FOR SPECIMEN SG-B

| | T PANEL A (R | TEST PAKEL A (REAR DIAGONAL BUCKLE | BUCKLED FIRST | 6 | | | | Test Ser | Test Serial No. 13 |
|---------|---------------------|------------------------------------|--|--------------------|--------|--------|--------|-------------|--------------------|
| į | Lead (LIN) | Strain | a de la companya de l | a de la composição | Strata | Strain | 9train | 9trate | Strain. |
| | | | • | 44 | 12 | 13 | 14 | | |
| | 7.23.7 | 69 | 461. | 18 | | 146 | 41 | | |
| 2 | 408 | π. | | • | | | | | |
| 3 | .58.8 | .96 | | | | | | | |
| • | 4.77. | .101 | 199- | | | 459 | | | |
| 5 | 1.96. | -99 | | | | | | | |
| 9 | .105.5 | .73 | | | | | | | |
| 7 | -114.5 | S. | • | | | 989 | | | |
| 8 | .124.1 | | • | | | | i co | | |
| 9 | -133.4 | | | | | | | | |
| 10 | .142.4 | 19 | , | | | | | | |
| = | 151.7 | | | | | | | OSO OSO | - |
| 12 | 154.4 | | | | | | | | |
| 13 | .153.8 | | | | | | | | P 4 |
| = | -154.9 | 196 | | | | | | | |
| 5 | .122.1 | 155 | 1314 | | | | | | |
| 16 | .121.8 | | | | | 733 | 9 | | 5 |
| 1 | .122.2 | 165 | -1319 | | | | | | |
| 9 | .122.0 | 168 | .1316 | | | | | | |
| 62 | .121.2 | 176 | .1311 | | | | | | |
| R | .121.3 | 181 | .1314 | | | | | | |
| 21 | 120.4 | 184 | . 1312 | | | | | | |
| 22 | 115.1 | 174 | .1295 | | | | | | |
| R | 114.9 | 171 | .1297 | | | | | | |
| 25 | .114.4 | 186 | .1303 | | | | | 446 | |
| 28 | 113.8 | | | | | | | | |
| 8 | .112.9 | 506 | .1308 | | | | | | |
| 27 | 111.4 | | .1289 | | | | | | |
| 8 | 7.111.7 | | 9001 | | | 787 | | | |
| 8 | | 227 | 1148 | * 22. | | 06.4 | | | |
| 8 | 103.5 | 255 | 1223 | | | 776 | • | 7 09 | |
| | | | | | | | | | |
| AXIAL | AXIAL FORCE (KN) | 7 | -28.3 | -2. | .27.3 | 20 | 20.5 | 20.1 | - |
| NO MONE | BENDING MOMENT(N.m) | 2 | 79.7 | 8 | 28.0 | 7.16- | 1,7 | 125. | 93 |
| | | | | | | | | | |

AXIAL FORCES AND BENDING MOMENT IN TEST MEMBERS FOR SPECIMEN SG-B

| No. Load (143) Borates | Load (RM) | Berzen | Birnelm | Strain. | Berein | | Bérain | Strain | Strain | Strain | Bérrain | Strain | Strate | ı |
|------------------------|---------------------|--------|---------|---------|---------|-----|--------|--------|--------|--------|---------|----------|--------|------------|
| | | 47 | • | • | 20 | 21 | 22 | | 2 | * | | * | | 8 |
| 1 | 755. | | 6 | 01. | 0. | 2 | | 9 | | .37 | | | • | P |
| 2 | 807 | | 10 | | 5. | ~ | | 8 | | 2 | | | ; | 3 |
| | 85 | 42 | | | | 9 | | _ | قِ ا | S | | | , ; | ij |
| * | A 7.7. | -57 | | | 6 | | 2 | | | 9.5 | - 6 | n u | 2 2 | 6 |
| S | 198 | .73 | | | 7 | = | | | | (4) | • | 3 0 | | |
| 6 | 106.5 | | | | 7 | 8.1 | - | | | 5 | | | | • |
| 7 | 114.5 | | | | 4 | | | | | 2 1 | | | Ž. | 3 |
| • | 1241 | 8 | 8 | 3 | | | | | 2017 | 6,6 | | | 22 | 3 |
| • | 133.4 | .106 | | | | | | | | 200 | 1 | | | |
| 2 | 1424 | .113 | | | | | | | | 910 | 3 6 | | | 1 |
| = | .151.7 | 121 | | | ι. | | | | | 22. | 1 | <u> </u> | | |
| 12 | 154.4 | 126 | | | | | | | | ž | | | | ([|
| 13 | e 531. | 120 | | | | | | | | 22 | | | | |
| 1 | 9 121 . | | 19 | | | 02 | | | | 2 | | , | | |
| 15 | 1221 | 411. | | | 7 | 8 | | | | - | | | | ŧ. |
| 92 | .121.8 | +11+ | | | | 37 | | | | 3 8 | | | | 3 |
| 11 | 1222 | 911. | 23 | | 8 | 37 | ė. | | | ! \$ | | | | 3 |
| = | .1220 | -115 | | | | | | | | 2 | | | A | 3 |
| 2 | .121 2 | -112 | | | | | | | | | | | | 3 |
| 8 | .121.3 | 111. | | | | | | | | 5 | | | | |
| 2 | 120. | ,0t- | 8 | | | | | | | 9 | | | | 8 8 |
| 8 | 1151 | 24 | | | 72: | 33 | | | | 2 | | 2. | 36 | 3 |
| R | 9711 | 8 | 22: | | | | , | | | 98 | 6 | | 20 | 1 |
| 2 | | 12. | | | | | 9- | | | 98 | | | 96 | Fâ |
| il. | | Đ. | 7 | 41. | | | 9. | | | 98 | 9 | | 776 | 1 |
| 8 | 112.0 | 8 | * | 2 | ŝ | | 6 | | | 187 | 7. | | | Ę |
| 27 | | 2 | 051 | 27 | <i></i> | | • | | | | | | | |
| 티 | | 117 | | | * | | 1 | | | 8 | | | | Ţξ |
| 티 | | = | 712. | 3 | 8 | | 7 | | | | | | | П |
| 8 | 1035 | 132 | 281 | \$ | : : | | 14 | | | | 30. | | 320 | F |
| 1 | 1 | | | | | | | | | | | | | |
| M. | AXIAL FORCE (KN) | -22.2 | | -16.8 | 9 | • | | | 7.3 | | -69.7 | | 20.7 | ļ |
| 2000 | DENDING MOREHT(N.m) | 12581 | 11 | 25 | 2 | 234 | • | | 5.7511 | | 6 96 | | | Τ |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN S6-C

test pamel a (front ,pamel a not buckled because of panel c,d buckled after the first

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN S6-C

| 788 | IT PANEL A (R | TEST PANEL A (REAR DIAGONAL) | | | | | | Test Serial No. 24 | al No. 24 |
|----------|------------------|------------------------------|--------|--------|--------|--------|--------|--------------------|---|
| 4 | Lond Gitt | | Strate | Strate | Strain | Strain | Strain | Strain | Strate |
| | | • | 2 | = | 77 | | | | |
| - | 3.46 | .237 | C\$- | 182 | | | | | *************************************** |
| 2 | 9.99 | | | | | | | | |
| | | | | | | | | | 433 |
| | | | 3. | | | | | | 535 |
| | | | | | | | | | |
| 4 | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| 6 | | | 011. | 1651: | | | | | |
| 9 | | | | | | | | | |
| • | | | | | | | | | |
| 2 | | | | 01810 | | | | | 1120 |
| <u> </u> | | | | | | | | | |
| 1 | | | ş | | | | | | |
| 4 | | | | | | | | | 200 |
| 4 | | | | | | | | | 986 |
| 1.0 | | | | | | | | | |
| = | | | | | | | | | |
| 91 | | | | 9001 | | | | | |
| 8 | | | | | | | | | |
| 2 | | | | • | | | | | |
| 8 | | | | | | | | | 1001 |
| 8 | | | | .855 | 249 | 484 | -88 | 414 | |
| 2 | | | | | | | | | |
| 8 | | | | | | | | | |
| 8 | | | | | | | | | |
| 27 | | | | | | | | | 1062 |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |
| AXIAL | AXIAL FORCE (KN) | | - | | | | | | |
| | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN 318RB

| | | T LEG BUCK | SEV FINOIS IN | THURSDAY BY | AAKEU . | | | Ì | | | Ĕ | | 7 |
|-----------|-------------------|------------|---------------|-------------------|---------|--------|--------|-------------|--------|------------------|--------|-----|---------------|
| į | 3 3 3 | - | at a second | the Strate Strate | į | Otrafa | Strain | Strate | Strain | Strain | Strain | ŀ | Otrada |
| | | | | | | | | | | • | | | 12 |
| | -6.2 | 8 | 8 | 32 | | | | .34 | | | | | |
| 2 | | | | | | | | | | | | | |
| 3 | | | | | | | | • | 901- | 103 | | | |
| * | -27.9 | 124 | | 117 | | | | | | | | | |
| 2 | -32.3 | | 201- | 135 | | | | | | | 131 | | |
| 9 | | .160 | | 151 | | | | | | | | | |
| 7 | -41.2 | | | 1689 | | | | | | 061 | | | |
| 9 | .45.6 | | .147 | 186 | | | | | | | | | |
| 6 | | .241 | -161 | | | | | | | | | | |
| 10 | | .267 | -176 | | | | | | | | | | |
| 13 | | | .175 | | | | | | | | | | |
| 12 | | | | | | | | | | | | | |
| 13 | 6 .99- | | .213 | | | | | | | | | | |
| 14 | -71.4 | | | | | | | | | | | | |
| 5 | | | | | | | | | | | | | |
| 16 | | | | | | | | | | | | | |
| 17 | | | | | | | | | | | | | |
| 6 | | | | | | | | | | | | | |
| 9 | -94.1 | | | | | | | | .370 | | | | |
| ଛ | | | | | | | | | | | | | |
| 21 | ļ | | | 414 | | | | | | | | | |
| 22 | | | | | | | | | | | | | |
| R | | | | | | | | | | | | | |
| 24 | | | 328 | | 521 | 089 | 644 | -547 | | .57 9 | 905 | 167 | 742 |
| 8 | | | | 486 | 250 | | | | | 965 | | | |
| 8 | | | | S | 257 | | | | | 919- | | | |
| 27 | | | 346 | 212 | 574 | | | | -478 | -633 | | | |
| 8 | | | | 235 | 291 | | | | | -650 | | | |
| 8 | - | | | 246 | 909 | 989 | | | | 599- | | | |
| R | - | | | \$2 | 618 | | | · | | 599- | · | | |
| Ē | ļ | | | 287 | 627 | 710 | | | | 099- | -647 | 613 | |
| 2 | | | 745 | 576 | | 716 | | | | 199- | | 8 | |
| g | | .507 | 592 | 200 | | 418 | 320 | 725 | -249 | 417 | | 34 | |
| | 689.3 | 7 | .260 | 325 | | 411 | | • | .244 | 4.4 | .351 | 456 | |
| AXIAL FOR | FORCES(NA) | -46 | 5.1 | 47 | 2 | 64 | 9. | 19 - | 4. | ķ | rć. | 36 | rů. |
| |] | | | | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN 31SRB

| į | 1111111 | ij | į | a de la companya de l | 414 | Strate | Strafe | | | Strain | dere | | |
|----------|-------------|-----|------|--|-------|-------------|-------------|------|-----|--------|------|------|------|
| | | 13 | 14 | 48 | 10 | - | | _ | | K | | _ | ** |
| | 1 -8.2 | 37 | 33 | .33 | 3 .37 | .31 | | | | æ | | | 5 |
| | 2 .15.5 | 88 | 61 | 69 | | | | 101 | | 72 | | 83. | 98. |
| | 3 .23.7 | 103 | 92 | .109 | • | 69 - | • | | | 901 | | | 137 |
| | 4 .27.9 | 124 | 112 | 128 | 137 | | | | | 128 | | | 163 |
| | 5 .32.3 | | 131 | -147 | | | | | 145 | 251 | 98 | | -185 |
| | .36.7 | | 151 | -165 | | | | | | | | 611. | 012- |
| | 7 -41.2 | 98 | 171 | -162 | | 151- | | | | | | | .236 |
| | 45.6 | | 181 | -20- | | | .225 | | | | | | 198. |
| | 9 .50.1 | | 213 | | | | | | | | | | 288 |
| | -54.7 | | 234 | .237 | | | | | | | | | 316- |
| | -54.6 | | 223 | 723. | | | | | | | | | 316 |
| | | 287 | 289 | | -294 | | -316 | | | | | | 363 |
| | 13 -66.9 | | 282 | -285 | | | | | | | | | 388: |
| | 14 -71.4 | | 313 | | | | -367 | | | | | | -421 |
| | 15 .75.8 | | 332 | -321 | | | | | | | | | 448 |
| | 16 -80.4 | 380 | 356 | | | | | | | | | .213 | 2,4 |
| 17 | | | 376 | | | | | | | | | | -510 |
| | 18 -89.6 | 434 | 386 | -372 | | | -476 | | | | | | 545 |
| | | | 418 | 986 | | | | | | | | 0CZ: | -574 |
| 2 | -96.5 | | 436 | | | | -532 | | | | | | 909 |
| 2 | | | 460 | 418 | | | | | | | | | 9 |
| Ci | 107.5 | | 481 | 430 | | | -591 | 847 | | | | | -674 |
| 2 | 3.111.6 | | 501 | \$ | 544 | | | | | | | | 902- |
| 24 | | | 522 | -455 | .573 | -407 | -649 | | 481 | 603 | 986 | .241 | -744 |
| Ä | 120.7 | 280 | 543 | -465 | | | | | 609 | | | | 783 |
| E | .124.9 | | 563 | 899- | | | .713 | | 525 | 653 | | | 929 |
| 8 | | | 583 | 691 | | -430 | -745 | 1102 | 542 | 677 | | | 788. |
| 4 | | | 601 | -466 | | | 977- | | 558 | 703 | | | -88- |
| ~ | | | 618 | 194- | | | | | 574 | 727 | 474 | -218 | -933 |
| ē | | 988 | 633 | 064- | -902 | -426 | .850 | 1214 | 584 | 751 | | | 596- |
| C | | | 644 | -380 | | -407 | 89 • | 1239 | 583 | 773 | | | 186- |
| Ħ | | Ž | 6462 | -316 | | 372 | 996- | 1280 | 009 | 783 | | | -100 |
| 33 | | 453 | 386 | 314 | -1149 | 215 | | 1058 | 358 | 594 | | | 185- |
| ਣ | -88.3 | 946 | 381 | 319 | -1145 | 214 | 1014 | 1069 | | 585 | | | 173- |
| AXIAL FO | FORCE B(MV) | 53. | | 9 | 9.7 | -5 | .5 | 64 | | 35 | e a | | - |
| | | | | | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN 31SRS

| į | 7 | Ptrain. | Strafe Table | 1 | | | | Strate | Strake | Strain | Strain. | Strate | Strain Str. | Strate | |
|-----------|-------------|---------|-----------------|----------|-------------|-----------------|-------|--------|--------|--------|------------------|--------|-------------|--------|-----------|
| | | R | | | E | 23 | X | | 31 | 1 32 | 22 | | | 2 | * |
| | 1 .8.2 | -43 | 98 | 9 | -20 | -36 | | | .39 | 62: / | | 37 | | | 18 |
| ," | -15.5 | \$ | -74 | | -51 | -67 | 64. | | | | | 27. | - | _ | 4 |
| | 3 .23.7 | .127 | 111- | 1 | .73 | -86 | | | - | | -13 | | | | 9 6 |
| 1 | -27.9 | .151 | .131 | 1. | 69 - | -120 | | | | | 31. | | 8 | | 911 |
| | 32.3 | .166 | -149 | 6 | -104 | .142 | | | | | | | - | | 2 |
| | 36.7 | 166 | 991 | | 120 | .167 | 181- | | | | | | - | | 8 |
| | 41.2 | -210 | .187 | 12 | -137 | 181 | 961- | | | | | | 4 | | 1 |
| • | .45.6 | .229 | -206 | 9 | .151 | .211 | -218 | | | | | | | | 200 |
| 6 | .50.1 | -249 | .226 | - GS | .167 | -236 | -236 | | | | | | 6 | | .22 |
| 9 | 54.7 | .289 | -245 | <u> </u> | .181 | .281 | .25 | | | | | -244 | - | | Š |
| = | 54.6 | .270 | .246 | 8 | -182 | -262 | .25 | | | | | | | | Ş |
| 12 | | .307 | -284 | | -208 | -310 | 962- | | | | | 976. | | | 280 |
| 13 | | .324 | | 6 | .221 | -332 | EIE. | | | | ğ | | 100 | | 313 |
| 7 | | .345 | | | -236 | .358 | 333 | | | | | | | L | 336 |
| 15 | | 236 | | | -247 | -381 | .351 | | | | , , | | | | .356 |
| 9 | | 286: | -362 | Rul | -261 | -410 | 376- | | | 317 | 🖣 | | _ | | 385 |
| 17 | | +05 | 385 | | -275 | 144. | .390 | | | | | | | | 406 |
| 2 | | -421 | -405 | | -285 | 63 4 | -410 | | 9 .440 | | | | - | | 428 |
| 2 | | 945 | 425 | | -285 | 484- | -428 | .428 | .461 | .375 | | E09- | | | 452 |
| श | | .457 | -444 | | 304 | :522 | -445 | | 9 -484 | | | | | | -475 |
| 2 | | 476 | .467 | | -314 | -554 | 29 | | | | | | | | 98 |
| X | | -493 | -468 | | -321 | 583 | 184 | | | | 35 | | -60 | L | 35 |
| ผ | | -511 | -512 | | -331 | -616 | .500 | -509 | | | ġ | | | | 543 |
| 2 | | 528 | -534 | | -337 | \$ | -518 | | 1-571 | | 35 | | | | 567 |
| £ | | 543 | 755 | | -339 | -89 | -535 | | 1 -591 | | 29 | | | | -590 |
| 8 | | 929 | -579 | | .340 | .716 | .550 | | | | \$ 9 | | | | -612 |
| 22 | | .573 | -605 | | 342 | .751 | -564 | -592 | .626 | | .9- | .537 | | | 63 |
| 82 | | -587 | 029- | | -338 | .791 | .579 | | | | \$ \$ | | | L | .655 |
| ĝ | | .596 | .653 | | 334 | 828 | -594 | -633 | | | 12. | | | | -677 |
| 8 | | 909- | -678 | | .322 | 998 | -603 | | | | .73 | | | | -692 |
| ē | | -613 | 989- | | -306 | 900 | -608 | | | | 27. | | | | .703 |
| R | | Ę | -700 | | -288 | -428 | -607 | 411 | 7 -642 | -645 | 7. | | | | -712 |
| 8 | | 380 | | | -150 | -629 | -400 | 1441 | 114- | | 97 | 1985 | | | 454 |
| ह | .88.3 | -392 | -458 | | -147 | -619 | -394 | -433 | 3 -404 | | 74. | | | | -447 |
| AXIAL FOR | FORCES(IAN) | -51 | .6 | | 47.4 | | -50.1 | 0.1 | ç. | -51.0 | 97- | 3.2 | | | |
| _ | | | | | | | | | | | | | | | Ī |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN 33SRC

| | | | | | | | | | | | CEST CONTROL INC. 10 | 5.5 | |
|----------|-------------------|------|-------|--------------|------|-------|----------|-----------------------|--------|---------|----------------------|-------------|--------|
| ź | Lond kill | | | • | | · | <u> </u> | 4 | Strain | Strain | | Otrada A | Strate |
| | 1 -46.0 | 40. | 108 | 397 | 58: | 5 | 18 | 1 | | | | | 2 |
| | -56.4 | 121 | 138 | | | | | | | | | 2115 | 121- |
| | 3 -68.2 | | 891 | | | | | | | | | | .151 |
| | -87.3 | | 912. | | | | | | | | | 176 | 181 |
| | S 110. | | | | | | | | | 156 | 282 | .225 | .238 |
| | | | 3 | | | | | | 7237 | .197 | -339 | | -308 |
| | | | Ş. | | | | | 346 | .265 | .219 | | | 246 |
| | | | S. | | | 333 | .379 | -379 | -280 | 822· | | .357 | |
| | | | 424 | | | 380 | -453 | -450 | | | | | 467 |
| | | | -468 | | | 430 | -500 | 494 | | | | | 3 |
| | | | 90S | | | | | | | | | | anc. |
| | | | 586 | .724 | | -527 | -626 | | | | | | 200 |
| 12 | | | 629 | 677. | -357 | | | | | 986 | | | |
| 13 | | | -675 | 940 | | -595 | .720 | | | 300 | | | è |
| * | | | -715 | 5889 | | | | | | 300 | | | 1 |
| 15 | | | .762 | 956 . | -407 | | | | 3 | 014 | 700 | | .782 |
| 9 | | 929 | -805 | -1018 | | | | | | 917 | | | 2 |
| 17 | | 9/9- | -862 | .1128 | 194- | | | | | 450 | | | 8 |
| 18 | | .703 | .829 | 1192 | -450 | | | | 84 | 2 | | | D. 6. |
| 2 | | 1231 | -977 | 1250 | -456 | | | , | 2.7 | 433 | | | .1022 |
| 8 | .367.0 | .753 | .1020 | .1320 | 191 | | | | 746 | Ž. | | | -1076 |
| 21 | 1 .378.7 | 177- | .1057 | .1373 | 899- | .A.24 | | | 200 | 2 | | | 128 |
| Ø | -382.3 | .783 | 1103 | | 675 | | | 3 | 90/. | -631 | | | 1168 |
| ผ | 8 407 8 | -814 | 1155 | | 807 | | | 911 | Ş | 724 | 1478 | 1006 | .1220 |
| 24 | | 2 | 1201 | | 100 | 9/9- | | 1202 | -815 | 407 | 1588 | 1042 | 1281 |
| 8 | | 243 | 1363 | | | Sec. | 1,200 | 122 | 988- | 381 | 9991 | -1077 | -1344 |
| 8 | | - | 91.0 | | 959- | /80 | 1382 | 1306 | 255 | 301 | 1834 | .1121 | .1440 |
| 27 | | 3 | 1000 | | 914: | 788- | 1379 | - 338 | -857 | -256 | 1922 | .1143 | .1485 |
| 8 | | 3 | | | 3 | S | -1411 | 1383 | 198- | .207 | -2015 | .1165 | 1536 |
| 8 | | 200 | 350 | | | 988 | 1450 | 1381 | 936 | -116 | 7912 - | 9611- | .1619 |
| | | | 2 | cnsi. | 381 | 878· | .1490 | -1409 | -873 | 20 | 2962 | 1254 | -1746 |
| 1 | 1 | Î | 22. | | 36 | * | -1532 | -1436 | 198 | 254 | 2865 | 11371 | 200 |
| 5 | 2,6 | 112 | 2 | 961 | 87 | 99 | -435 | -58780 | 31908 | 4088 | -23604 | 10430 | 13307 |
| | | | | | | | | • | | | | | |
| 20 10 10 | AVIAL EABASE ALAN | | | | | | | buckled inside | Inside | | buckled outside | outside | |
| SAIME TO | MACO (MM) | 7 | 2 | -147 | 7.3 | -154 | 3 | -148.6 | 3.6 | -150.5 | 0.5 | -21 | -212.B |
| | | | | | | | | | | | | | |

AXIAL FORCES IN TEST MEMBERS FOR SPECIMEN 338RC

| | | Strate | 4 | Bernis | Service Control | 4 | - Transfer | Short | | | | ſ | |
|-------|--------------|--------------|-------|--------|-----------------|--------|------------|--------|-------|--------------|-------|--------|--------------|
| | | 13 | 14 | _ | | _ | | + | 8 | 7 | 22 | 2 | z I |
| | 1-46.0 | 121. | .113 | .122 | | -92 | 127 | • | | 115 | | | į |
| | .564 | 147 | .136 | -147 | | • | | | | | | | 136 |
| | S -68.2 | 174 | .163 | .175 | | -135 | | | 191. | | | | 181. |
| | .67.3 | .219 | -206 | .222 | | .168 | | | | | | | 902 |
| | .110.8 | 3 -273 | -260 | .278 | 252- | -210 | | | | -280 | 304 | | 26. |
| | .124.0 | .303 | .291 | -312 | | -231 | 346 | | | | | | 200 |
| | 138.5 | 332 | -321 | .342 | | | | | | | 976- | | 322 |
| | 162.2 | 986 | -382 | -406 | .361 | 282 | | | | | | -472 | 3005 |
| | 177.8 | -423 | -421 | | | | | | | | | | -420 |
| 2 | 192.9 | 457 | -457 | -485 | | | | | | | | | -450 |
| = | .220.3 | -519 | .526 | 999 | | | | | | | | | -511 |
| 12 | .235.4 | .552 | -565 | | | | | | 985 | 895 | | 585 | 540 |
| 13 | .251.8 | 88 5: | -606 | 9-9- | | | | | | | | | 773- |
| = | .265.5 | -616 | .641 | -676 | | | | | | | | | 909- |
| 2 | 282.1 | 999 | -685 | .721 | | 894- | 198- | | | | 628 | 618 | -636 |
| 9 | -297.0 | 889 | .725 | .763 | | | | | 756 | | .870 | | -665 |
| 2 | .323.1 | .743 | 282 | -834 | | | • | | 629 | | 656. | | .718 |
| | .336.5 | 577- | .836 | .877 | | 2ES: | .1073 | | .873 | 992. | 1004 | 8 | 745 |
| 9 | .353.4 | 908 | .877 | 928· | | -546 | .1133 | 191. | 916- | | 1056 | • | 577- |
| ત | | | 916- | .95e | | -557 | .1188 | | 956 | | 1102 | | 967. |
| 2 | | | 946 | 286- | .796 | 995 | .1238 | .B17 | 166 | 168- | -1142 | | 818 |
| × | -382.3 | 288 | 986 | .1033 | 228 | -575 | .1297 | 948- | -1030 | .853 | 1611. | | -839 |
| R | | | .1030 | 1079 | | 583 | 9901- | | 1077 | 728- | | | -965 |
| ă | | | 1072 | .1124 | -872 | -588 | .1430 | ∙904 | .1120 | 269 - | | | -885 |
| ĸ | -433.3 | 286 | 1114 | .1166 | | -589 | .1483 | | 9511. | 016- | | | 689· |
| 8 | | 970 | .1132 | .1185 | | .588 | .1522 | .943 | 1175 | 116- | 1361 | | 106 |
| 27 | | | 1150 | 1204 | 906 | -587 | -1552 | | -1192 | -922 | 1384 | 7181. | 906 |
| 8 | | | -1172 | .1226 | | .580 | 1587 | | 1210 | 226- | .1407 | .1336 | ÷06- |
| 8 | | | -1196 | .1248 | 026- | -574 | .1629 | .983 | 1231 | -824 | 1434 | .1356 | 906· |
| R | Ŧ | -1003 | -1220 | -1271 | -828 | -563 | -1672 | | -1252 | -927 | -1466 | 1361- | 906 - |
| 3 | 2.6 | 81. | 380 | -378 | | 901 | 19. | 10- | 14 | 89 | 17. | 101 | *1 |
| | | | | | | | | | | | | | |
| | | | | | | | | | | | | | |
| AXIAL | FORCES (KIN) | -142.6 | 2.6 | -14 | 1.1 | -143.4 | 3.4 | -144.4 | 1.4 | -153.5 | 3.5 | -146.6 | 6.6 |
| | | | | | | | | | | | - | | |

LXIAL FORCES IN TEST MEMBERS FOR SPECIMEN 33SRC

| | | | | | | | | | | | TOTAL COLUMN INC. 10 | | | |
|----------|-------------|------|----------|-------|-------|--------|------|--------|------|---|----------------------|---------|--------------|---|
| į | 3 | R | 7 | *** | | | | Į. | | | Strain. | Otrain. | Strade | |
| | 46.0 | | A01. | | | | | | * | 2 | X | | 2 | * |
| | 2 -58.4 | | æ1. | | | | | 551. | 501. | | | | + | |
| | 3 -66.2 | | 951. | | | | | | | | | | + | |
| | 4 -87.3 | | 5003 | | 222 | 223 | | | | | | | \downarrow | T |
| | 5 .110.8 | | -256 | | 282: | 283 | | | | | | | + | |
| | .124.0 | .33 | -286 | | -316 | | | | 176. | | | | 1 | |
| | 7 -136.5 | | .320 | | -349 | | | | Ş | | | | + | |
| | .162.2 | -42 | -362 | | 415 | | | | 956 | | | | 1 | |
| | 9 .177.8 | 94- | -420 | | | | | | 8 | | | | + | |
| 2 | | | -457 | | | | | | 123 | | | | 1 | |
| Ξ | 1 .220.3 | 95 | -527 | | 295 | 155 | 381 | | | | | | + | T |
| 12 | 235.4 | | -566 | | 989 | 185. | 904 | | | | | | \downarrow | |
| 13 | | | -609 | | 969- | *** | 044 | | 930 | | | | - | |
| = | | | -646 | | 079- | -671 | 994 | | 555 | | | | \downarrow | |
| 15 | | | -690 | -613 | 902- | -712 | | | 629 | | | | | |
| 16 | | | .731 | -855 | .743 | .752 | 929 | | 209- | | | | | |
| 7 | | | -802 | 008 | -902 | -820 | ¥29· | | -639 | | | | | |
| 9 | | | -645 | -975 | 838 | 1961 | -602 | | 959 | | | | | |
| 18 | | | -666 | 1018 | -872 | -904 | -630 | | 229- | | | | | |
| R | | | -925 | .1059 | 106- | 0+6- | 653 | | 695 | | | | | |
| <u>ت</u> | | | 956 | 1094 | -927 | 126- | -675 | 1309 | 507. | | | | | |
| Z | | | -986 | | 458 | 0101- | | -1379 | 111. | | | | | |
| R | | | 1044 | | 286 | 9501- | .725 | -1472 | 602- | | | | _ | |
| 2 | | | 1084 | 1257 | .1000 | -1099 | 647- | 1564 | 669· | | | | - | |
| 8 | | | 1124 | .1316 | .1010 | .1138 | 177- | -1674 | .673 | | | | - | |
| 8 | 438.3 | 107 | 1140 | -1342 | -1012 | -1154 | 677- | 22/1- | 999 | | | | L | |
| 2 | ļ | | .1157 | .1365 | 7101. | 1711. | 788 | 1768 | 649 | | | | - | |
| 8 | | | .1176 | 1395 | 9101- | .1190 | 787- | 0081. | 9. | | | | _ | |
| 8 | | -111 | -1196 | -1421 | .1022 | .1209 | 908 | 1883 | -615 | | | | - | |
| 8 | 7 | -112 | -1210 | -1446 | -1025 | -1233 | 718 | 3081- | ** | | | | | |
| ē | 2.6 | 8 | 8 | -54 | S | 9 | 11 | 175 | 22 | | | | L | |
| | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | |
| AXML 70 | PORCES (RM) | 3 | 5 | -158. | 9.5 | -131.3 | .3 | -162.4 | 7 | | | | | |
| | | | | | | | | i | - | | | | | |

VITA AUCTORIS

Yean Sun was born in Weifang, China on March 3rd, 1966.

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